

ELEC 312: ELECTRONICS – II : ASSIGNMENT-5
Department of Electrical and Computer Engineering
Winter – 2012

Solution: 9.97

All V_{ov} are the same, all V_A are the same
 All r_o are identical and all g_m 's are identical

$$\text{We know } A_d(s) = g_m R_0 \left[\frac{1 + \frac{s \cdot C_m}{2 g_m r_o}}{1 + \frac{s \cdot C_m}{g_m r_o}} \right] \cdot \left(\frac{1}{1 + s C_L R_0} \right)$$

We also know that the frequencies of the zero f_z and the pole f_{p2} occur at very high frequencies. Thus we can assume that the pole $f_{p1} = 1 / (2\pi C_L R_0)$ dominates the response of $A_d(s)$ passed the unity gain

Thus:

$$A_d(s) = g_m R_0 \left(\frac{1}{1 + j\omega C_L R_0} \right);$$

At unity gain $|A_d(\omega_1)| = 1$

$$\Rightarrow 1 = \frac{g_m R_0}{\sqrt{1 + (\omega_1 C_L R_0)^2}}$$

$$\Rightarrow \omega_1^2 = \frac{(g_m R_0)^2 - 1}{(C_L R_0)^2}$$

$$\text{since } g_m R_0 = g_m \frac{r_o}{2} \gg 1 \Rightarrow \omega_1 \approx g_m / C_L$$

$$\Rightarrow f_1 = \frac{g_m}{2\pi \cdot C_L}$$

For $V_A = 20 \text{ V}$, $V_{ov} = 0.2 \text{ V}$,

$I = 0.2 \text{ mA}$, $C_L = 100 \text{ fF}$, $C_m = 25 \text{ fF}$

All r_o are identical:

$$r_o = \frac{V_A}{I_D} = \frac{20 \text{ V}}{\frac{0.2 \text{ mA}}{2}} = 200 \text{ k}\Omega$$

$$\text{All } g_m \text{ are identical : } g_m = \frac{2 I_D}{V_{ov}} = \frac{0.2 \text{ mA}}{0.2} = \frac{1 \text{ mA}}{\text{V}}$$

The low frequency differential gain is :

$$A_{dDC} = g_m \frac{r_o}{2} = 100 \text{ V/V}$$

$$f_{p1} = \frac{1}{2\pi \cdot C_L R_0} = 15.9 \text{ MHz}$$

$$f_{p2} = \frac{g_m}{2\pi \cdot C_m} = 6.37 \text{ GHz}$$

$$f_Z = \frac{2g_m}{2\pi \cdot C_m} = 2 \times f_{p2} = 12.74 \text{ GHz}$$

Solution: 9.105

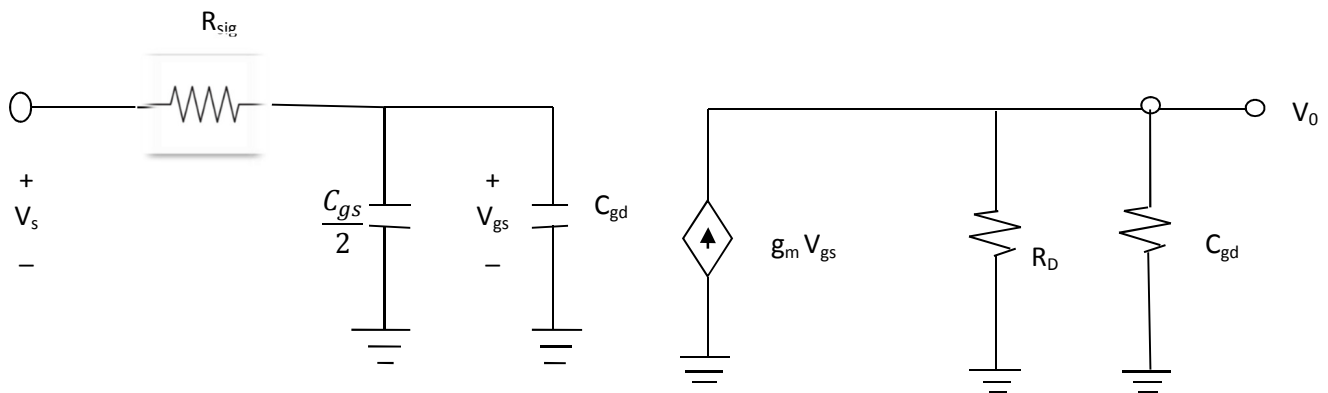
$$V_{G1} = \frac{V_s \cdot \frac{2}{g_m}}{\frac{2}{g_m} + R_{sig}} \quad \text{and} \quad I = \frac{V_{G1}}{\frac{2}{g_m}}$$

$$V_0 = I R_D = \frac{V_s \cdot R_D}{\frac{2}{g_m} + R_{sig}}$$

$$A_0 = \frac{V_0}{V_s} = \frac{g_m \cdot R_D}{2 + g_m R_{sig}}$$

$$g_m = \frac{200 \mu A}{0.2 V} = 1 \text{ mA} \quad \text{so} \quad A_0 = 247.5 \text{ V/V}$$

The high frequency equivalent circuit is:



Thus the pole at the input has a frequency $f_{p1} = \frac{1}{2\pi \cdot R_{sig} \left(\frac{C_{gs}}{2} + C_{gd}\right)} = 350 \text{ KHz}$

and the pole at the output has a frequency $f_{p2} = \frac{1}{2\pi \cdot R_D \cdot C_{gd}} = 3.18 \text{ MHz}$

$$\text{Thus } f_H = \frac{1}{\sqrt{\left(\frac{1}{f_{p1}}\right)^2 + \left(\frac{1}{f_{p2}}\right)^2}} = 52$$

ELEC 312: ELECTRONICS – II : ASSIGNMENT-6
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1. A series-series feedback circuit represented by Fig.1, and using an ideal transconductance amplifier operates with $V_s = 100$ mV, $V_f = 95$ mV, and $I_o = 10$ mA. What are the corresponding values of A and β ? Include the correct units for each.

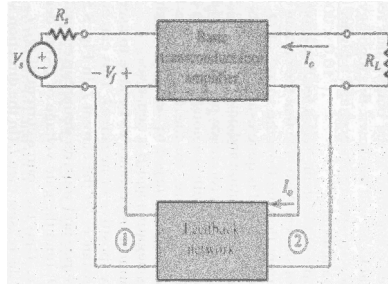


Figure 1:

Hints:

$$V_1 = V_s - V_f; V_f = \beta I_o \text{ hence, } \beta = V_f / I_o; A = I_o / V_1; A_F = I_o / V_s = A / (1 + A \beta).$$

2. For an amplifier connected in a negative feedback loop in which the output voltage is sampled (i.e., a shunt connection), measurement of the output resistance before and after the loop is connected shows a change by a factor of 80. Is the resistance with feedback higher or lower? What is the value of the loop gain $A\beta$? If R_{of} is 100Ω , what is R_o without feedback?

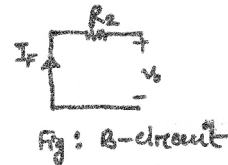
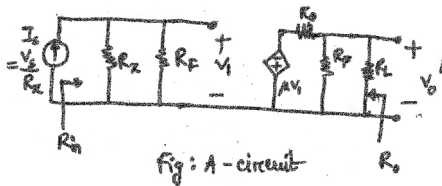
Hints:

$$R_o \text{ is lowered by amount of feedback i.e. } (1 + A \beta) = 80; A\beta = 79, R_o = R_{of} (1 + A \beta)$$

3. The shunt-shunt feedback amplifier in the Figure 3 has $I = 1$ mA and $V_{GS} = 0.8$ V. The MOSFET has $V_t = 0.6$ V and $V_A = 30$ V. For $R_S = 10$ k Ω , $R_1 = 1$ M Ω , and $R_2 = 4.7$ M Ω , find the voltage gain v_o/v_s , the input resistance R_{in} and the output resistance R_{out} . You need to figure out the *ac* parameters for the MOS device.

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Figure 3:

Hints:

$$\underline{g_m = 2I_D/V_{OV} \text{ and } r_o = V_A/I,}$$

Shunt-shunt feedback. We use Y-parameter model for the feedback circuit.

Find y_{11} , y_{22} , y_{12} for R_1 , R_2 . Remember $\beta = y_{12}$.

Draw loaded ac equivalent circuit. Use $R_{11}(=1/y_{11})$ in shunt at input, $R_{22}(=1/y_{22})$ in shunt at output..

$$\beta = I_F/V_o = -1/R_2, \text{ Let } R_x = R_s + R_1 \text{ and } \mu = g_m r_o, A = V_o'/I_s' = -[R_x \parallel R_2][R_2 \parallel r_o]g_m;$$

$$A_F = V_o/I_s = A/(1+A\beta),$$

$$\text{Thus } V_o/(I_s R_x) = V_o/V_1 = 1/(\beta R_x) = -R_2/(R_1 + R_s)$$

$$R_i' = (R_s + R_1) \parallel R_2; R_{if} = R_i'/(1+A\beta), R_{in} = R_{if} - R_s$$

$$R_o' = R_2 \parallel r_o, R_{of} = R_o'/(1+A\beta)$$

4. An op amp having a low-frequency gain of 10^3 and a single-pole transfer function with -3dB frequency of 10^4 rad/s is connected in a negative feedback loop via a feedback network having a transmission $\beta(s)$ given by $\beta(s) = \frac{\beta_o}{(1 + s/10^4)^2}$. Find the value of β_o above which the closed-loop amplifier becomes unstable.

Hints:

$$A(s) = \frac{10^3}{1 + s/10^4}, \beta(s) = \frac{\beta_o}{(1 + s/10^4)^2}$$

$$\text{Ang}(A\beta) = -\tan^{-1}(\omega/10^4) - 2\tan^{-1}(\omega/10^4) = 3\tan^{-1}(\omega/10^4)$$

For 180° , $\omega_{180} = \sqrt{3} \times 10^4$; for $|A\beta(\omega_{180})| < 1$, Determine condition for β_o

5. A DC amplifier has an open-loop gain of 1000 and two poles, a dominant one at 1 kHz and a high-frequency one whose location can be controlled. It is required to connect this amplifier in a negative feedback loop that provides a dc closed-loop gain of 100 and a maximally flat response. The transfer function of the amplifier can be modeled as:

$$A(s) = \frac{1000}{(1 + s/\omega_1)(1 + s/\omega_2)}$$

In the above ω_1 is the dominant pole frequency. It is required that under feedback, the amplifier will have a maximally flat response according to the model

$$A_f(s) = \frac{1000\omega_1\omega_2}{s^2 + (\omega_p/Q_p)s + \omega_p^2}, \text{ with } Q_p = 0.707.$$

Calculate the required ω_2 .

Hints:

$$A(s) = \frac{1000}{(1 + s/\omega_1)(1 + s/\omega_2)};$$

$A_f(0) = 10^3/(1+10^3\beta) = 100$, calculate β .

Formulate the $A_f(s)$ under feedback, and concentrate on the denominator polynomial $D(s)$ in the form

$$s^2 + (\omega_p/Q_p)s + (\omega_p)^2$$

Compare it with

$$s^2 + s(\omega_1 + \omega_2) + (1 + A_o\beta)\omega_1\omega_2 = 0$$

$Q_p = \sqrt{[(1 + A_o\beta)\omega_1\omega_2]/(\omega_1 + \omega_2)}$, calculate ω_2 Where, $Q_p = 0.707$ and $\omega_1 = 2\pi \times 1000$ rad