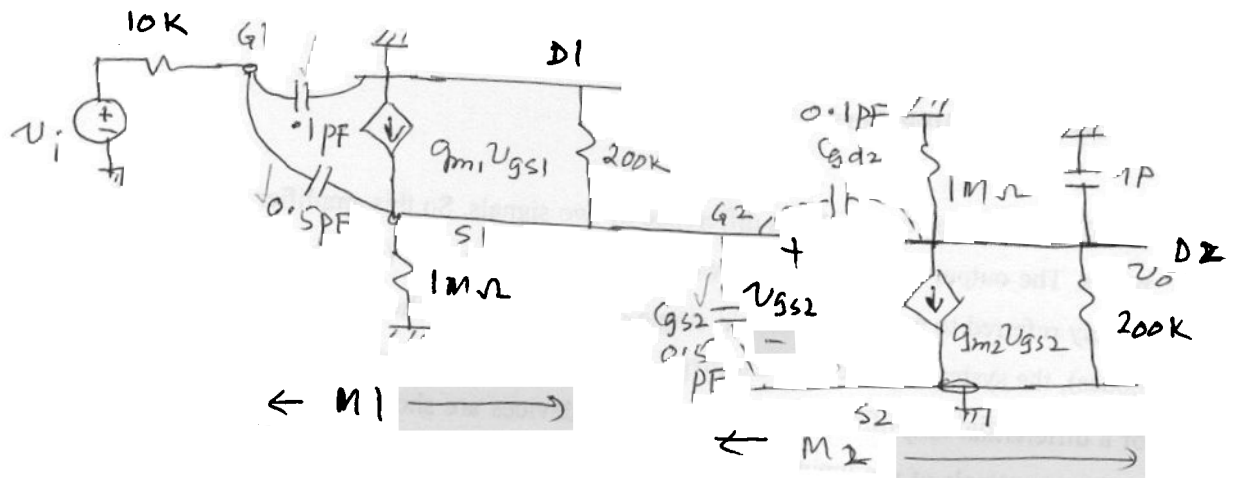


3-8.7
(Contd.)

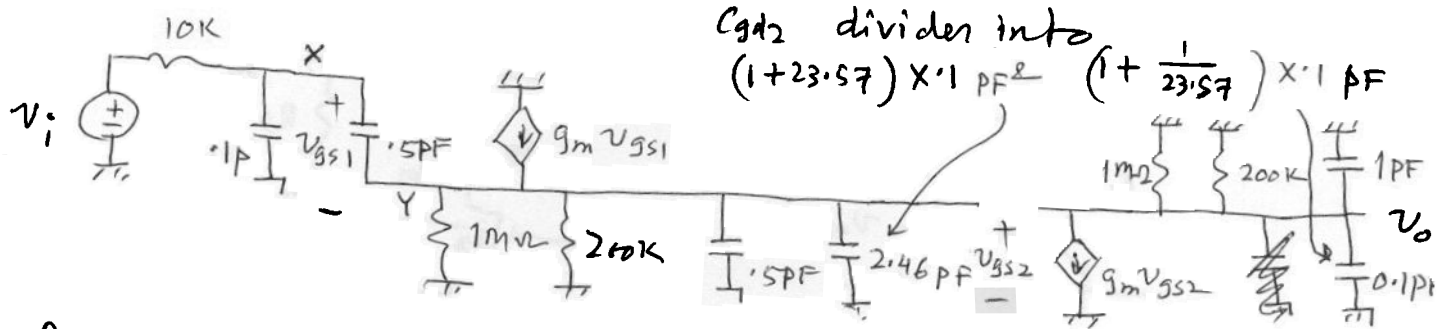


For M_2 we apply Miller's Theorem

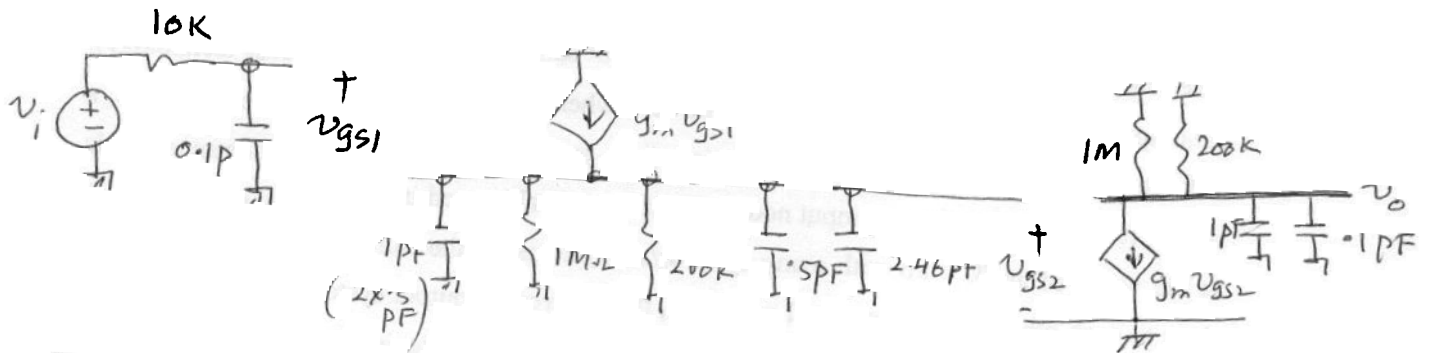
The gain = $-1411.4 \times 10^6 \times 166.7K = -23.57$

$$(-g_{m2}R_D) = -1411.4 \times 10^{-6} \times (1M\Omega \parallel 200K)$$

So



Between nodes X and Y, the CD amplifier has a voltage gain of ≈ 1 . We can apply Miller's Theorem to convert further



There are three time constants involved

For the 0.1 PF cap the time constant is $0.1 \times 10^{-12} \times 10K = T_1$

For the $(1PF + 0.5PF + 2.46PF)$ cap., the time constant is

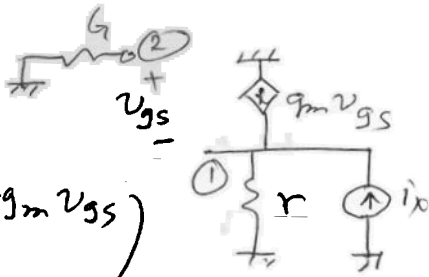
$$T_2 = \frac{3.96 \times 10^{-12} \times (1M\Omega \parallel 200K)}{1 + g_m \cdot (1M\Omega \parallel 200K)} \quad \text{where } g_m = 1411.4 \mu V$$

3.8.7

proof for τ_3

By nodal matrix

$$\begin{pmatrix} g & 0 \\ 0 & g \end{pmatrix} \begin{pmatrix} v_{(1)} \\ v_{(2)} \end{pmatrix} = \begin{pmatrix} i_x + g_m v_{gs} \\ 0 \end{pmatrix}$$



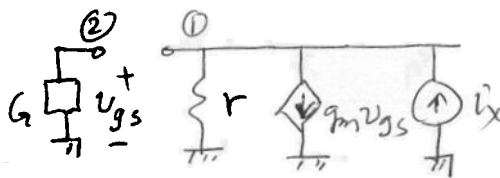
$$R_{TH} = \frac{v_{(1)}}{i_x}$$

But $v_{gs} = v_{(2)} - v_{(1)}$. So

$$\begin{pmatrix} g_m + g & -g_m \\ 0 & g \end{pmatrix} \begin{pmatrix} v_{(1)} \\ v_{(2)} \end{pmatrix} = \begin{pmatrix} i_x \\ 0 \end{pmatrix}$$

Solving for $\frac{v_{(1)}}{i_x} \rightarrow \frac{1}{g + g_m} = \frac{r}{1 + g_m r} = R_{TH}$

Similarly for



$$\begin{pmatrix} g & 0 \\ 0 & g \end{pmatrix} \begin{pmatrix} v_{(1)} \\ v_{(2)} \end{pmatrix} = \begin{pmatrix} i_x - g_m v_{gs} \\ 0 \end{pmatrix}$$

but $v_{gs} = v_{(2)}$ now

So

$$\begin{pmatrix} g & g_m \\ 0 & g \end{pmatrix} \begin{pmatrix} v_{(1)} \\ v_{(2)} \end{pmatrix} = \begin{pmatrix} i_x \\ 0 \end{pmatrix}$$

$$\frac{v_{(1)}}{i_x} = \frac{1}{g} = r = R_{TH}$$

(note $v_{gs2} \rightarrow v_g - v_{s2} \rightarrow 0 - 0 \rightarrow 0$; so $g_m v_{gs2} \rightarrow 0$, open circuit current source)

So the time constant τ_3 for the (1pF + 0.1pF) cap. is

$$= 1.1 \times 10^{-12} \times (1M\Omega || 200k)$$

Calculate τ_1, τ_2, τ_3 , then $\omega_H \approx \frac{1}{\tau_1 + \tau_2 + \tau_3}$ rad/sec

3.8.8
(Contd.)

$$\begin{bmatrix} g_s & 0 & 0 \\ g_m & g_m + 2g_{o1} & -g_{o1} \\ 0 & -g_m - g_{o1} & g_{o1} + g_{o2} \end{bmatrix} \begin{bmatrix} v_1 \\ v_x \\ v_o \end{bmatrix} = \begin{bmatrix} i_s \\ 0 \\ 0 \end{bmatrix}$$

$$v_x = \begin{bmatrix} g_s & i_s & 0 \\ g_m & 0 & -g_{o1} \\ 0 & 0 & g_{o1} + g_{o2} \end{bmatrix} \frac{1}{\Delta}$$

$$v_1 = \begin{bmatrix} i_s & 0 & 0 \\ 0 & g_m + 2g_{o1} & -g_{o1} \\ 0 & -g_m - g_{o1} & g_{o1} + g_{o2} \end{bmatrix} \frac{1}{\Delta}$$

$$\frac{v_x}{v_1} = -4.809$$

whx

$$g_m = 141.4 \mu S$$

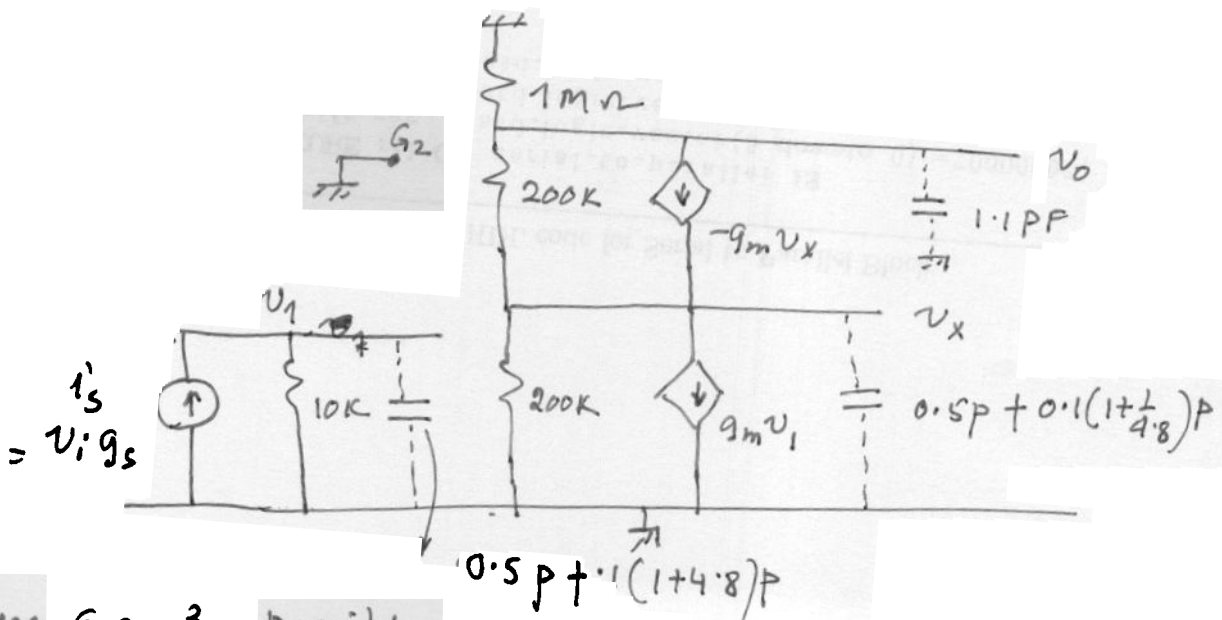
$$g_{o1} = \frac{1}{200k\Omega}$$

$$g_{o2} = \frac{1}{1M\Omega}$$

$$g_s = \frac{1}{10k\Omega}$$

So Miller gain is -4.8 .

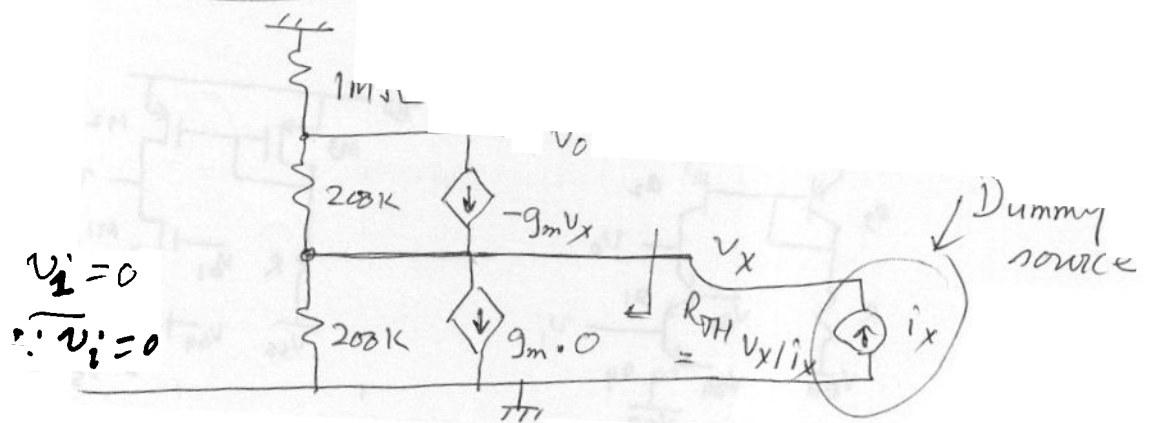
Modified ac equivalent circuit is



There are 3 possible O.C.T.C values at nodes v_1, v_x, v_o respectively

3.8.8
(Contd.)

For v_x node



Let $g_{o1} = \frac{1}{200k}$; $g_{o2} = \frac{1}{1M\Omega}$

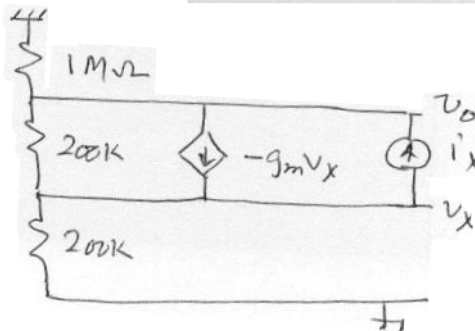
$$\begin{pmatrix} g_{o1} + g_{o1} & -g_{o1} \\ -g_{o1} & g_{o1} + g_{o2} \end{pmatrix} \begin{pmatrix} v_x \\ v_0 \end{pmatrix} = \begin{pmatrix} i_x - g_m v_x \\ g_m v_x \end{pmatrix}$$

$$\begin{pmatrix} g_m + g_{o1} + g_{o1} & -g_{o1} \\ -g_{o1} - g_m & g_{o1} + g_{o2} \end{pmatrix} \begin{pmatrix} v_x \\ v_0 \end{pmatrix} = \begin{pmatrix} i_x \\ 0 \end{pmatrix}$$

$$v_x = \begin{vmatrix} i_x & -g_{o1} \\ 0 & g_{o1} + g_{o2} \end{vmatrix} / \begin{vmatrix} g_m + g_{o1} + g_{o1} & -g_{o1} \\ -g_m - g_{o1} & g_{o1} + g_{o2} \end{vmatrix}$$

$$R_{THx} = \frac{v_x}{i_x} = \frac{g_{o1} + g_{o2}}{g_m + g_{o1} + g_{o1} - \frac{g_{o1}^2}{g_{o1} + g_{o2}}} \approx 34013 \Omega \rightarrow$$

Next for v_0 node, the measurement set up changes to



$$R_{TH0} = \frac{v_0 - v_x}{i_x}$$

3.8.8.
(contd.)

The NAM changes to

$$\begin{bmatrix} 2g_{o1} & -g_{o1} \\ -g_{o1} & g_{o1} + g_{o2} \end{bmatrix} \begin{bmatrix} v_x \\ v_o \end{bmatrix} = \begin{bmatrix} -i_x - g_m v_x \\ i_x + g_m v_x \end{bmatrix}$$

$$\begin{bmatrix} g_m + 2g_{o1} & -g_{o1} \\ -g_m - g_{o1} & g_{o1} + g_{o2} \end{bmatrix} \begin{bmatrix} v_x \\ v_o \end{bmatrix} = \begin{bmatrix} -i_x \\ i_x \end{bmatrix}$$

Let $\Delta = \begin{vmatrix} g_m + 2g_{o1} & -g_{o1} \\ -g_m - g_{o1} & g_{o1} + g_{o2} \end{vmatrix} = 0.1764 \times 10^{-9}$

$$v_o = \frac{1}{\Delta} \begin{vmatrix} g_m + 2g_{o1} & -i_x \\ -g_m - g_{o1} & i_x \end{vmatrix} = \frac{1}{\Delta} \cdot i_x = \frac{5 \times 10^{-5}}{\Delta} i_x$$

$$v_x = \frac{1}{\Delta} \begin{vmatrix} -i_x & -g_{o1} \\ i_x & g_{o1} + g_{o2} \end{vmatrix} = \frac{1}{\Delta} \cdot i_x = -0.1 \times 10^{-5} \frac{i_x}{\Delta}$$

$$\begin{aligned} \text{So } v_o - v_x &= \frac{0.6 \times 10^{-5}}{\Delta} i_x ; \quad \frac{v_o - v_x}{i_x} = R_{TH0} = \frac{0.6 \times 10^{-5}}{\Delta} \\ &= 3403.6 \Omega \end{aligned}$$

It appears that both R_{THx} & R_{TH0} are about equal

Time constant at v_x node

$$= 3403 \times \left[0.5 + 1 \left(1 + \frac{1}{4.8} \right) \right] \times 10^{-12} = \cancel{10.5 \times 10^{-8} \text{ sec.}} \\ = 2.11 \times 10^{-8} \text{ sec.}$$

Time constant at v_o node

$$= 3403 \times 1.1 \times 10^{-12} = 3.74 \times 10^{-8}$$

~~$f_H \approx \frac{1}{3.74 \times 10^{-8} + 2.11 \times 10^{-8}} = \frac{1}{5.85 \times 10^{-8}} = 1.71 \times 10^7 \text{ Hz} = 17.1 \text{ MHz}$~~

~~$f_H \approx \frac{1}{2.11 \times 10^{-8}} = 4.74 \times 10^7 \text{ Hz} = 47.4 \text{ MHz}$~~

~~$f_H \approx \frac{1}{3.74 \times 10^{-8}} = 2.67 \times 10^7 \text{ Hz} = 26.7 \text{ MHz}$~~

3.8.6
(contd.)

Time constant at v_1 node

$$= 10k \times (5 + 5.8 \times 1) p$$

$$= 10.8 \times 10^9 \text{ sec}$$

$$\text{Then } \omega_H \approx \frac{1}{2.11 \times 10^{-8} + 3.74 \times 10^{-8} + 10.8 \times 10^9} = 14.43 \times 10^6$$

$$f_H = \frac{\omega_H}{2\pi} = 2.297 \text{ MHz}$$