

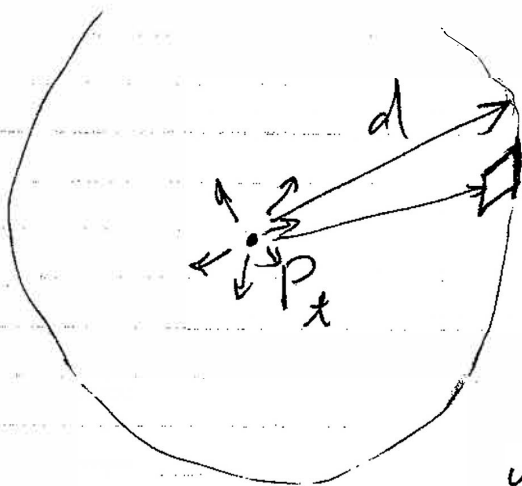
Mobile Radio propagation:

Large Scale path loss.

Line of Sight (LOS): Free Space Model

Take a transmitter with power P_t with an omnidirectional antenna. A receiver at a distance d receives a power density of $\frac{P_t}{4\pi d^2}$ where $4\pi d^2$

is the area of the a sphere of radius d .



If an antenna with an effective area A_e , the received power will be:

$$P_r(d) = \frac{P_t}{4\pi d^2} A_e$$

The gain of an antenna is related to its effective area as:

$$G = \frac{4\pi A_e}{\lambda^2}$$

where $\lambda = \frac{c}{f}$ is the wavelength of the transmitter

signal. Substituting A_e (in terms of G_r) in the expression for received power, we get

$$P_r(d) = \frac{P_t G_r \lambda^2}{(4\pi d)^2}$$

If instead of an omnidirectional antenna, the transmitter sends information using an antenna with a gain G_t , then P_t is replaced by $G_t P_t = \text{EIRP}$, i.e.

Effective Isotropic Radiated Power.

So, for LOS propagation, we have

$$P_r(d) = \frac{P_t G_t G_r}{(4\pi d/\lambda)^2} = \frac{P_t G_t G_r}{L_s}$$

where $L_s = \left(\frac{4\pi d}{\lambda}\right)^2$ is the path loss.

If there are other losses such as rain fading or insertion loss in cabling and connections we have

$$P_r(d) = \frac{P_t G_t G_r}{L_s L_o}$$

where L_o is the product of all other losses.

To put this in dB, we have

$$P_r(d) \text{ in dBW} = P_t + G_t + G_r - L_s$$

where L_s is the path loss in dB, i.e.,

$$L_s = 10 \log \left(\frac{4\pi d}{\lambda} \right)^2$$

Example: A transmitter transmits at ~~a rate~~ with 50 W power at a frequency of 10 GHz. to a satellite at a Geostationary orbit (at an altitude of 36000 km.). Find the received power at the satellite if the Earth station antenna has a diameter of 2 m and an efficiency of $\eta = 0.65$ and the receiving antenna (at the satellite) has a gain of 45 dB.

Solution:

The gain of the transmitter antenna

$$\text{is } G_t = \frac{4\pi A_e}{\lambda^2}$$

$$\text{where } \lambda = \frac{c}{f} = \frac{3 \times 10^8}{10 \times 10^9} = 0.03 \text{ m}$$

$$A_e \equiv \left(\frac{D}{2}\right)^2 \pi \times \eta = \left(\frac{2}{2}\right)^2 \times \pi \times 0.65 = 2.04$$

$$G_t = \frac{4\pi A_e}{\lambda^2} = \frac{2.04 \times 4 \times \pi}{(0.03)^2} = 28484 = 44.55 \text{ dB}$$

$$P_t = 10 \log 50 \approx 17 \text{ dB W} = 47 \text{ dBm}$$

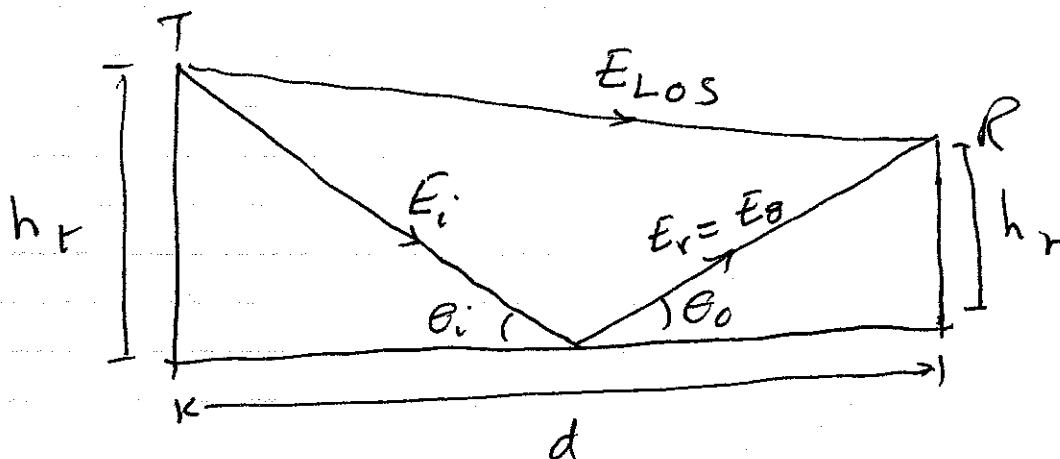
$$L_s = 10 \log \left(\frac{4\pi d}{\lambda}\right)^2 = 203.57$$

$$P_r(d) = P_t + G_t + G_r - L_s = 47 + 44.55 + 45 - 203.$$

$$P_r(d) = -67. \text{ dBm or } -\cancel{97} \text{ dBW}$$

Two-ray reflection model:

In this model in addition to LOS path, there is a ray reflected from ground



If the distance d , between transmitter and receiver is much larger than the product

of the antenna heights, i.e., if

$$d > \frac{20\pi h_t h_r}{3\lambda} \approx \frac{20 h_t h_r}{\lambda}$$

then the received signal power at a distance d is:

$$P_r(d) = \frac{P_t G_t G_r h_t^2 h_r^2}{d^4}$$

Example: A mobile transmit to a base station with a power 50 mW in 900 MHz. band.

The distance between the base station and the mobile is 10 km. The base station antenna is at a height of 20 m. and mobile's antenna is at a height of 1.5 m.

The mobile's antenna has a gain of 3 dB and base station's antenna has 10 dB gain. Find the power received at the base station.

Solution:

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{900 \times 10^6} = \frac{1}{3} \text{ m}$$

$$d = 10,000$$

$$\text{and } \frac{20 h_t h_r}{\lambda} = \frac{20 \times 20 \times 1.5}{1/3} = 1800$$

$$\text{So, } d > \frac{20 h_t h_r}{\lambda}$$

and

$$P_r(d) = \frac{P_t G_t G_r}{d^4} h_t^2 h_r^2$$

$$G_t = 3 \text{ dB} = 2$$

$$G_r = 10 \text{ dB} = 10$$

So

$$P_r(d) = \frac{50 \times 10^{-3} \times 2 \times 10}{(10,000)^4} \times (20)^2 (1.5)^2 = 9 \times 10^{-10}$$

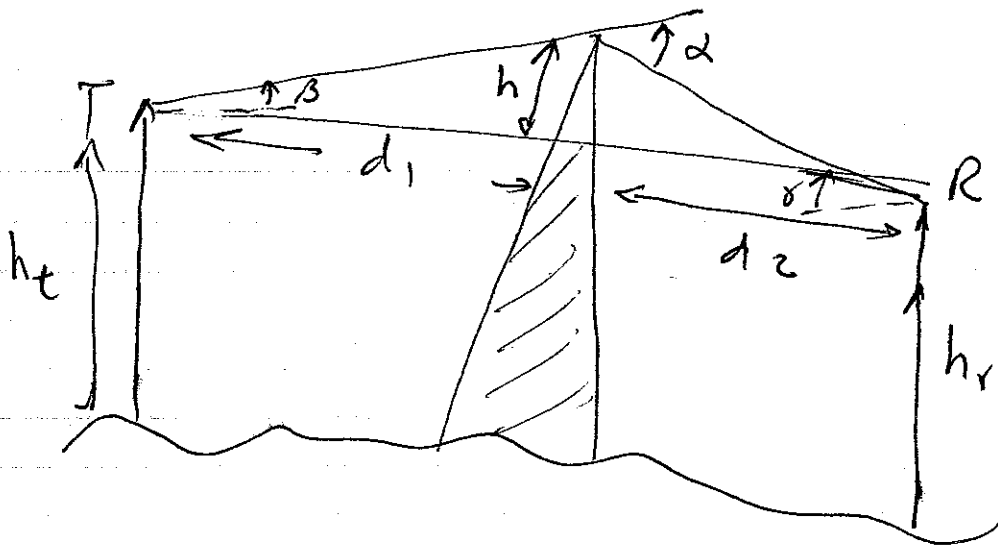
or

$$P_r(d) = -90.46 \text{ dBW} = -60.46 \text{ dBm.}$$

Fresnel Zone Geometry:

Another loss mechanism is diffraction

This happens when an obstacle, a hill, for example, stands between transmitter and receiver:



Assuming that $h \ll d_1$ and d_2 and $h \gg \lambda$
we have the excess path length as

$$\Delta \cong \frac{h^2}{2} \frac{(d_1 + d_2)}{d_1 d_2}$$

The phase difference between two paths is:

$$\phi = \frac{2\pi \Delta}{\lambda} \cong \frac{2\pi}{\lambda} \frac{h^2}{2} \frac{(d_1 + d_2)}{d_1 d_2}$$

Let $\Delta \cong \frac{h^2}{2} \frac{(d_1 + d_2)}{d_1 d_2}$

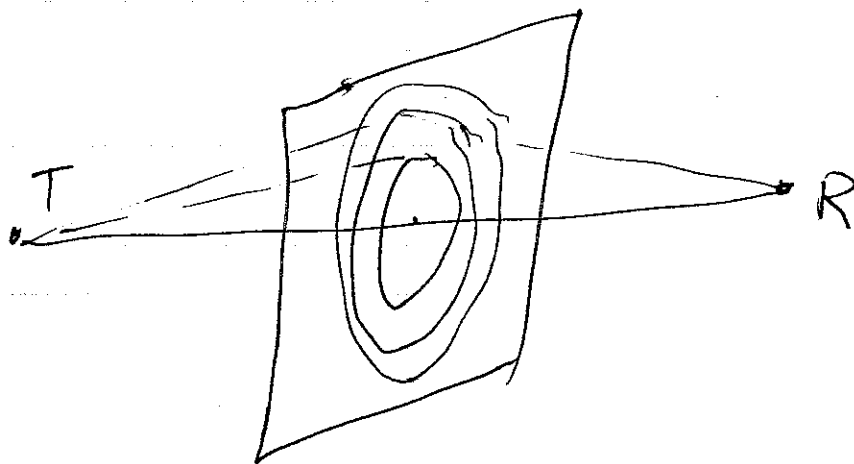
The parameter:

$$v = h \sqrt{\frac{2(d_1 + d_2)}{\lambda d_1 d_2}}$$

is called the Fresnel-Kirchhoff diffraction parameter. Then

$$\Phi = \frac{\pi}{2} v^2$$

Visualize having a screen between transmitter and receiver.



Fresnel zones represent regions where secondary wave has a phase difference of $n\pi$ ~~from~~ with the direct ray, or ~~phase~~ differ in length by $\frac{n\lambda}{2}$ from the primary path.

The radius of the n th Fresnel ~~zone~~ ^{circle is}

$$r_n = \sqrt{\frac{n \lambda d_1 d_2}{d_1 + d_2}}$$

^{Qn} The so called gain (in fact loss) is given as

$$G_d \text{ (dB)} = 20 \log |F(v)|$$

Where,

$$F(v) = \frac{E_d}{E_0} = \frac{1+j}{2} \int_0^{\infty} e^{-\frac{j\pi t^2}{2}} dt$$

G_d (dB) has been tabulated and also empirical formulas for it exist, e.g.,

$$G_d \text{ (dB)} = 0 \quad v \leq -1$$

$$G_d \text{ (dB)} = 20 \log (2.5 - 0.62 v) \quad -1 \leq v \leq 0$$

$$G_d \text{ (dB)} = 20 \log (0.5 \exp(-0.95 v)) \quad 0 \leq v \leq 1$$

$$G_d \text{ (dB)} = 20 \log (0.4 - \sqrt{0.1184 - (0.38 - 0.1v)^2}) \quad 1 \leq v \leq 2.4$$

$$G_d \text{ (dB)} = 20 \log \frac{0.225}{v} \quad v \geq 2.4$$

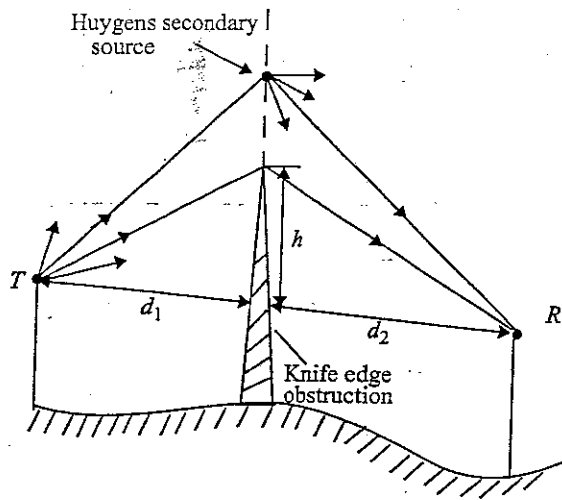


Figure 3.13
Illustration of knife-edge diffraction geometry. The receiver R is located in the shadow region.

The diffraction gain due to the presence of a knife edge, as compared to the free space E-field, is given by

$$G_d(\text{dB}) = 20\log|F(v)| \quad (3.60)$$

In practice, graphical or numerical solutions are relied upon to compute diffraction gain. A graphical representation of $G_d(\text{dB})$ as a function of v is given in Figure 3.14. An approximate solution for equation (3.60) provided by Lee [Lee85] as

$$\begin{aligned} G_d(\text{dB}) &= 0 & v \leq -1 \\ G_d(\text{dB}) &= 20\log(0.5 - 0.62v) & -1 \leq v \leq 0 \\ G_d(\text{dB}) &= 20\log(0.5 \exp(-0.95v)) & 0 \leq v \leq 1 \\ G_d(\text{dB}) &= 20\log\left(0.4 - \sqrt{0.1184 - (0.38 - 0.1v)^2}\right) & 1 \leq v \leq 2.4 \\ G_d(\text{dB}) &= 20\log\left(\frac{0.225}{v}\right) & v > 2.4 \end{aligned}$$

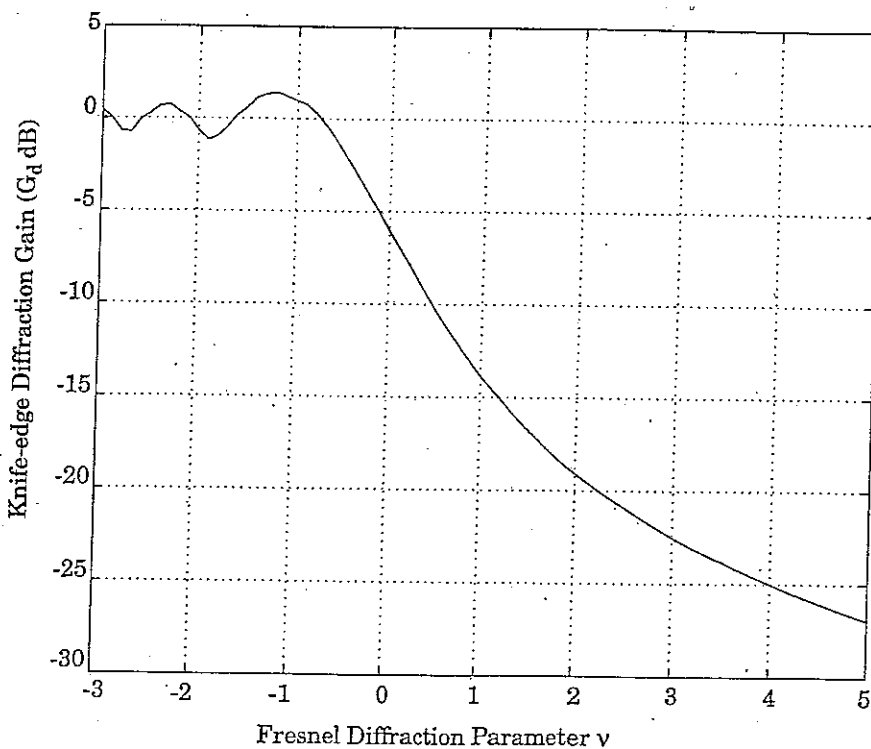


Figure 3.14
Knife-edge diffraction gain as a function of Fresnel diffraction parameter v .

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Example: For $\lambda = \frac{1}{3}$ m, $d_1 = 1$ km, $d_2 = 1$ km

and a) $h = 25$ m b) $h = 0$, c) $h = -25$ m

find the diffraction loss:

$$a) \quad v = h \sqrt{\frac{2(d_1 + d_2)}{\lambda d_1 d_2}} = 25 \sqrt{\frac{2(1000 + 1000)}{\frac{1}{3} \times 1000 \times 1000}} = 2.74$$

also specify the Fresnel zone where tip of obstruction

$$G_d(\text{dB}) = 20 \log\left(\frac{0.225}{v}\right) = -21.7 \text{ dB} \quad (21.7 \text{ dB loss})$$

from curve 22 dB

~~b) $h = 0$~~

$$\Delta \approx \frac{h^2}{2} \frac{(d_1 + d_2)}{d_1 d_2} = \frac{25^2}{2} \times \frac{1000 + 1000}{1000 \times 1000} = 0.625 \text{ m}$$

$$\Delta = n \frac{\lambda}{2} \quad \lambda = \frac{1}{3}$$

$$0.625 = n \times \frac{1}{6} \Rightarrow n = 3.75$$

So, tip of the obstruction obstructs first three (3) Fresnel zones.

$$b) \quad h = 0 \Rightarrow v = 0$$

$$G_d(\text{dB}) = 20 \log(0.5 - 0.62v) = 20 \log 0.5 \Rightarrow -6 \text{ dB}$$

$h = 0, \Delta = 0$ so, tip of obstruction is in the middle of 1st Fresnel zone

$$c) \quad h = -25 \Rightarrow v = -2.74$$

$$G_d(\text{dB}) = 0 \text{ dB} \quad (\text{from Graph } 1 \text{ dB})$$

Empirical Path Loss Models:

Log-distance Path Loss Model:

$$\overline{PL}(d) \propto \left(\frac{d}{d_0}\right)^n$$

or

$$\overline{PL}(dB) = \overline{PL}(d_0) + 10n \log\left(\frac{d}{d_0}\right)$$

Typical values of the path-loss exponent n :

Environment	Path Loss Exponent (n)
Free space	2
Urban Area Cellular	2.7 to 3.5
Shadowed Urban Area Cellular	3 to 5
In-building LOS	1.6 to 1.8
obstructed in building	4 to 6
obstructed in Factories	2 to 3

Log-normal shadowing:

$$PL(d)_{dB} = \overline{PL(d)} + X_\sigma = \overline{PL(d_0)} + 10 \log\left(\frac{d}{d_0}\right) + X_\sigma$$

and

$$P_r(d)_{dBm} = P_{t,dBm} - PL(d)_{dB} + G_t + G_r$$

X_σ is a zero-mean Normal (Gaussian) random variable.

Note: the deviation from mean in dB is

Normal, so, the name log-normal shadowing

$$P_r [P_r(d) > \gamma] = \int_{\gamma}^{\infty} p(x) dx$$

$$p(x) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left[-\frac{(x - \overline{P_r(d)})^2}{2\sigma^2}\right]$$

$$P_r [P_r(d) > \gamma] = \frac{1}{\sqrt{2\pi}\sigma} \int_{\gamma}^{\infty} \exp\left[-\frac{(x - \overline{P_r(d)})^2}{2\sigma^2}\right] dx$$

let $\frac{x - \overline{P_r(d)}}{\sigma} = u$

$$P_r [P_r(d) > \gamma] = \frac{1}{\sqrt{2\pi}} \int_{\frac{\gamma - \overline{P_r(d)}}{\sigma}}^{\infty} \exp \left[-\frac{u^2}{2} \right] du$$

$$P_r [P_r(d) > \gamma] = Q \left[\frac{\gamma - \overline{P_r(d)}}{\sigma} \right]$$

where

$$Q(y) = \frac{1}{\sqrt{2\pi}} \int_y^{\infty} e^{-u^2/2} du$$

The path loss exponent n and σ are found by curve fitting the measured data.

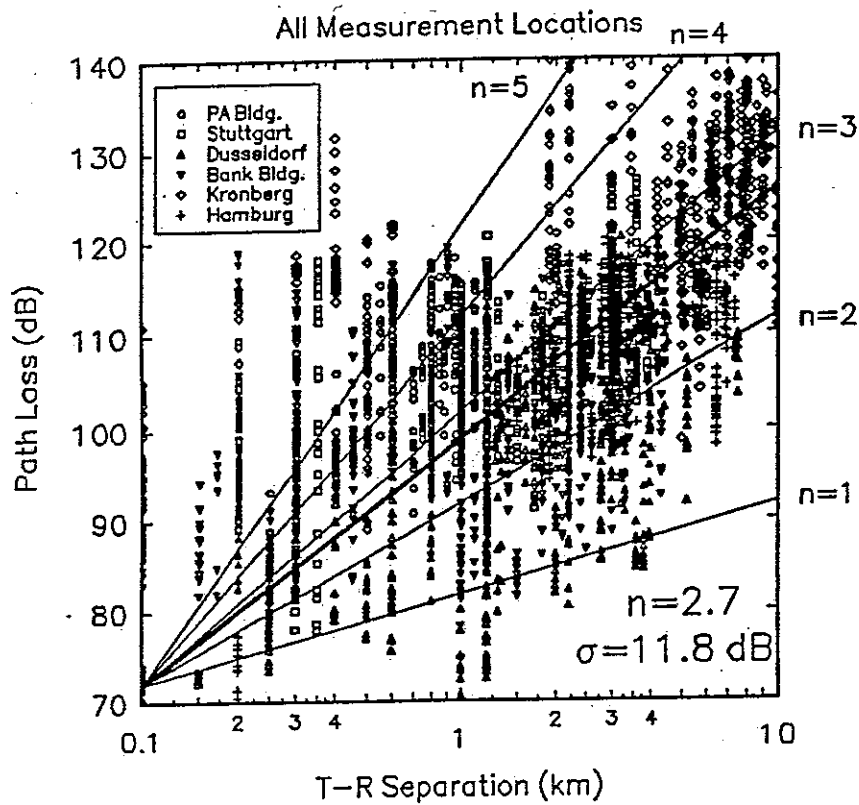


Figure 3.17
 Scatter plot of measured data and corresponding MMSE path loss model for many cities in Germany. For this data, $n = 2.7$ and $\sigma = 11.8$ dB [From [Sei91] © IEEE].

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