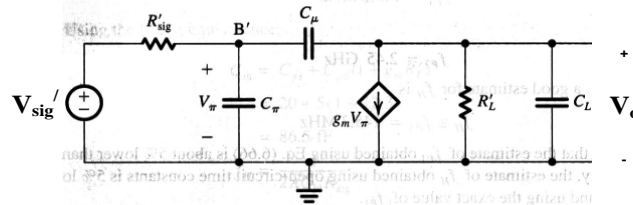


**ELEC 312: ELECTRONICS – II : ASSIGNMENT set 2**  
**Department of Electrical and Computer Engineering**  
**Fall 2012**

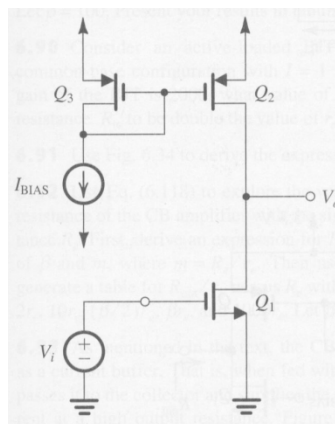
1. A common-emitter amplifier that can be represented by the following equivalent circuit, has  $C_\pi = 10$  pF,  $C_\mu = 0.5$  pF,  $C_L = 2$  pF,  $g_m = 20$  mA/V,  $\beta = 100$ ,  $r_x = 200$   $\Omega$ ,  $R_L' = 5$  k $\Omega$  and  $R_{sig} = 1$  k $\Omega$ . Find (i) the mid band gain  $A_M$ , (ii) the frequency of the zero  $f_Z$ , and (iii) the approximate values of the pole frequencies  $f_{P1}$  and  $f_{P2}$ . Hence estimate the 3-dB frequency  $f_H$ . Note that  $R'_{sig}$  is the equivalent Thevenin resistance looking towards the signal source and includes the effects of  $R_{sig}$ ,  $r_x$  and  $r_\pi$ . For approximate estimates, you may use OCTC method.



**Hints:**

- (i)  $A_M = -r_\pi(g_m R'_L)/(R_{sig} + r_x + r_\pi)$ ; (ii)  $f_Z = g_m/(2\pi C_\mu)$  (iii)  $f_{P1} = 1/[2\pi\{(C_\pi + C_\mu(1 + g_m R'_L))R'_{sig} + (C_L + C_\mu)R'_L\}]$ ;  $f_{P2} = [(C_\pi + C_\mu(1 + g_m R'_L))R'_{sig} + (C_L + C_\mu)R'_L]/[2\pi\{C_\pi(C_L + C_\mu) + C_L C_\mu\}]R'_{sig}R'_L$ ;  $f_{P1} \ll f_{P2}$  &  $f_{P1} \ll f_Z$ , hence  $f_H \approx f_{P1}$
2. Analyze the high-frequency response of the CMOS amplifier shown below. The dc bias current is 100  $\mu$ A. For  $Q_1$ ,  $\mu_n C_{ox} = 90$   $\mu$ A/V<sup>2</sup>,  $V_A = 12.8$  V,  $W/L = 100$   $\mu$ m/1.6  $\mu$ m,  $C_{gs} = 0.2$  pF,  $C_{gd} = 0.015$  pF. For  $Q_2$ ,  $C_{gd} = 0.015$  pF,  $C_{gs} = 36$  fF and  $|V_A| = 19.2$  V. Assume that the resistance of the input signal generator is negligibly small. Also, for simplicity assume that the signal voltage at the gate of  $Q_2$  is zero. Find the low-frequency (i.e., at DC) gain, the frequency of the pole, and the frequency of the zero. You may use nodal analysis.

Note: fF=10<sup>-15</sup> F, pF=10<sup>-12</sup> F.



**Hints:**

DC gain =  $-g_m(r_{01} // r_{02})$ , where  $g_m = \sqrt{2\mu_n C_{ox} I_D W/L}$ ,  $r_0 = V_A / I_D$  and  
 Small-signal gain,  $v_o / v_i = (g_m - sC_{gd1}) / [1 / r_{01} + 1 / r_{02} + s(C_L + C_{gd1})]$  where  $C_L = C_{gd2}$   
 $f_z = g_m / (2\pi C_{gd1})$ ;  $f_p = (1/2\pi) [ (1 / r_{01} + 1 / r_{02}) / (C_L + C_{gd1}) ]$

3. A CG amplifier is specified to have  $C_{gs} = 2$  pF,  $C_{gd} = 0.1$  pF,  $C_L = 2$  pF,  $g_m = 5$  mA/V,  $\chi = 0.2$ ,  $R_{sig} = 1$  k $\Omega$  and  $R_L' = 20$  k $\Omega$ . Neglecting the effects of  $r_o$ , find the low-frequency gain  $v_o / v_{sig}$ , the frequencies of the poles  $f_{p1}$  and  $f_{p2}$  and hence an estimate of the 3-dB frequency  $f_H$ . For a CG amplifier you can use  $g_{mb} = \chi g_m$ . Use ac equivalent circuit.

**Hints:**

From the small-signal equivalent circuit,

$v_o / v_i = [ \{ 1 / (g_m + g_{mb}) \} / \{ R_S + 1 / (g_m + g_{mb}) \} ] (g_m + g_{mb}) R'_L$ ;  $f_{p1} = 1 / [ 2\pi C_{gs} \{ R_{sig} // (1 / (g_m + g_{mb})) \} ]$ ;  
 $f_{p2} = 1 / [ 2\pi (C_{gd} + C_L) R'_L ]$ .  $f_{p2} \ll f_{p1}$ ,  $f_{p2}$  is the dominant pole and  $f_H \approx f_{p2}$

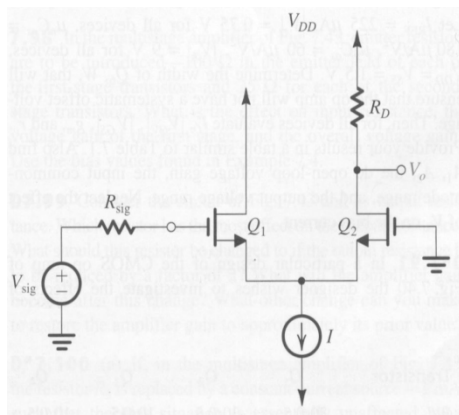
4. (a) Consider a CS amplifier having  $C_{gd} = 0.2$  pF,  $R_{sig} = R_L = 20$  k $\Omega$ ,  $g_m = 5$  mA/V,  $C_{gs} = 2$  pF,  $C_L$  (including  $C_{db}$ ) = 1 pF, and  $r_o = 20$  k $\Omega$ . Find (i) the low-frequency gain  $A_M$ , and (ii) estimate  $f_H$  using open-circuit time constants.

Hence determine the gain-bandwidth (GBW = mid-freq. gain *times*  $f_H$ ).

**Hints:**

$A_M = g_m R'_L$ ;  $f_H = 1 / (2\pi\tau_H)$  where  $\tau_H = C_{gs}R_{gs} + C_{gd}R_{gd} + C_L R'_L$ ,  $R_{gs} = R_{sig}$ ,  $R_{gd} = R_{sig}(1 + g_m R'_L) + R'_L$ ;  $GBW = |A_M|f_H$

5. Consider the following circuit for the case:  $I = 200$   $\mu$ A and  $V_{OV} = 0.25$  V,  $R_{sig} = 200$  k $\Omega$ ,  $R_D = 50$  k $\Omega$ ,  $C_{gs} = C_{gd} = 1$  Pf (for both transistors). Find the dc (i.e., low-frequency) gain, the high-frequency poles, and an estimate of  $f_H$ . (hint: need to find  $g_m$  from  $I$  and  $V_{OV}$  data!).

**Hints:**

$V_{G1} = V_S \cdot [ (2/g_m) / ((2/g_m) + R_S) ]$ ,  $I = V_{G1} / (2/g_m)$ ,  $V_O = IR_D$  hence,  $A_O = V_O / V_S = g_m R_D / (2 + g_m R_S)$ ;  $f_{p1} = 1 / [ 2\pi R_S (C_{gs} / 2 + C_{gd}) ]$ ;  $f_{p2} = 1 / (2\pi R_D C_{gd})$



6.

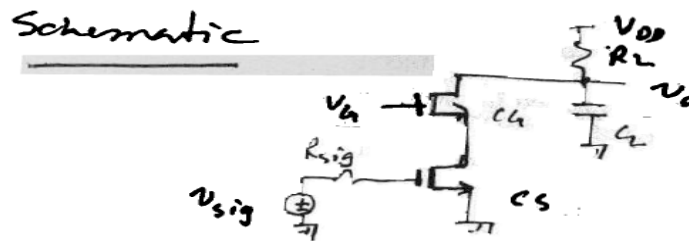
(a) Consider a CS stage having  $C_{gd} = 0.2 \text{ pF}$ ,  $R_{sig} = 20 \text{ k}\Omega$ ,  $g_m = 5 \text{ mA/V}$ ,  $C_{gs} = 2 \text{ pF}$ , and  $r_o = 20 \text{ k}\Omega$ .

(b) A CG stage is connected in totem-pole configuration with the CS transistor in (a) to create a cascode amplifier. The ac parameters of this stage are identical with those of the CS stage. Regarding the body-effect in the CG stage assume  $\chi = 0.2$ . Further  $R_L = 20 \text{ k}\Omega$ , and is shunted by a load capacitance  $C_L = 1 \text{ pF}$ . Show a schematic diagram of the system using NMOS transistors. Show the ac equivalent circuit.

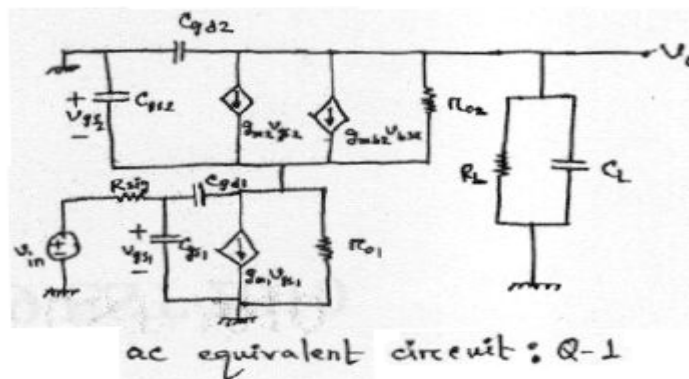
Find (i) the low-frequency gain  $A_M$ , and (ii) estimate the gain-bandwidth of the system. You may use OCTC method to determine the dominant high frequency pole  $f_H$  of the system.

Hints:

For the cascade amplifier:



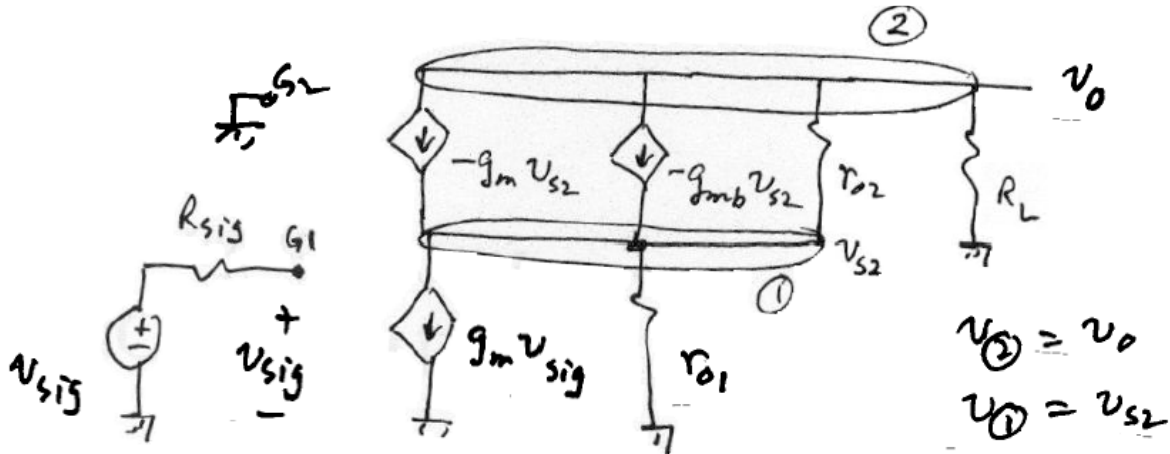
AC Equivalent circuit:



$$V_{gs2} = V_g - V_{s2} = 0 - V_{s2}$$

$$V_{bs2} = V_b - V_{s2} = 0 - V_{s2}$$

For low frequency gain, ignore all  $C_{gs}$  and  $C_{gd}$



Consider the 2- node system and derive  $V_o/V_{sig}$

$$\begin{bmatrix} g_{01} + g_{02} & -g_{02} \\ -g_{02} & g_{02} + g_2 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} -g_m v_{sig} - (g_m + g_{mb})v_1 \\ (g_m + g_{mb})v_1 \end{bmatrix}$$

$$\frac{v_o}{v_{sig}} = - \frac{g_m (g_m + g_{mb} + g_0)}{(g_m + g_{mb})g_L + g_0(g_0 + 2g_L)}$$

Here  $g_{01} = g_{02} = g_0 = \frac{1}{r_0}$

Using the values:  $\frac{v_o}{v_{sig}} \approx - 98.37$  v/v

For Dominant pole calculation, note:

For  $C_{gd1}$ , the Miller effect amplifications are :

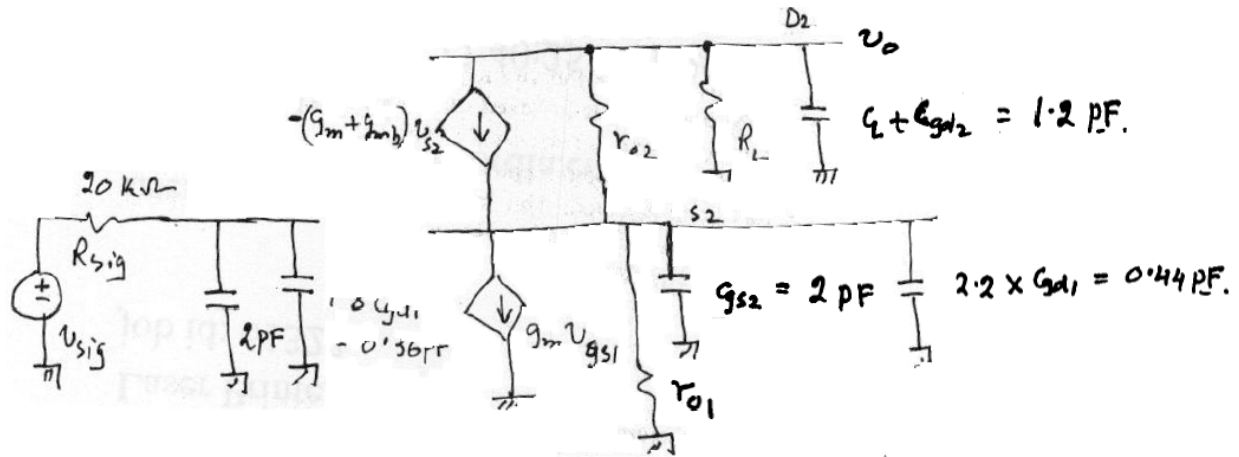
i) At input  $(1 + K_1) C_{gd1}$ ,  $K_1 = \frac{g_m}{g_m + g_{mb}} = \frac{1}{1.2} = 0.8$

ii) At input  $(1 + \frac{1}{k_1}) C_{gd1} = (1 + 1.2) C_{gd1}$



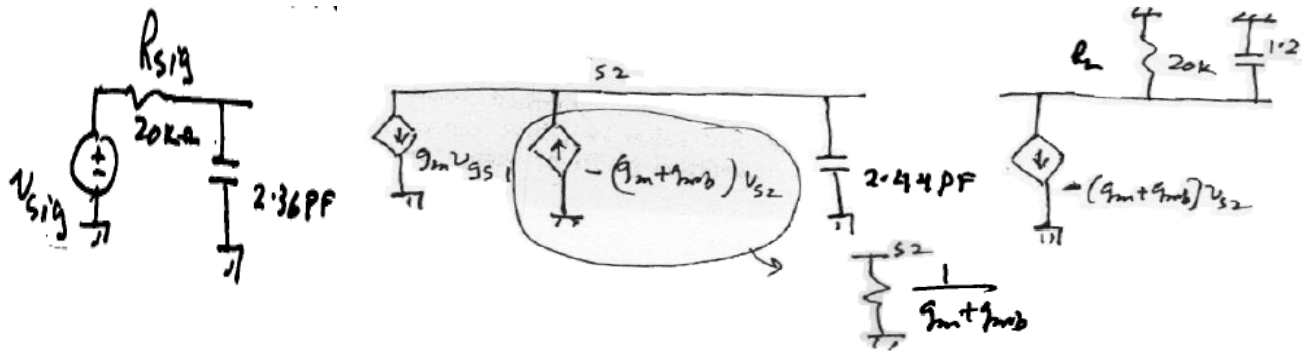
$C_{gd2}$  does not have miller effect

**So the AC equivalent circuit is**



Ignoring  $r_{o1}$  and  $r_{o2}$  as was done in the class lecture.

**CE-CB Cascade**



The time constants are:

$$\tau_1 = 2.36 \times 10^{-12} \times 20 \times 10^3 = 4.72 \times 10^{-8} \text{ sec}$$

$$\tau_2 = \frac{2.44 \times 10^{-12}}{1.2 \times 10^{-3}} = 4.07 \times 10^{-10} \text{ sec}$$

$$\tau_3 = 1.2 \times 10^{-12} \times 20 \times 10^3 \text{ sec}$$

$\tau_1, \tau_3$  are close enough, so dominant time constant principle may not apply



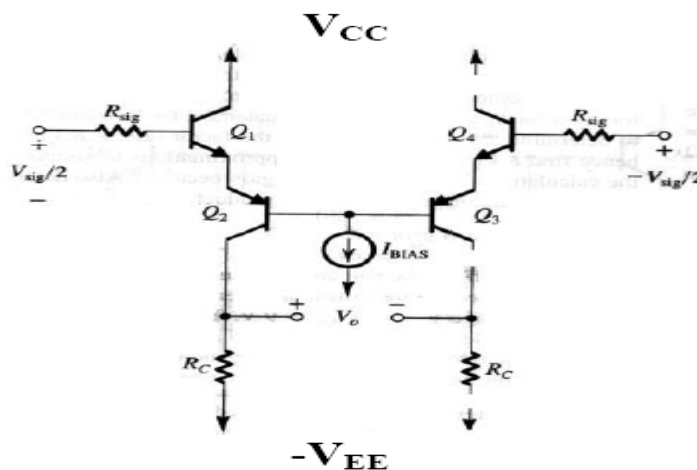
We will take  $\tau_H = \tau_1 + \tau_2 + \tau_3 = f_H = \frac{1}{2\pi} \frac{1}{7.161 \times 10^{-8}} = 2.22 \text{ MHz}$

$$\text{GBW} = |-98.37| \times 2.2 \times 10^6 = 218.6 \text{ MHz}$$

7. For the following circuit, let the bias be such that each transistor is operating at  $100\text{-}\mu\text{A}$  collector current. Let the BJTs have  $h_{fe} = 200$ ,  $f_T = 600 \text{ MHz}$ , and  $C_\mu = 0.2 \text{ pF}$ , and neglect  $r_o$  and  $r_x$ . Also,  $R_{sig} = RC = 50 \text{ k}\Omega$ .

Show the ac equivalent circuit.

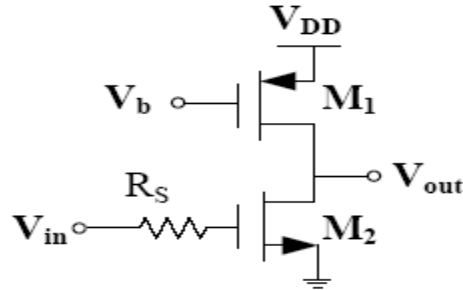
Find (i) the low-frequency gain, (ii) the high-frequency poles, and (iii) an estimate of the dominant high frequency pole  $f_H$  of the system. Now find the GBW (gain-bandwidth) of the system. You may use half-circuit technique.



**Hints:**

- (i)  $A_o = \alpha R_C / [(R_{sig}/(\beta+1)) + 2r_c]$ ; where  $\beta = h_{fe}$  (ii)  $f_{p1} = 1/[2\pi(R_{sig} || 2r_\pi)(C_\pi/2 + C_\mu)]$ ;  $f_{p2} = 1/[2\pi R_C C_\mu]$ ; where  $2\pi f_T = g_m/(C_\pi + C_\mu)$ , calculate  $C_\pi$  from here. (iii)  $f_H = \sqrt{[(1/f_{p1})^2 + (1/f_{p2})^2]}$ ; (iv)  $\text{GBW} = |A_o|f_H$

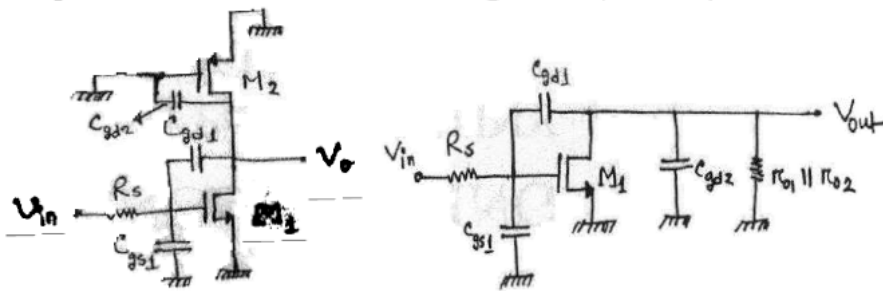
8. In the following circuit assume both transistors operate in saturation and  $\lambda \neq 0$ . For each transistor you can assume the parasitic capacitances as  $C_{gsi}$ ,  $C_{gdi}$ , ( $i=1,2$ ).



Draw the *ac* equivalent circuit, analyze and derive the expression for the dominant pole frequency.

**Hints:**

Simplified circuit models for small signal analysis are given below:



Analyzing the small signal equivalent circuit we get,

$$\omega_{P1} = 1 / [ \{ 1 + g_{m1}(r_{o1} || r_{o2}) \} C_{gd1} R_S + R_S C_{gs1} + (r_{o1} || r_{o2}) ( C_{gd1} + C_{gd2} ) ]$$

$$\omega_{P2} = [ \{ 1 + g_{m1}(r_{o1} || r_{o2}) \} C_{gd1} R_S + R_S C_{gs1} + (r_{o1} || r_{o2}) ( C_{gd1} + C_{gd2} ) ] / [ R_S (r_{o1} || r_{o2}) ( C_{gs1} C_{gd1} + C_{gd2} C_{gd1} + C_{gs1} C_{gd2} ) ]$$

