



Outline

- Precipitation Hardening
- Dispersion Strengthening
- Martensite
- Mechanical Properties of Steel
- Effect of Pearlite



Precipitation Hardening

- Particles **impede** dislocations.
- Things that slow down/hinder/impede dislocation movement will increase, σ_y and σ_{TS}

• And also other phases - especially v. small, well dispersed particles.
In some alloys, we can get small, uniform particles to precipitate out of (solid) solution. Hence named "precipitation hardening" also known as "AGE" - hardening. Examples include:

- Al-Cu
- Cu-Be
- Cu-S
- Mg-Al
- Some alloy and stainless steels

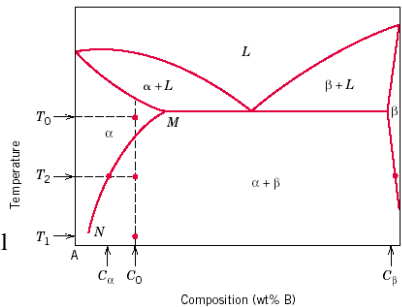
- Many **Al-alloys** are precipitation hardenable
- **Al - Cu** is best known alloy, e.g. Al - 4% Cu



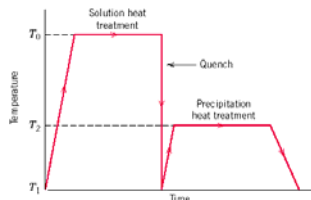
Precipitation Hardening

Procedure:

- Heat to T_0 ; Hold until only α - phase present.
- Quench (**rapid cooling**) to T_1 ; because rapid, no diffusion occurs - SSSS - Super-saturated solid solution of α forms. B atoms "....." in α . Not thermodynamically stable.
- Reheat to T_2 ; diffusion can occur, small precipitates of β -phase form.

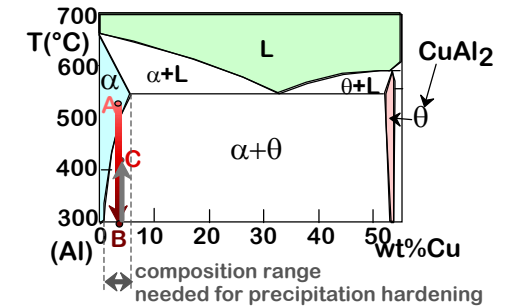


M = Max. solubility of metal B in metal A.
Solid solubility decreases to N as $T \downarrow$

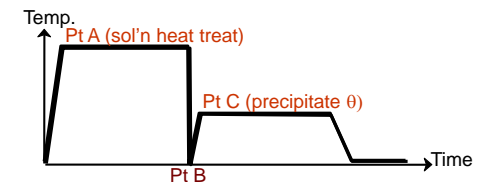


Precipitation Hardening

- Ex: Al-Cu system
- Procedure:
 - Pt A: solution heat treat (get a solid solution)
 - Pt B: quench to room temp.
 - Pt C: reheat to nucleate small θ crystals within α crystals.



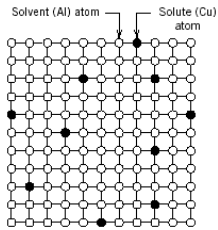
$\alpha + \theta \rightarrow$ Heat ($\sim 550^\circ\text{C}$) \rightarrow Quench (0°C) $\rightarrow \alpha$ (sss) \rightarrow Heat/age ($\sim 150^\circ\text{C}$) $\alpha + \theta_{ppt}$





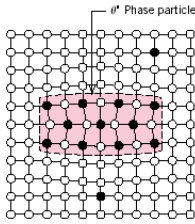
Precipitation Hardening

Single phase - α (SSSS)



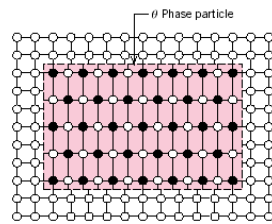
Initially have a supersaturated solid solution of Cu in Al

$\alpha + \theta''$ ppt



- form various zones or small Cu clusters
- upon further aging form θ'' particles

$\alpha + \theta$ ppt



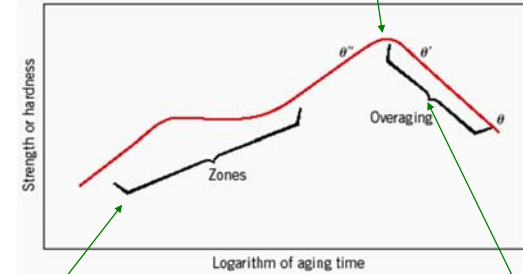
Can no longer match up with each other (.....)
- less resistance to dislocation movement

Lattices are trying to match up with each other (stay) - large lattice strain - high resistance to dislocation movement



Precipitation Hardening

Max. strength/hardness



Formation & growth of precipitates. These are very small ($5 \times 10^{-9}m$) initially but grow with time.

Too long at temperature and precipitates get too large and occurs.

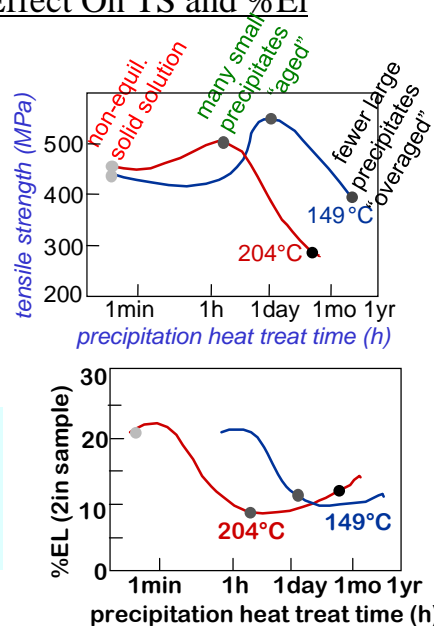
- θ' is the optimum for strengthening
- θ is overaged because the precipitates are becoming incoherent with the Al matrix



Precipitate Effect On TS and %EL

- TS peaks with precipitation time.
- Increasing T process.
- %EL reaches minimum with precipitation time.

• Higher strength achieved at lower ageing temperatures but for longer times
• Consequently, if cold-working is to be done, it should be carried out after and before



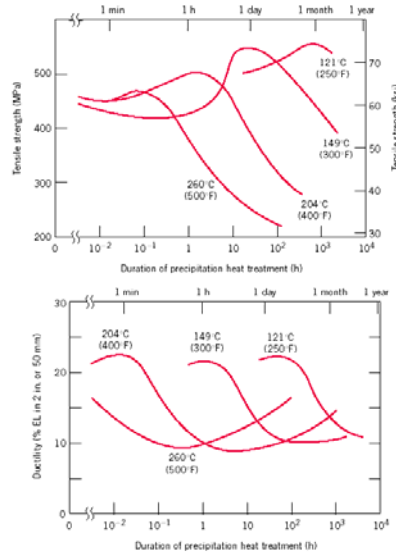
Simulation of Effect of Precipitate Size on Dislocation Movement



Precipitation Hardening

2014 Al Alloy:

- **Natural aging** occurs at **room temperature**
 - so will start aging at RT unless stored at low temperature - *freezer!*
E.g. some Al-alloys for rivets
- **Artificial aging** occurs at **elevated** temperature and is accelerated
- Aluminum alloys which show *age hardening* are:
 - Al-Cu
 - Al-Mg
 - Al-Mg-Zn
 - combinations of above



Dispersion Strengthening

- Adding very small foreign particles (**hard** + **inert**/non-reactive) into matrix metal.
- Particles may be metals/non-metals but oxides are often used - Thorium oxide (Thoria/ThO₂)
- Like *precipitation hardening*, particles interfere with dislocation movement
- But not as large strengthening effect, however, not greatly affected by temperature - so good for applications.

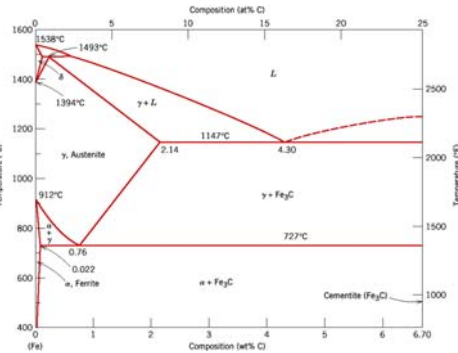
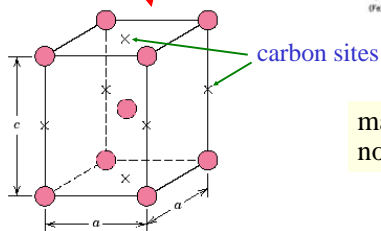
Examples:

- Nickel + 3 vol% Thoria (*TD Nickel*)
- SAP (*sintered Al. powder*)



Martensite

- Austenite dissolves **~2% C** whereas ferrite only dissolves **0.022% max.**
- If a medium to high carbon steel is *quenched* then **C remains** in solid solution forming a body-centred tetragonal phase (BCT) called ***martensite***

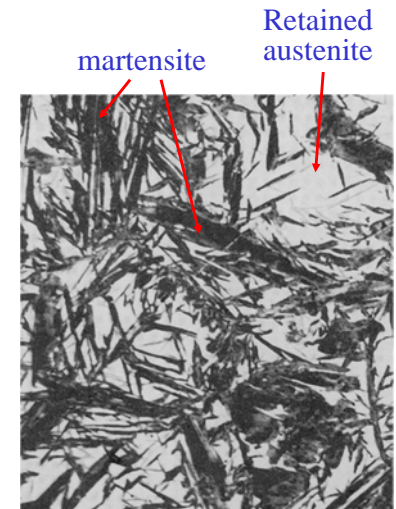


martensite is and does not appear on the phase diagram



Martensite Microstructure

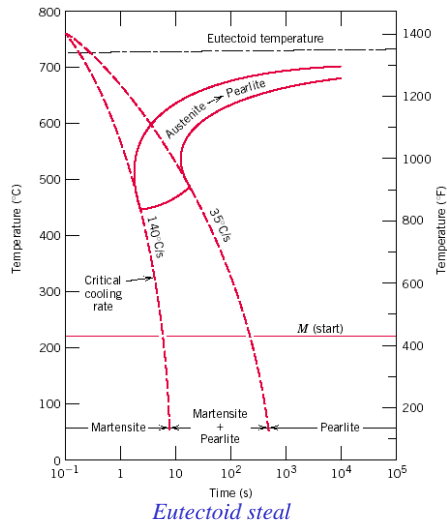
- Diffusionless transformation: $\gamma \rightarrow \alpha$ -martensite (*very fast*)
- platelike or needle-like appearance
- microstructure always contains *retained austenite*
- microstructural development of *martensite* and *bainite* defined by **transformation curves**,
 - e.g.: time, temperature, transformation (TTT)
- **alloying element** affect the *ease* of martensite formation





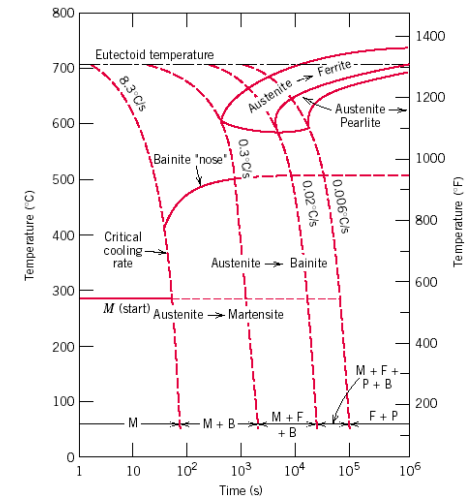
Martensite

Note: need to cool faster than 140°C/s to get 100% martensite!



Martensite

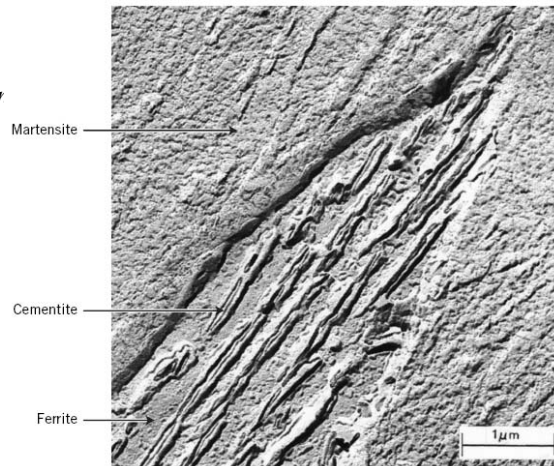
Alloy steel; + Ni, Cr, Mo.
Get martensite at slower cooling rates.



Bainite

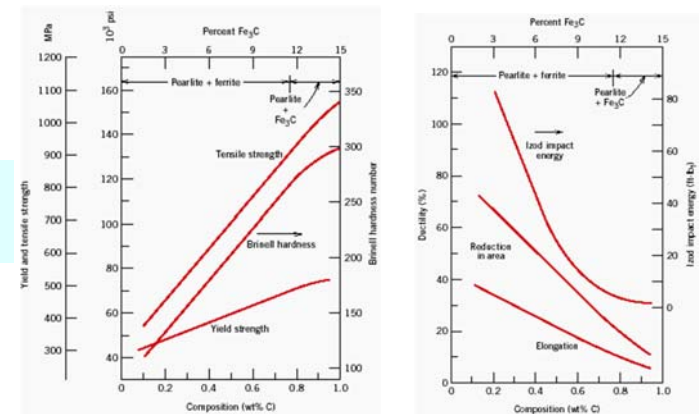
How does the bainite look like?

FIGURE 10.17 Transmission electron micrograph (TEM) showing the structure of bainite. A grain of bainite passes from lower left to upper right-hand corners, which consists of elongated and needle-shaped particles of Fe₃C within a ferrite matrix. The phase surrounding the bainite is martensite.



Mechanical Properties of Steel

Effect of Fe₃C and pearlite



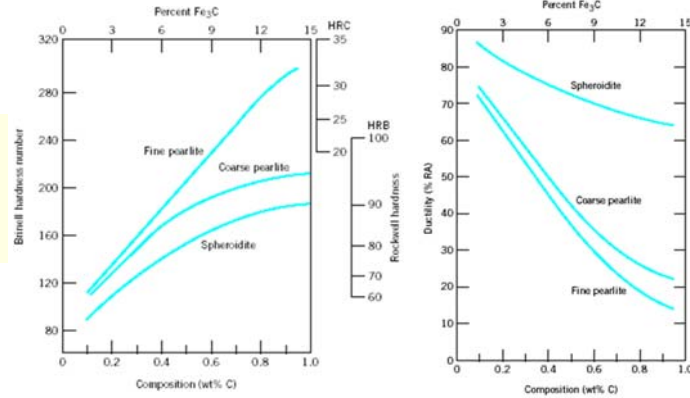
- Depending on microstructure, obtain different mech. properties
- amount of Fe₃C (hard phase) in microstructure the **hardness** and **strength**
- whereas, the **ductility** and **impact resistance**



Effect of Pearlite

- Fine pearlite is **stronger** and **harder** than coarse pearlite
- cementite adheres strongly to ferrite and **restricts** its deformation (*reinforces*)
- plastic deformation (dislocations) cannot cross α -Fe₃C phase boundary

Boundary area/unit volume is much **greater** in the case of ***fine pearlite***



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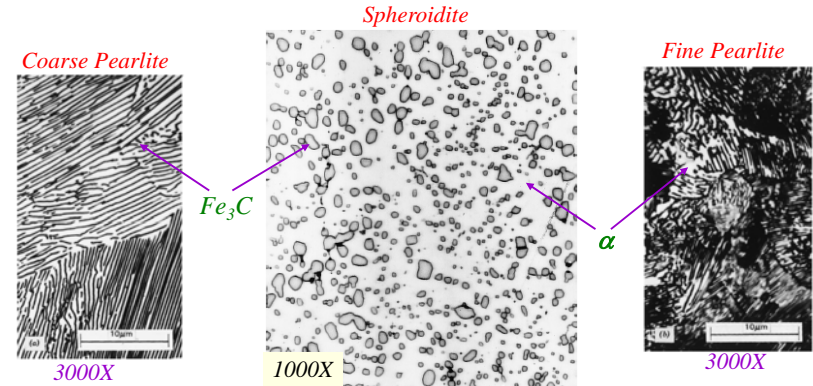
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Spheroidite

- **least** boundary area/unit volume
- soft, **low strength** and **ductile structure** (easy to machine)
- spheroidized carbide is a **low stress raiser**



Spheroidite vs. fine and coarse pearlite

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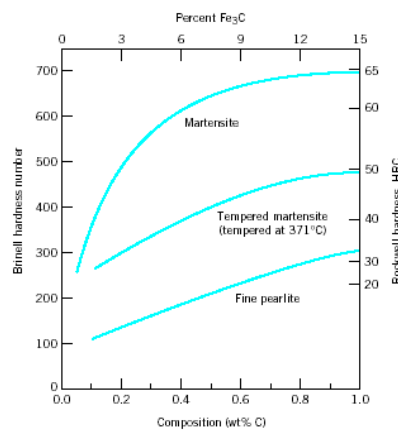
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Martensite

- Hardness of martensite is dependant on the carbon content up to **~0.6%C**
- plastic deformation (dislocation motion) is restricted by **interstitial carbon**
- high carbon martensite is the **hardest most brittle** microstructure in steel
- there is an increase in **volume** upon quenching which can cause **cracking**



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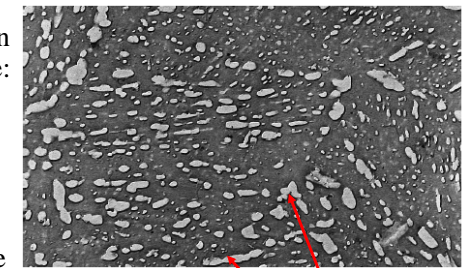
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Tempered Martensite

- **Tempering** (heating) at 250-650°C allows diffusion of carbon out of **supersaturated** martensite:
 α -martensite \rightarrow α -ferrite + Fe₃C
(bct) (bcc)
- Microstructure is **tempered martensite**
- Cementite precipitates (hard) are **very fine** and **dispersed**
- Continuous α (ductile) phase
- **Very large** boundary area/unit volume
- This microstructure makes TM and



9300X

Cementite precipitates

When both TM structure and pearlite structure have the same strength, the fracture toughness of TM structure will be much than that for pearlite structure.

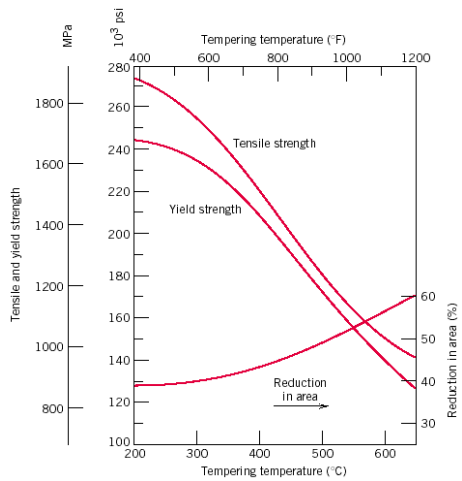
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Effect of Tempering on Mechanical Properties of Steel



- The mechanical properties are affected by the precipitate size
- Precipitate size with tempering *time* and *temperature* up to the eutectoid composition (carbon diffusion)

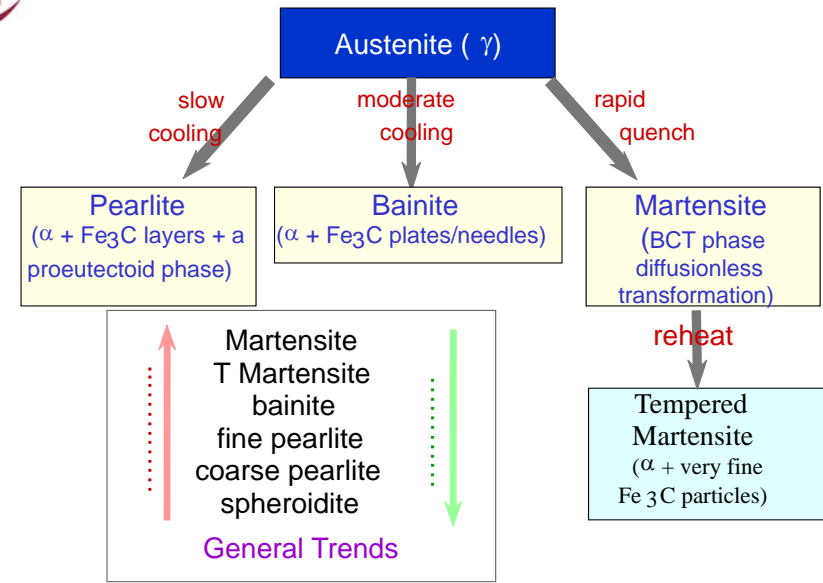
The microstructure will become Spheroidite

Note high yield strength:
Maximum with fine pearlite was 500MPa.

1 hour tempered 4340 steel

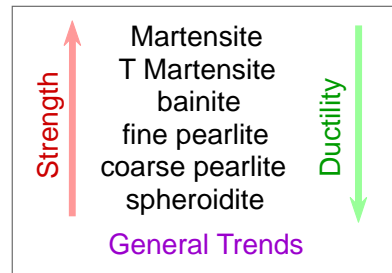


Summary: Processing Options



Summary

- The versatility of steel arises because of the wide range of microstructures that can be achieved, and the corresponding wide range of mechanical properties.
- In general, steel microstructures in which carbides are more finely dispersed have strength and fracture toughness.



Next topic:
Composites

