

# **APPENDICES**

## Appendix A

**A.1:** Coefficients of denominator polynomial, in the form  $s^n + a_1s^{n-1} + a_2s^{n-2} + \dots + a_{n-2}s^2 + a_{n-1}s + 1$ , for Butterworth filter function of order  $n$ , with pass-band from 0 to 1 rad/sec<sup>+</sup>.

$n$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$	$a_6$
2	1.4142					
3	2.0000	2.0000				
4	2.6131	3.4142	2.6131			
5	3.2361	5.2361	5.2361	3.2361		
6	3.8637	7.4641	9.1416	7.4641	3.8637	
7	4.4940	10.0978	14.5918	14.5918	10.0978	4.4940

**A.2:** Coefficients of denominator polynomial, in the form  $s^n + a_1s^{n-1} + a_2s^{n-2} + \dots + a_{n-2}s^2 + a_{n-1}s + a_n$ , for Chebyshev filter function of order  $n$ , with pass-band from 0 to 1 rad/sec<sup>+</sup>.

Pass-band ripple $A_p$	$n$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$	$a_6$
$\epsilon=0.3493$	1	2.863					
	2	1.425	1.516				
	3	1.253	1.535	0.716			
	4	1.197	1.717	1.025	0.379		
	5	1.1725	1.9374	1.3096	0.7525	0.1789	
	6	1.1592	2.1718	1.5898	1.1719	0.4324	0.0948
$\epsilon=0.5089$	1	1.965					
	2	1.098	1.103				
	3	0.988	1.238	0.491			
	4	0.953	1.454	0.743	0.276		
	5	0.9368	1.6888	0.9744	0.5805	0.1228	
	6	0.9282	1.9308	1.2021	0.9393	0.3071	0.0689
$\epsilon=0.7648$	1	1.308					
	2	0.804	0.637				
	3	0.738	1.022	0.327			
	4	0.716	1.256	0.517	0.206		
	5	0.7065	1.4995	0.6935	0.4593	0.0817	
	6	0.7012	1.7459	0.8670	0.7715	0.2103	0.0514

**A.3:** Coefficients of denominator polynomial, in the form  $s^n + a_1s^{n-1} + a_2s^{n-2} + \dots + a_{n-2}s^2 + a_{n-1}s + a_n$ , for Bessel-Thomson filter function of order  $n^+$ .

$n$	$a_1$	$a_2$	$a_3$	$a_4$	$a_5$	$a_6$
1	1					
2	3	3				
3	6	15	15			
4	10	45	105	105		
5	15	105	420	945	945	
6	21	210	1260	4725	10395	10395

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<sup>+</sup> R. Schaumann et al, "Design of Analog Filters- Passive, Active RC, and Switched Capacitor", Prentice-Hall Inc., © 1990

## Appendix B

**B.1:** Element interconnections and values for *all-pole* low-pass single-resistance-terminated lossless ladder. Figures B.1(a)-(b) are the structures for voltage source driven with even and odd order filters respectively. Figures B.1(c)-(d) are for current source driven with even and odd order filters respectively.<sup>1</sup> The element values for several orders are given in **TABLE B.1**.

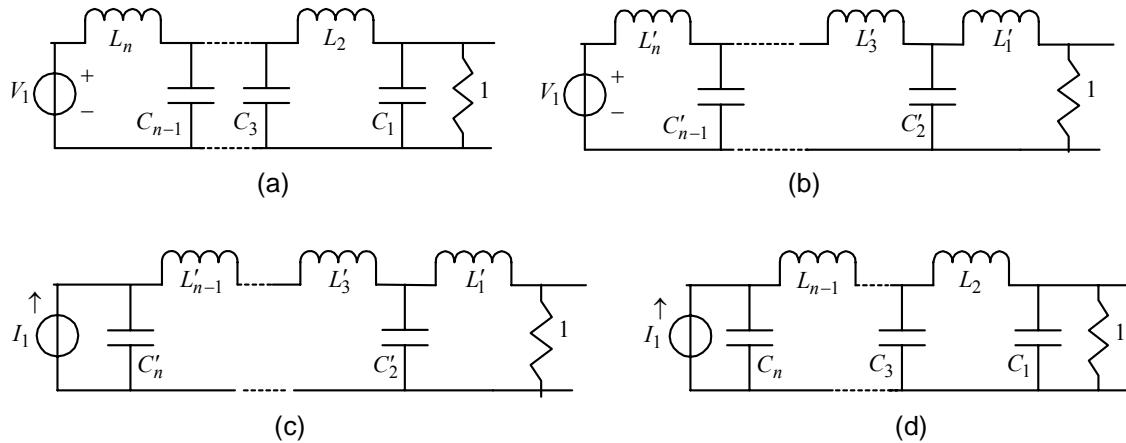


Figure B.1:

**TABLE B.1**

n	C <sub>1</sub>	L <sub>2</sub>	C <sub>3</sub>	L <sub>4</sub>	C <sub>5</sub>	L <sub>6</sub>	C <sub>7</sub>
2	.7071	1.4142	<b>Butterworth</b>	(1 rad/s bandwidth)			
3	.5000	1.3333	1.5000				
4	.3827	1.0824	1.5772	1.5307			
5	.3090	.8944	1.3820	1.6944	1.5451		
2	.7014	.9403	<b>0.5 dB ripple</b>	<b>Chebyshev</b>			
3	.7981	1.3001	1.3465	(1 rad/s bandwidth)			
4	.8352	1.3916	1.7279	1.3138			
5	.8529	1.4291	1.8142	1.6426	1.5388		
2	.9110	.9957	<b>1 dB ripple</b>	<b>Chebyshev</b>			
3	1.0118	1.3332	1.5088	(1 rad/s bandwidth)			
4	1.0495	1.4126	1.9093	1.2817			
5	1.0674	1.4441	1.9938	1.5908	1.6652		
2	.3333	1.0000		<b>Bessel-Thomson</b>			
3	.1667	.4800	.8333	(1 s delay at DC)			
4	.1000	.2899	.4627	.7101			
5	.0667	.1948	.3103	.4215	.6231		
6	.0476	.1400	.2246	.3005	.3821	.5595	
7	.0357	.1055	.1704	.2288	.2827	.3487	.5111
n	L <sub>1'</sub>	C <sub>2'</sub>	L <sub>3'</sub>	C <sub>4'</sub>	L <sub>5'</sub>	C <sub>6'</sub>	L <sub>7'</sub>

<sup>1</sup> L.P.Huelsman, "Active and Passive Analog Filter Design – An Introduction", McGraw-Hill, Inc., ©1993.

**B.2:** Element interconnections and values for *all-pole* low-pass double-resistance-terminated lossless ladder. Figures B.2(a)-(b) are the structures for even and odd order filters respectively. Figures B.2(c)-(d) are alternate structures for even and odd order filters respectively.<sup>!</sup> The element values for several orders are given in **TABLE B.2**.

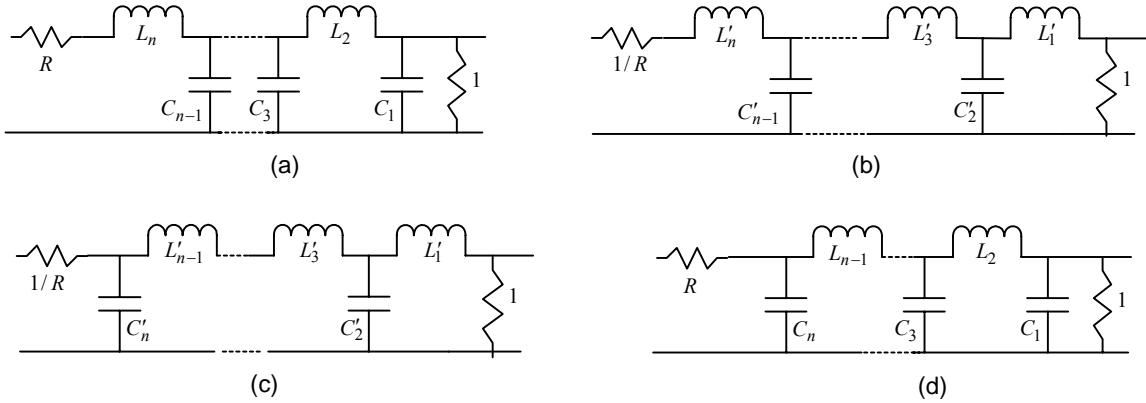


Figure B.2:

**TABLE B.2**

n	$C_1$	$L_2$	$C_3$	$L_4$	$C_5$	$L_6$	$C_7$
2	1.4142	1.4142	<b>Butterworth</b>	(1 rad/s bandwidth)			
3	1.0000	2.0000	1.0000				
4	.7654	1.8478	1.8478	.7654			
5	.6180	1.6180	2.0000	1.6180	.6180		
3	1.5963	1.0967	1.5963	<b>0.5 dB ripple</b>	<b>Chebyshev</b>	(1 rad/s bandwidth)	
5	1.7058	1.2296	2.5408	1.2296	1.7058		
7	1.7373	1.2582	2.6383	1.3443	2.6383	1.2582	1.7373
3	2.0236	.9941	2.0236	<b>1 dB ripple</b>	<b>Chebyshev</b>	(1 rad/s bandwidth)	
5	2.1349	1.0911	3.0009	1.0911	2.1349		
7	2.1666	1.1115	3.0936	1.1735	3.0936	1.1115	2.1666
2	1.5774	.4226		<b>Bessel-Thomson</b>			
3	1.2550	.5528	.1922	(1 s delay at DC)			
4	1.0598	.5116	.3181	.1104			
5	.9303	.4577	.3312	.2090	.0718		
6	.8377	.4116	.3158	.2364	.1480	.0505	
7	.7677	.3744	.2944	.2378	.1778	.1104	.0375
n	$L'_1$	$C'_2$	$L'_3$	$C'_4$	$L'_5$	$C'_6$	$L'_7$

<sup>!</sup> L.P.Huelsman, "Active and Passive Analog Filter Design – An Introduction", McGraw-Hill, Inc., ©1993.

**B.3:** Element values for *elliptic* low-pass double-resistance-terminated lossless ladder. Figures in B.3(a) show the structures for even and odd order filters respectively. Figures in B.3(b) are alternate structures for even and odd order filters respectively.<sup>1</sup>

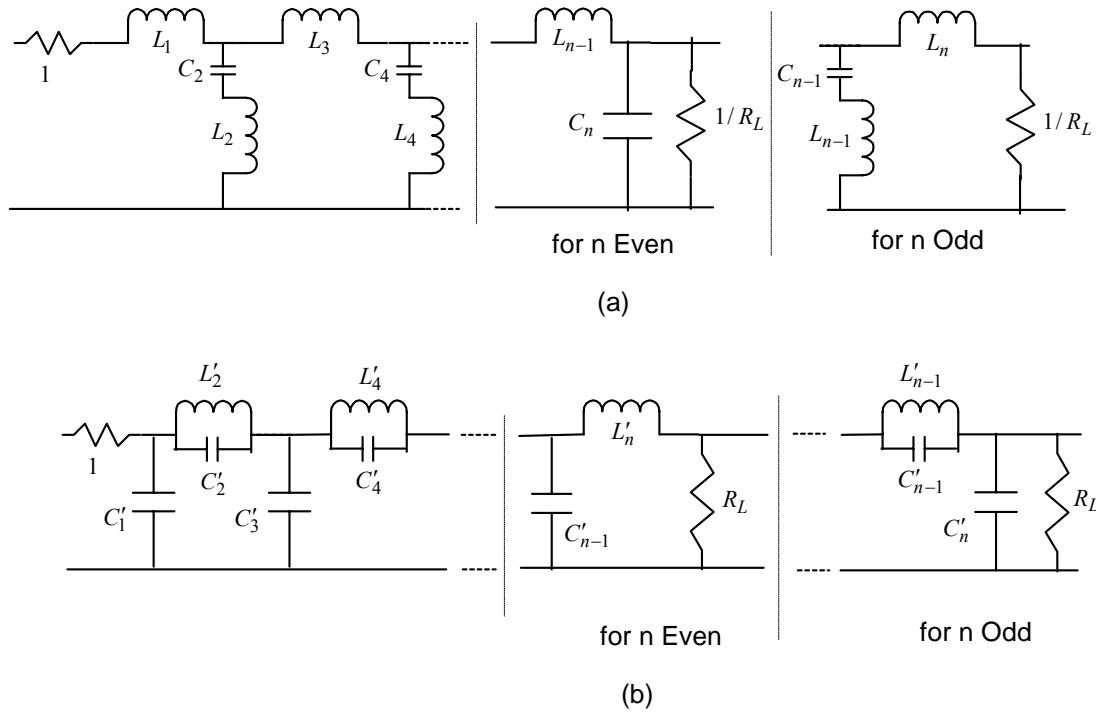


Figure B.3:

**TABLE B.3A** provide element values for odd orders of several values and also for several even order values for the case when the response at infinite frequency is forced to zero by adopting a modified expression for the transfer function. In this transfer function the denominator is of degree  $n$  while the numerator degree is forced to be  $n-2$ . The expression has the form:

$$H_N(s) = \frac{H_c \prod_{i=2}^{n/2} (s^2 + \Omega_i^2)}{a_0 + a_1 s + \dots + a_{n-1} s + a_n s^n} \quad \dots \text{ (B.3.1)}$$

In this case the load and source resistances are equal with a value of  $1\Omega$  each. **TABLE B.3B** provide alternate set of element values for several even orders, where the modified elliptic transfer function has the same form as in Eq. B.3.1 above, but the values of the  $\Omega_i$  are slightly different. As a result the transition band slope becomes different. The nature of difference for order  $n=4$  may be appreciated by considering figures B.4(a)-(b). The difference lies in the magnitude of the transfer function at DC (zero frequency). This is similar to the case of even and odd order Chebyshev approximation functions. The source and load resistances for this alternate case, are unequal with  $R_s = 1 \Omega$ . In each of these tables only two values have been used for  $A_p$ , i.e., .1 dB and 1.0 dB.

<sup>1</sup> L.P.Huelsman, "Active and Passive Analog Filter Design – An Introduction", McGraw-Hill, Inc., ©1993.

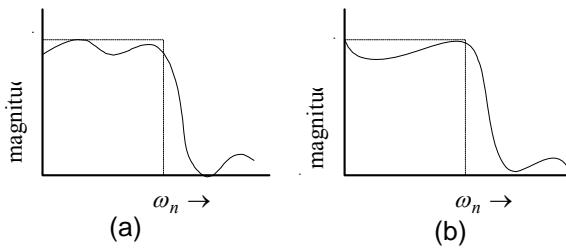


Figure B.4:

TABLE B.3A

$n$	$\omega_s$	$A_a$	$L_1$	$C_2$	$L_2$	$L_3$	$C_4$	$L_4$	$L_5$	(see Fig. B.3(a))
3	1.05	1.748	.35550	.15374	5.39596	.35550				
	1.10	3.374	.44626	.26993	2.70353	.44626				
	1.20	6.691	.57336	.44980	1.30805	.57336				
	1.50	14.848	.77031	.74561	.47797	.77031				
	2.00	24.010	.89544	.93759	.20697	.89544				0.1-dB passband ripple
4	1.05	3.284	.00442	.17221	4.93764	1.01224	.84445			
	1.10	6.478	.17279	.32758	2.30986	1.04894	.89415			
	1.20	12.085	.37139	.56638	1.09294	1.11938	.92440			
	1.50	23.736	.62815	.94009	.40730	1.24711	.93518			
	2.00	36.023	.77554	1.17646	.17957	1.33473	.93382			
5	1.05	13.841	.70813	.76630	.73572	1.12761	.20138	4.38116	.04985	
	1.10	20.050	.81296	.92418	.49338	1.22445	.37193	2.13500	.29125	
	1.20	28.303	.91441	1.06516	.31628	1.38201	.60131	1.09329	.52974	
	1.50	43.415	1.02789	1.21517	.15134	1.63179	.93525	.44083	.81549	
	2.00	58.901	1.08758	1.29322	.07317	1.79387	1.14330	.20038	.97720	
3	1.05	8.134	1.05507	.25223	3.28904	1.05507				
	1.10	11.480	1.22525	.37471	1.94752	1.22525				
	1.20	16.209	1.42450	.52544	1.11977	1.42450				
	1.50	25.176	1.69200	.73340	.48592	1.69200				
	2.00	34.454	1.85199	.85903	.22590	1.85199				
4	1.05	11.322	.63708	.35277	2.41039	1.11522	1.39953			
	1.10	15.942	.80935	.54042	1.40015	1.18107	1.45001			
	1.20	22.293	1.00329	.77733	.79634	1.26621	1.49217			
	1.50	34.179	1.25675	1.11431	.34362	1.38981	1.53225			
	2.00	46.481	1.40677	1.32367	.15960	1.46762	1.55071			
5	1.05	24.135	1.56191	.67560	.83449	1.55460	.26584	3.31881	.88528	
	1.10	30.471	1.69691	.77511	.58827	1.79892	.39922	1.98907	1.12109	
	1.20	38.757	1.82812	.87005	.38720	2.09095	.56347	1.16672	1.38094	
	1.50	53.875	1.97687	.97694	.18824	2.49161	.79362	.51950	1.71889	
	2.00	69.360	2.05594	1.03392	.09152	2.73567	.93561	.24486	1.91939	
$n$	$\omega_s$	$A_a$	$C_1'$	$L_2'$	$C_2'$	$C_3'$	$L_4'$	$C_4'$	$C_5'$	(see Fig. B.3(b))

**TABLE B.3B**

<i>n</i>	$\omega_s$	$A_a$	$L_1$	$C_2$	$L_2$	$L_3$	$C_4$	$L_4$	$L_5$	$C_6$	(see Fig. B.3(a))
4	1.05	4.485	.15780	.18091	4.73822	1.20743	.82637				
	1.10	8.308	.33411	.33438	2.28333	1.26881	.84827				
	1.20	14.387	.53773	.55478	1.12558	1.36980	.85261				
	1.50	26.320	.79962	.88310	.43628	1.53672	.84068				0.1-dB passband ripple
	2.00	38.697	.95051	1.08631	.19517	1.64684	.83004				$R_t=0.73781 \Omega$
6	1.05	20.307	.57153	.65752	1.01346	.92972	.32584	2.72744	1.03524	.88809	
	1.10	27.889	.70783	.81703	.67992	1.10484	.51890	1.54640	1.19779	.88523	
	1.20	37.827	.84244	.98082	.43111	1.32791	.75659	.88144	1.37708	.87992	
	1.50	55.966	.99836	1.17887	.20248	1.64500	1.08849	.38623	1.61158	.87198	
	2.00	74.548	1.08280	1.28970	.09690	1.84134	1.29301	.18123	1.75160	.86710	
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4	1.05	13.243	.95111	.26779	3.20104	1.90749	.80699				
	1.10	18.140	1.16239	.39958	1.91077	2.05228	.80907				
	1.20	24.700	1.40135	.56068	1.11374	2.23453	.80633				1.0-dB passband ripple
	1.50	36.771	1.71483	.78307	.49201	2.49368	.79924				$R_t=0.37598 \Omega$
	2.00	49.156	1.90048	.91820	.23091	2.65459	.79441				
6	1.05	30.730	1.40432	.58067	1.14761	1.37588	.31837	2.79144	1.79883	.82259	
	1.10	38.342	1.56906	.69149	.80335	1.66832	.45609	1.75937	1.99786	.82076	
	1.20	48.285	1.73631	.80659	.52424	2.01190	.62218	1.07185	2.22816	.81822	
	1.50	66.425	1.93461	.94611	.25229	2.47740	.85305	.49283	2.53990	.81461	
	2.00	85.008	2.04359	1.02402	.12205	2.75884	.99547	.23540	2.72966	.81243	
<hr/>											
		$C_1'$	$L_2'$	$C_2'$	$C_3'$	$L_4'$	$C_4'$	$C_5'$	$L_6'$		(see Fig. B.3(b))