

Q1.

$$I_0 = \mu C_0 \times \frac{W}{2L} (V_{GS} - V_{TH})^2$$

$$= 100 \times 10^6 \times \frac{10}{2} \cdot (V_{GS} - 0.5)^2 = 100 \times 10^6$$

$$\hookrightarrow 5 (V_{GS} - 0.5)^2 = 1 \quad ; \quad (V_{GS} - 0.5)^2 = 0.2$$

$$V_{GS} - 0.5 = \sqrt{0.2} = \pm 0.447$$

$$V_{GS} = 0.947 \quad (\text{acceptable})$$

$$r \because > V_{TH}$$

$$V_{GS} = V_G - V_S = V_G + 5 = 0.947$$

$$\hookrightarrow V_G = -4.05 \text{ V.}$$

Since $I_{ref} = I_0$, MOS being identical

$$= 100 \mu A = \frac{V_{DD} - V_G}{R} = \frac{5 + 4.05}{R}$$

$$R = \frac{9.05}{100 \mu A} = 90.5 \text{ k}\Omega$$

← design value (Ans.)

Q2.

$$I_0 = I_{REF} \frac{1}{1 + \frac{n+1}{\beta}}$$

'n' not given
let $n = 1$

$$I_{REF} - I_0 = I_{REF} \left[1 - \left(\frac{1}{1 + \frac{n+1}{\beta}} \right) \right]$$

$$= I_{REF} \left[\frac{1 + \frac{n+1}{\beta} - 1}{1 + \frac{n+1}{\beta}} \right] = I_{REF} \cdot \frac{n+1}{\beta + n+1}$$

$$\frac{I_{REF} - I_0}{I_{REF}} = \frac{n+1}{\beta + n+1}$$

this should be $< 5\%$

Q2

$$S_0 \frac{n+1}{\beta + n+1} < .05, \beta > \frac{(n+1)(1-.05)}{.05}$$

If n=1, $\frac{2}{\beta+2} < .05$

$\beta > 19(n+1)$

p2/4

$$.05\beta + 0.1 > 2 \quad ; \quad .05\beta > 1.9$$

$$\beta > \frac{1.9}{.05} = 38$$

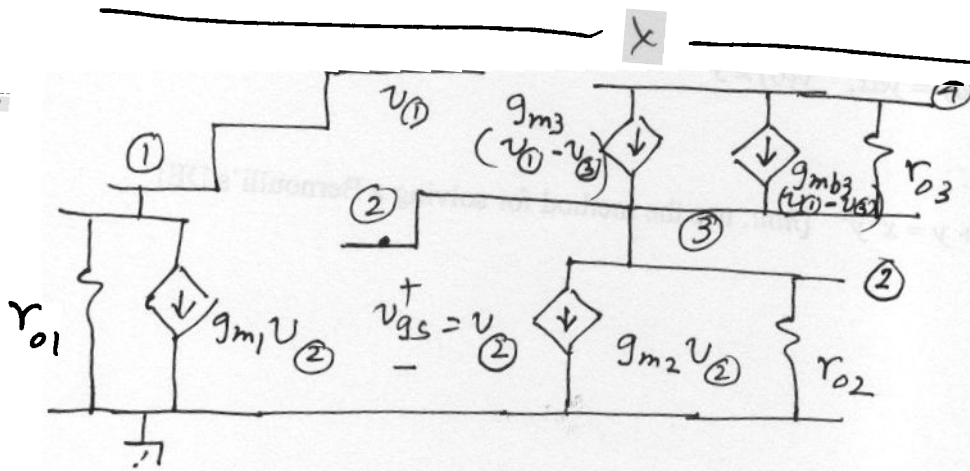
If n=2,

$$\frac{3}{\beta+3} < .05$$

$$.05\beta + .15 > 3 \quad ; \quad .05\beta > 2.85$$

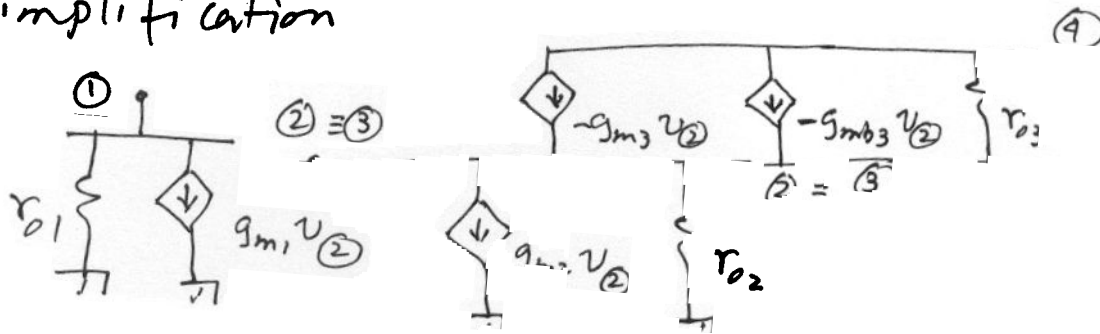
$$\beta > 57$$

Q3:



note:
 $v_3 \equiv v_2$

$\therefore I_{REF}$ is DC no 'ac' current at node 1
So we can take $v_1 = 0$. for further simplification



Q4:

We need to use degenerating resistors in series with each emitter arm.

P3/4

With R_E as this resistance,

$$R_{in} = 2(\beta+1)(R_E+r_e)$$

The voltage drop $2V_{be}$ is across $2(\beta+1)r_e$ component

$$\text{So } 2(\beta+1)r_e < 6 \text{ mV (rms)}$$

$$\text{or } (\beta+1)r_e < 3 \text{ mV.}$$

For given problem, the total drop across $2(\beta+1)(R_E+r_e)$ is 50 mV

$$\text{i.e. } (\beta+1)(R_E+r_e) = 25 \text{ mV.}$$

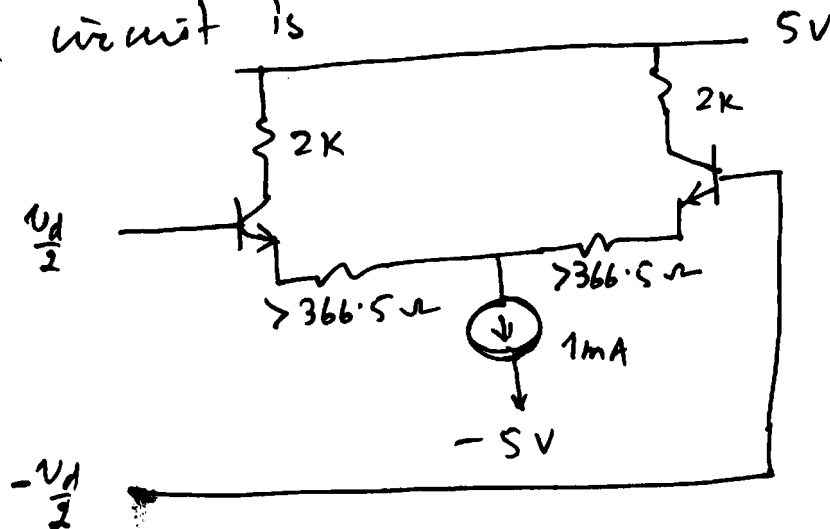
Taking the ratio $\frac{R_E+r_e}{r_e} > \frac{25 \text{ mV}}{3 \text{ mV}} \rightarrow 8.33$

$$R_E > (8.33 - 1)r_e \rightarrow 7.33 r_e$$

$$r_e \approx \frac{V_T}{I_E} = \frac{25 \text{ mV}}{0.5 \text{ mA}} = 50 \Omega$$

$$\text{So } R_E > 7.33 \times 50 \rightarrow 366.5 \Omega \rightarrow 390 \Omega \text{ a practical value}$$

Modified circuit is



Q.5: With active load, the differential gain is $-g_m \cdot (r_{o1} \parallel r_{o2})$

p414

Where $r_{o1} = \frac{V_{AN}}{I_{CN}}$; $r_{o2} = \frac{V_{AP}}{I_{CP}}$

For the circuit $I_{CN} = I_{CP} \approx \frac{I_{EE}}{2} = 1\text{mA}$

So $r_{o1} = \frac{25}{1\text{mA}} = 25\text{K}\Omega$; $r_{o2} = \frac{50}{1\text{mA}} = 50\text{K}\Omega$

$g_m \approx \frac{I_E}{V_T} = \frac{1\text{mA}}{25\text{mV}} = 0.04\text{mA/V}$. Note: $I_E \approx I_{CN} \approx I_{CP}$

So voltage gain = $-0.04 \times (50\text{K}\Omega \parallel 25\text{K}\Omega)$
 $= -0.04 \times 16.67\text{K}\Omega = -666.67\text{V/V}$

Gain $\approx -666.67\text{V/V}$