



Rolls-Royce



Liquid Impingement Erosion: Modeling Droplet Impacts onto Elastic Solids

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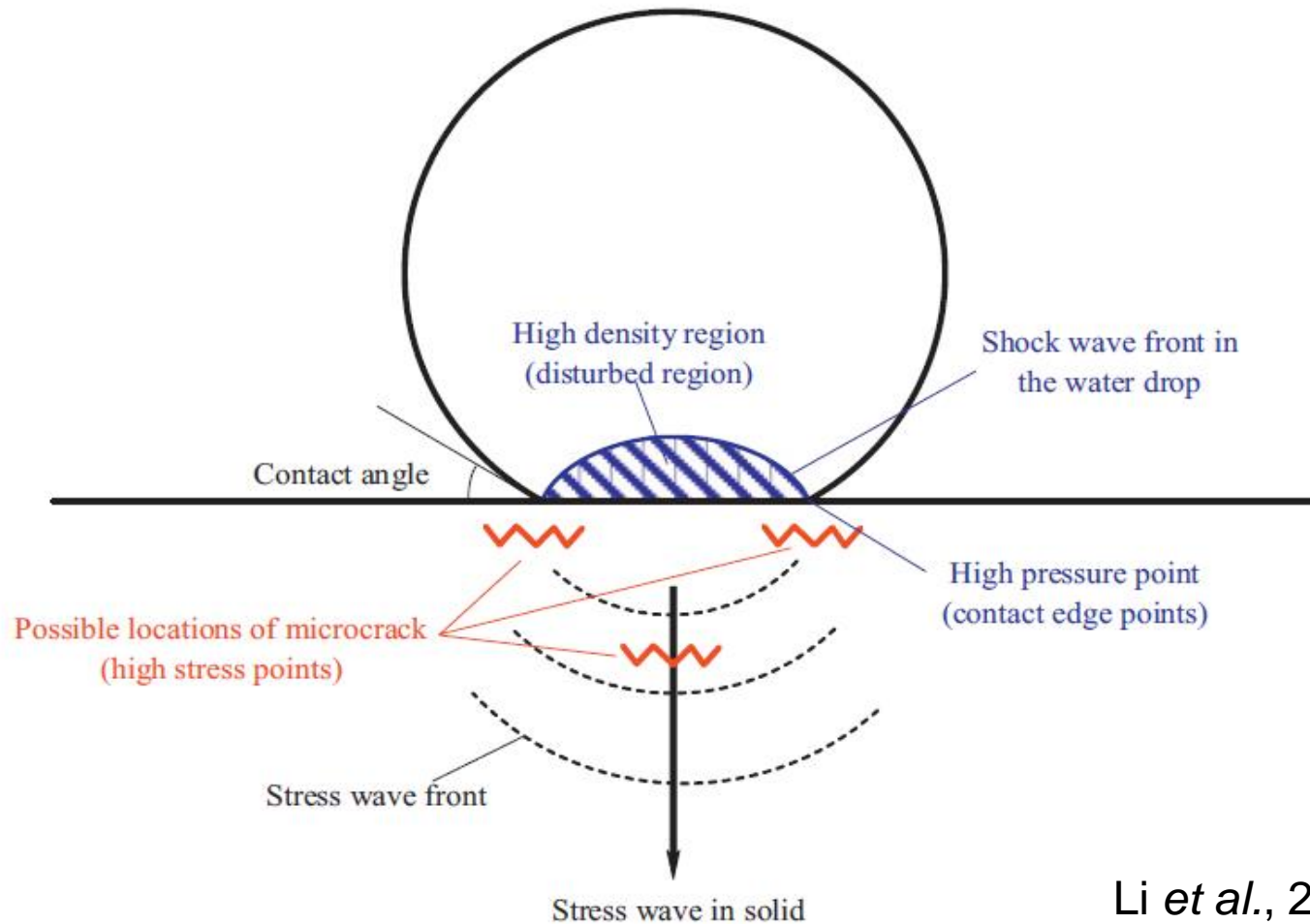
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Concordia University, Montreal

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Fluid-Solid Interaction (FSI)

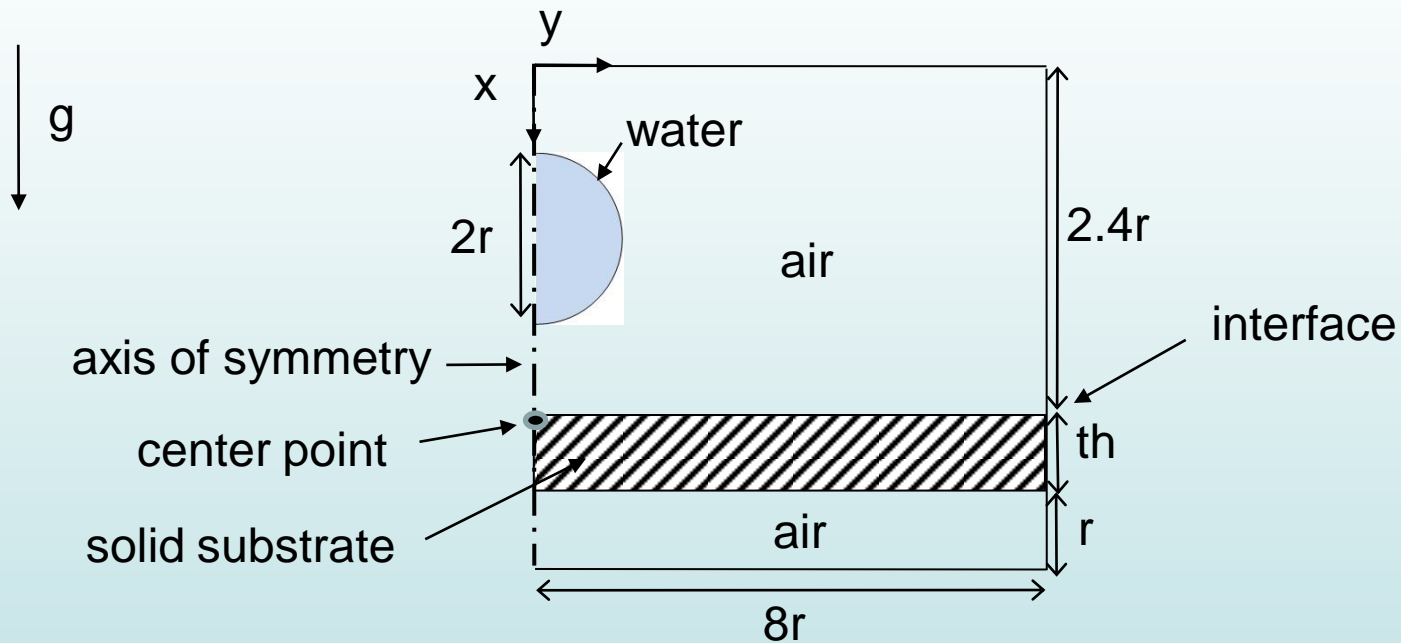


Li *et al.*, 2008

Objectives

- Modeling single droplet impact on an elastic solid
- Capturing droplet deformation upon impact
- Obtaining coupled liquid pressure and solid stress
- Finding maximum transient stress in the solid
- Studying the effect of impact velocity, substrate thickness, droplet diameter, solid material
- Comparing the results with previous works

Computational domain



Note: Not to scale

Governing equations

Fluid:

$$\nabla \cdot V_f = 0 \quad (\text{Continuity})$$

$$\rho_f \frac{\partial V_f}{\partial t} + \rho_f (\nabla V_f) V_f = \nabla \cdot \sigma_f + \rho_f g \quad (\text{Momentum})$$

Solid:

$$\rho_s \frac{\partial V_s}{\partial t} + \rho_s (\nabla V_s) V_s = \nabla \cdot \sigma_s + \rho_s g \quad (\text{Elastic deformation})$$

Coupling Eq'ns:

$$\sigma_s n = \sigma_f n \quad (\text{Force balance})$$

$$V_s = V_f \quad (\text{No-slip condition})$$

Governing equations cont'd

$$\boldsymbol{\sigma}_f = -p_f \mathbf{I} + \rho_f \boldsymbol{\nu}_f (\nabla \mathbf{V}_f + \nabla \mathbf{V}_f^T) \quad \text{(Fluid stress tensor)}$$

$$\boldsymbol{\sigma}_s = \frac{1}{J} \mathbf{F} (\lambda_s (\text{tr} \mathbf{S}) \mathbf{I} + 2\mu_s \mathbf{S}) \mathbf{F}^T \quad \text{(Solid stress tensor)}$$

$$\mathbf{F} = \mathbf{I} + \nabla \mathbf{U}_s \quad \text{(Deformation gradient tensor)}$$

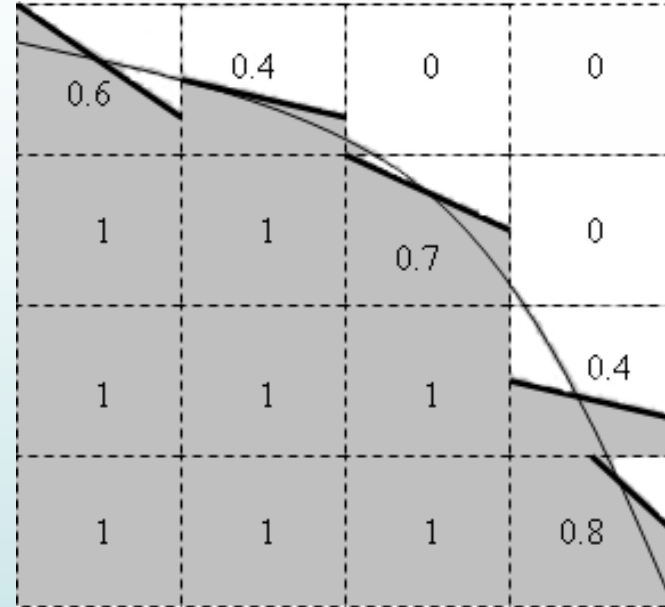
$$\mathbf{S} = \frac{1}{2} (\mathbf{F}^T \mathbf{F} - \mathbf{I}) \quad \text{(St. Venant-Kirchhoff tensor)}$$

$$\lambda_s = \frac{\nu_s E}{(1 + \nu_s)(1 - 2\nu_s)} \quad \text{(Lamé coefficients)}$$

$$\mu_s = \frac{E}{2(1 + \nu_s)}$$

Volume of Fluid method

$$\begin{cases} \alpha_i = 0 & \text{Gas phase} \\ 0 < \alpha_i < 1 & \text{Interface} \\ \alpha_i = 1 & \text{Liquid phase} \end{cases}$$



➤ Advection:

$$\frac{\partial \alpha_l}{\partial t} + \nabla \cdot (V_f \alpha_l) = 0$$

➤ Interface Reconstruction:

Piecewise Linear Interface Calculation (PLIC) of Youngs, 1982.

Impact conditions

- Substrate materials: Martensitic stainless steel, Ti-6Al-4V
- Substrate thicknesses: 2.5, 5.0, 10.0 mm
- Drop diameters: 0.5, 1.0 mm
- Impact velocities: 10, 20, 40 m/s

Equivalent stress:

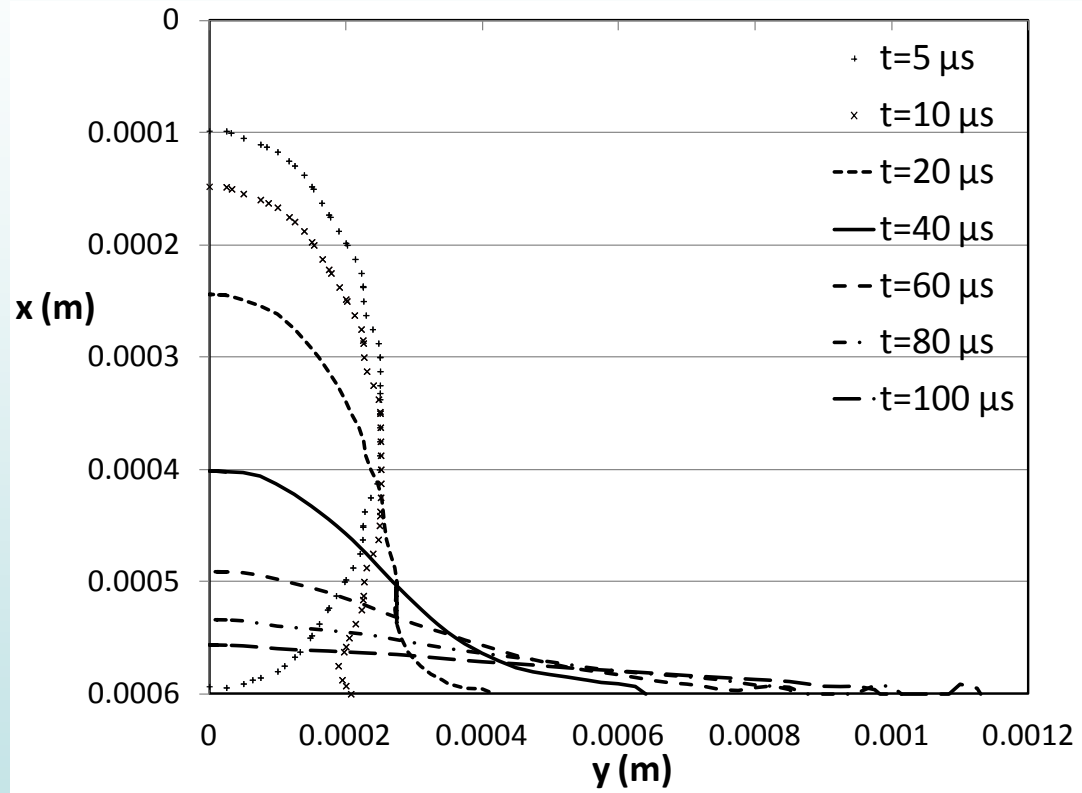
$$\sigma = \sqrt{\frac{1}{2} [(\sigma_{11} - \sigma_{22})^2 + (\sigma_{11} - \sigma_{33})^2 + (\sigma_{22} - \sigma_{33})^2 + 6(\sigma_{12}^2 + \sigma_{23}^2 + \sigma_{13}^2)]}$$

Material properties

Fluid properties	Air	Water
Density (kg/m ³)	1	1000
Kinematic viscosity (m ² /s)	1.48e-05	1e-06
Surface tension (N/m)	-	0.07

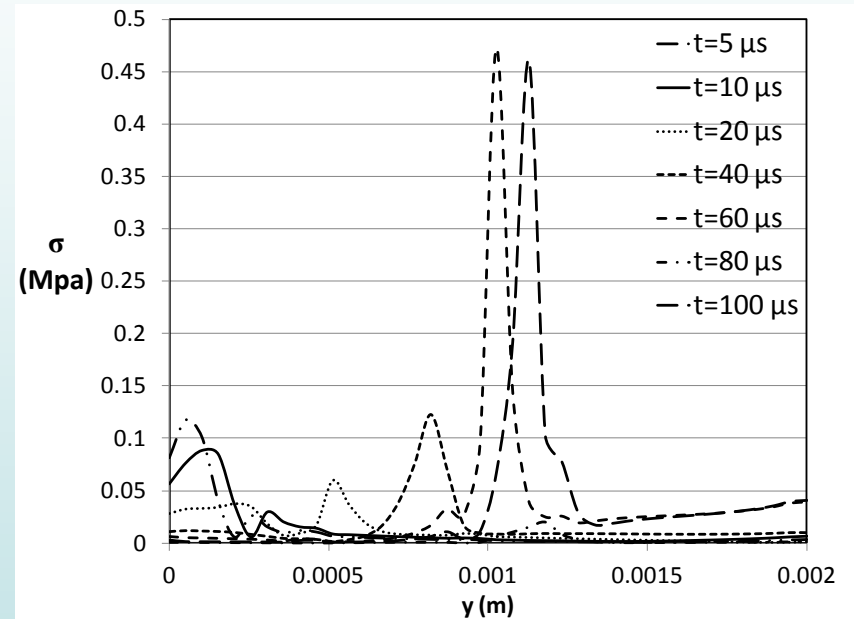
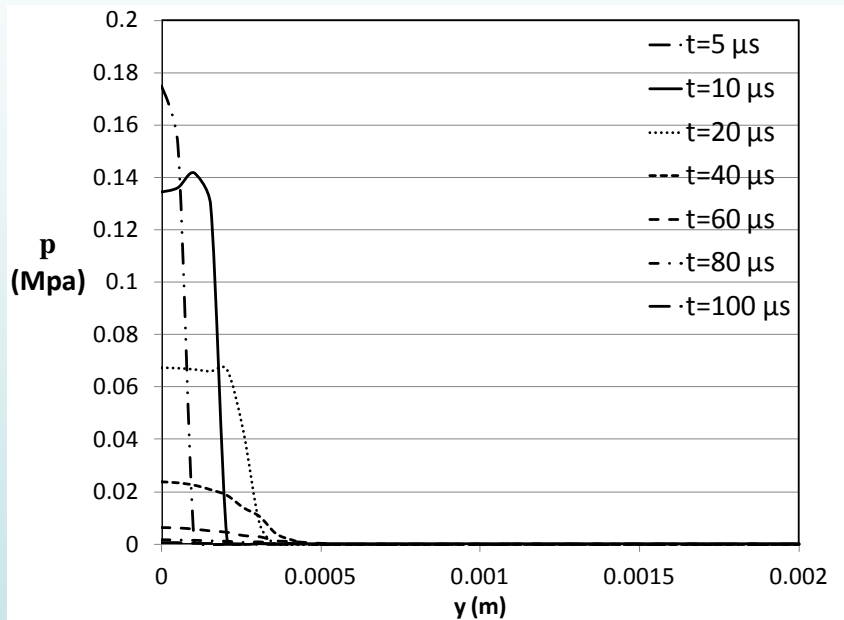
Solid properties	Stainless Steel	Ti-6Al-4V
Density (kg/m ³)	7850	4430
Poisson ratio	0.3	0.342
Young's modulus (Gpa)	200	113

Droplet deformation



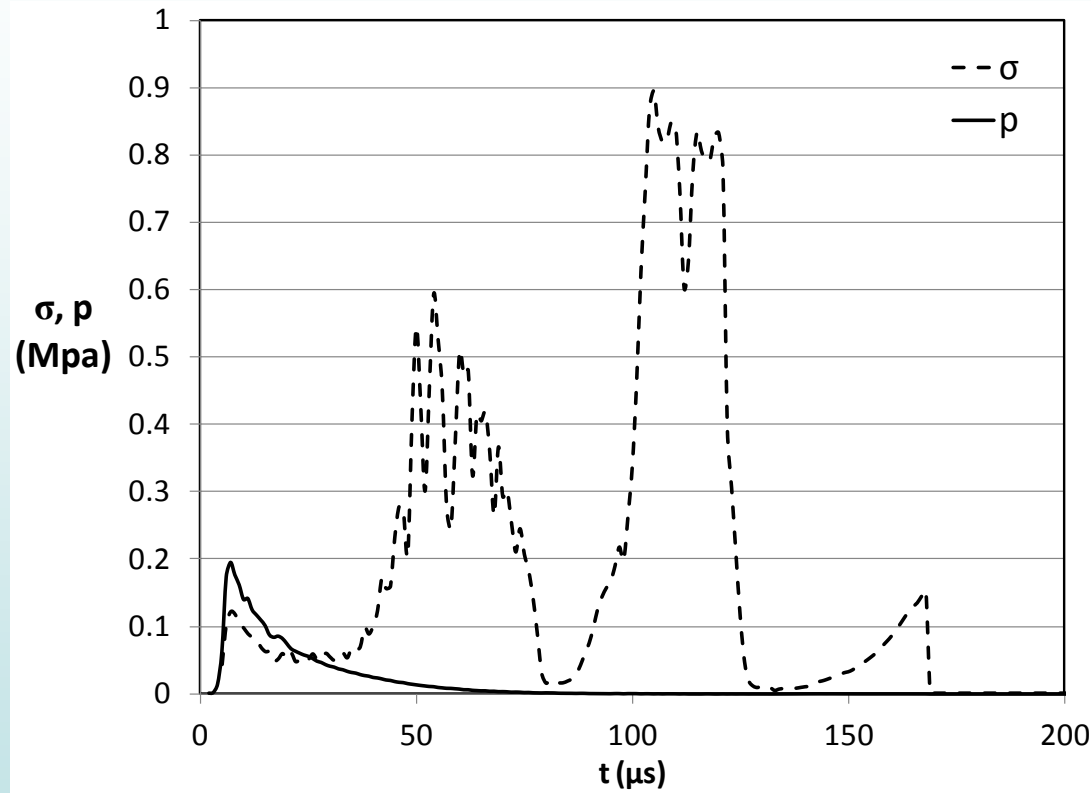
(SS, $V=10\text{m/s}$, $D=0.5 \text{ mm}$, $th=10 \text{ mm}$)

Pressure/stress along interface



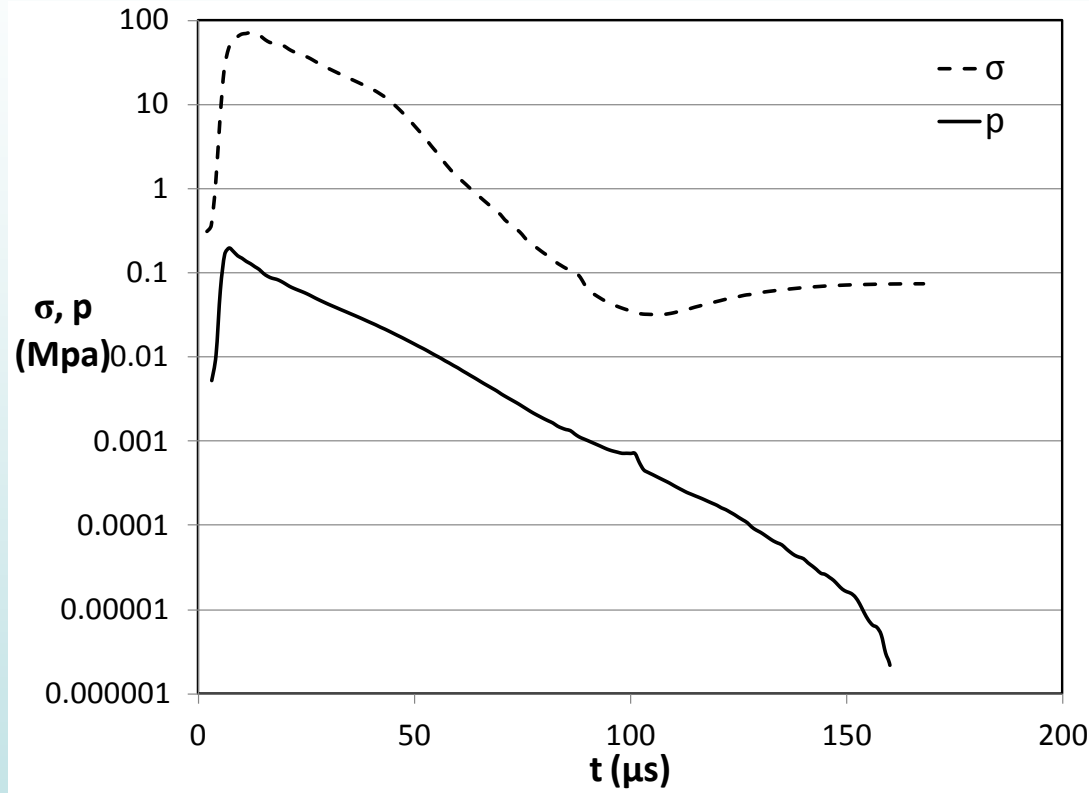
(SS, $V=10\text{m/s}$, $D=0.5 \text{ mm}$, $th=10 \text{ mm}$)

Peak stress/pressure, interface



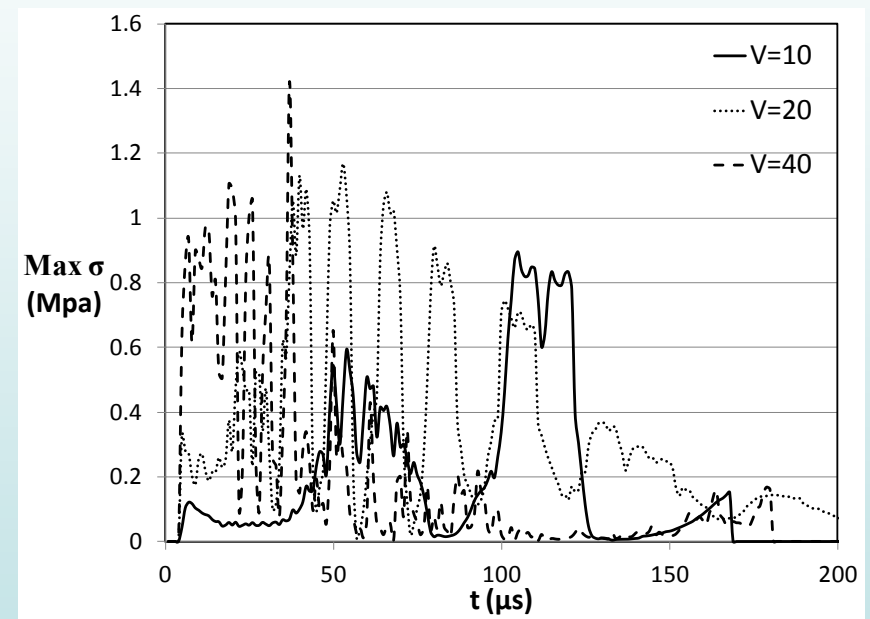
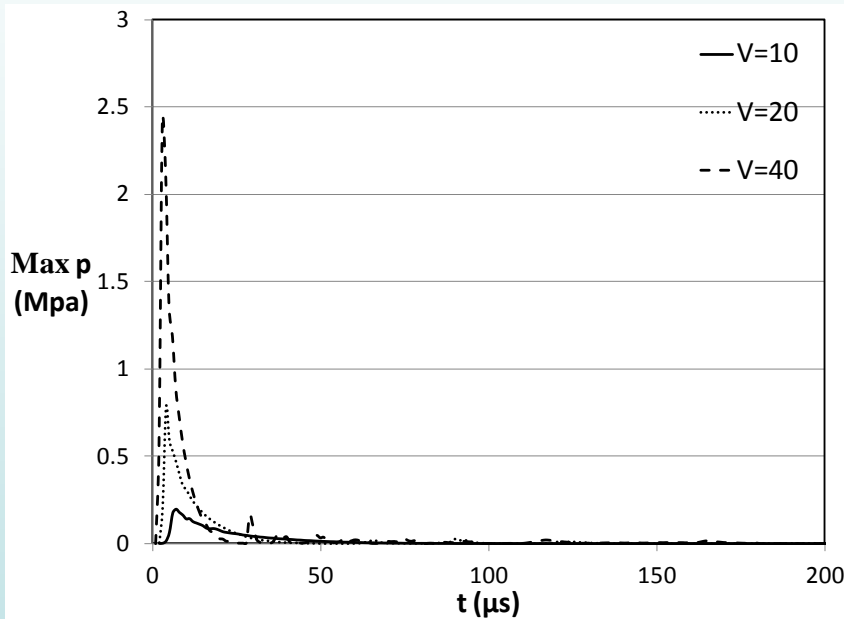
(SS, $V=10\text{m/s}$, $D=0.5 \text{ mm}$, $th=10 \text{ mm}$)

Peak stress/pressure, axis



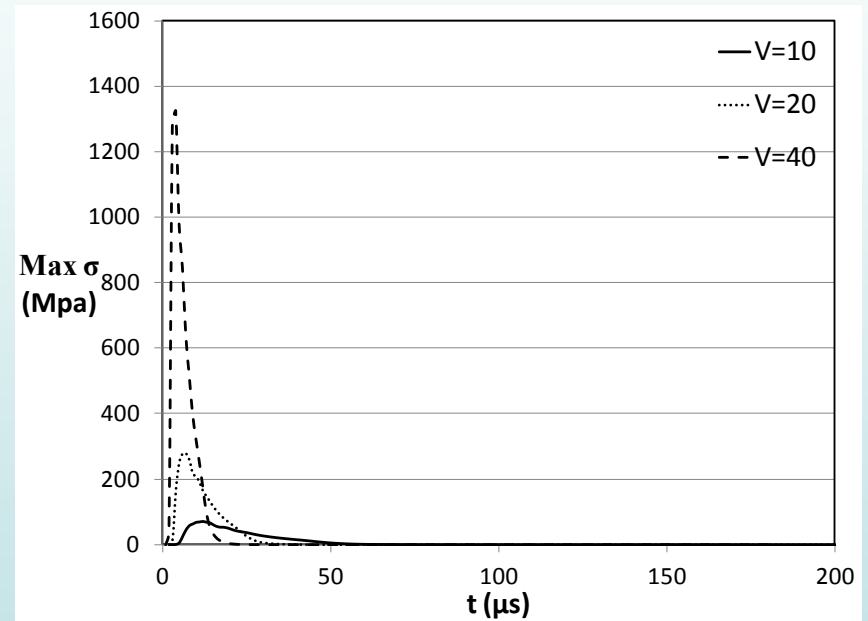
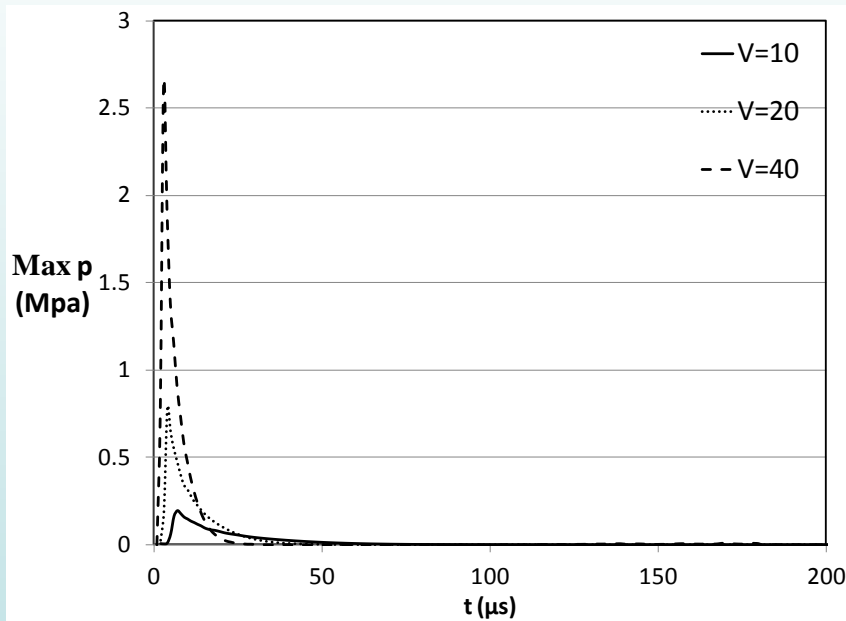
(SS, $V=10\text{m/s}$, $D=0.5\text{ mm}$, $th=10\text{ mm}$)

Impact velocity, interface



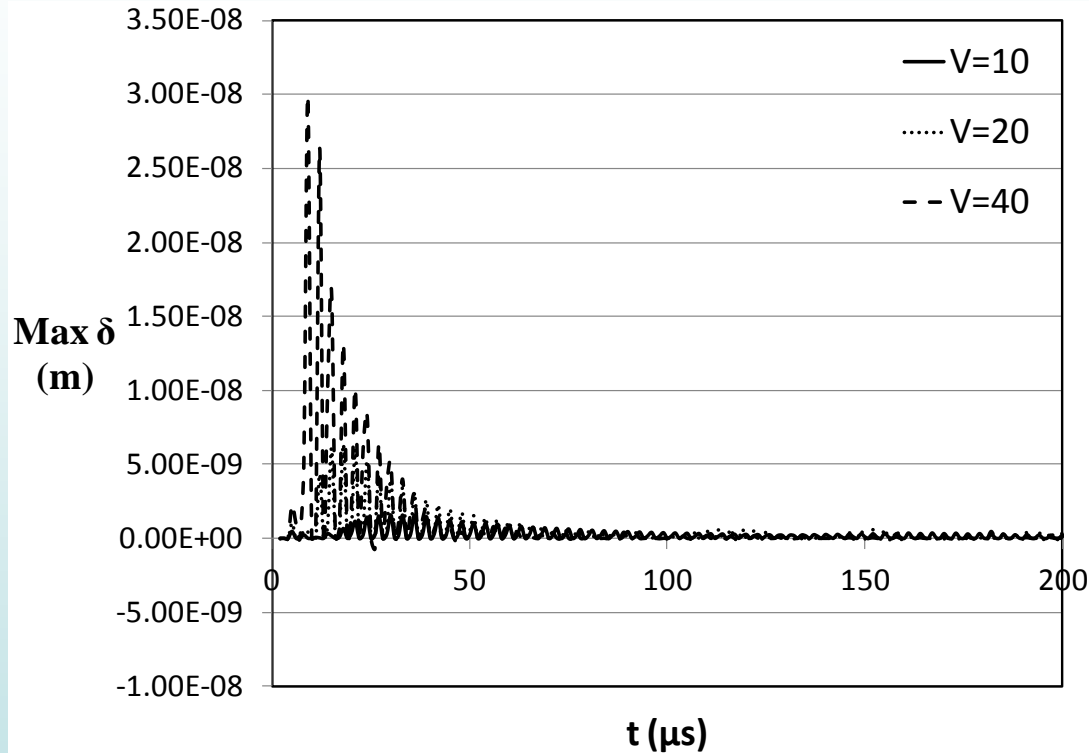
(SS, D=0.5 mm, th=10 mm)

Impact velocity, axis



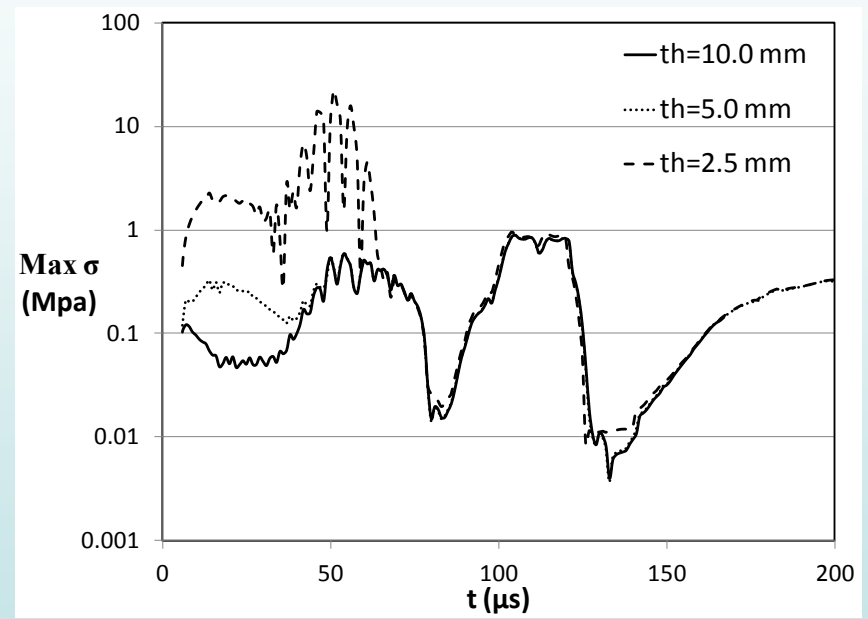
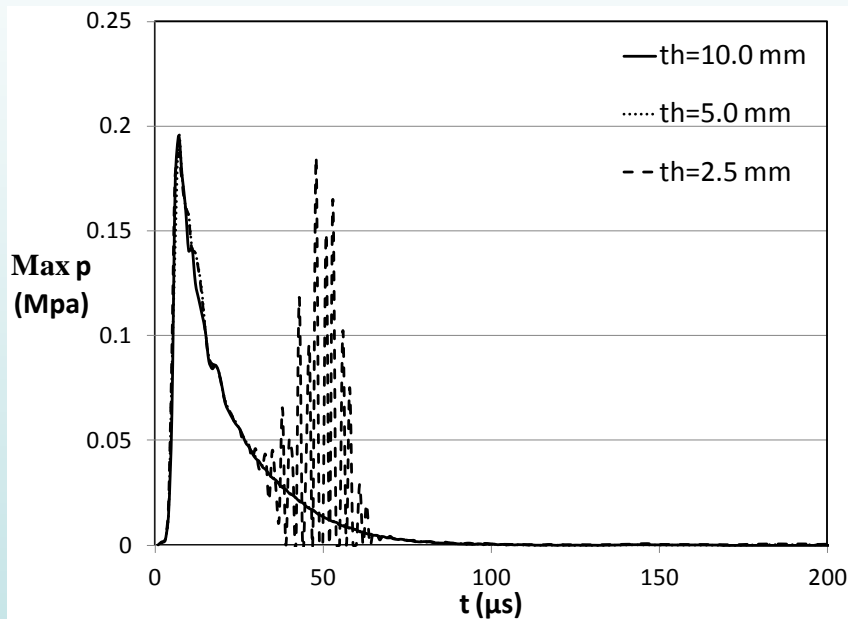
(SS, D=0.5 mm, th=10 mm)

Impact velocity, deflection



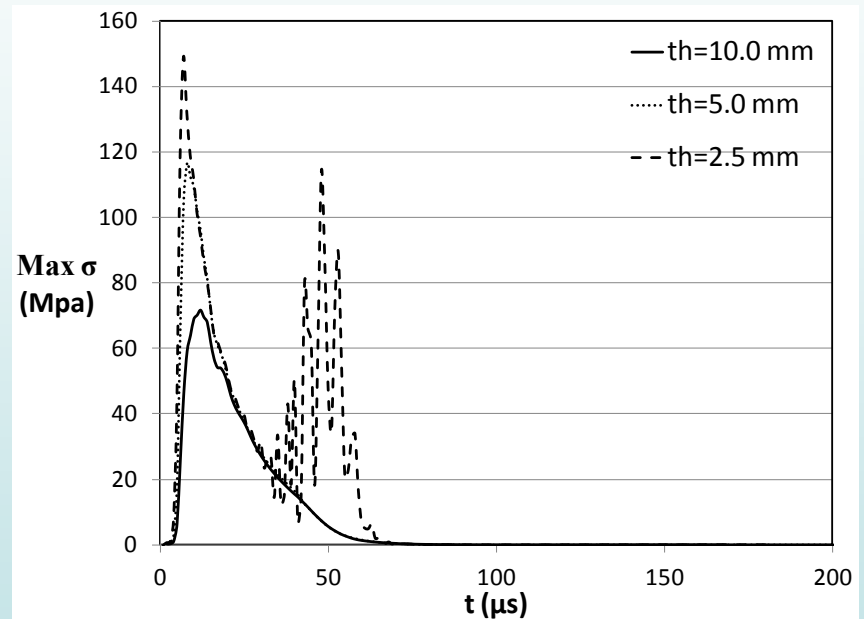
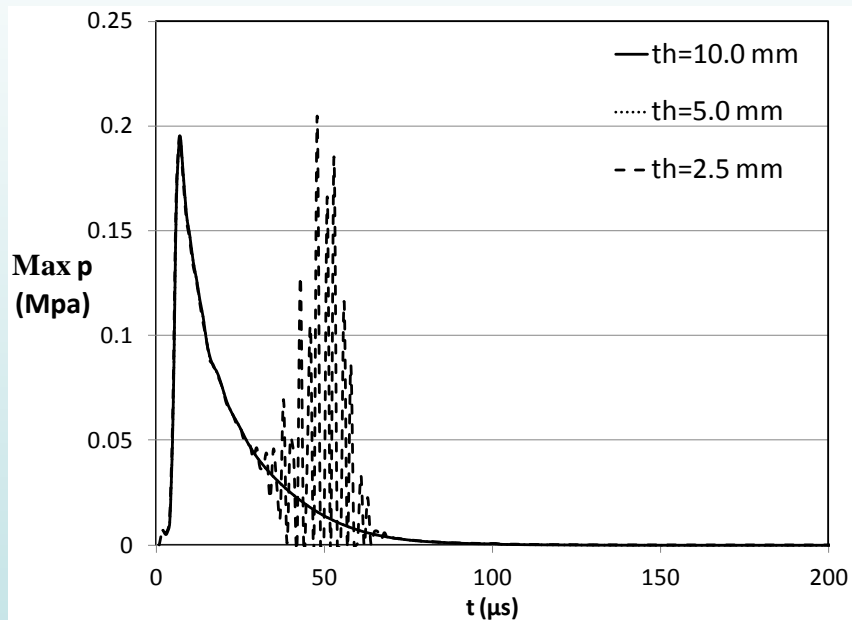
(SS, $D=0.5$ mm, $th=10$ mm)

Substrate thickness, interface



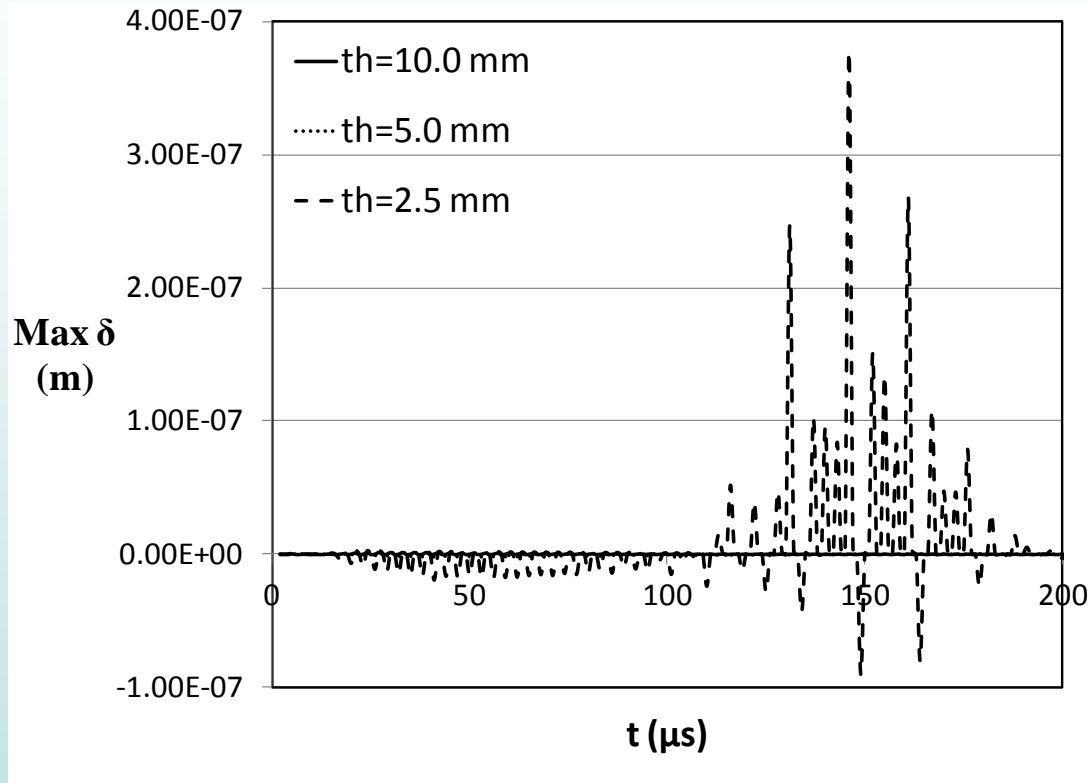
(SS, $V=10\text{m/s}$, $D=0.5\text{ mm}$)

Substrate thickness, axis



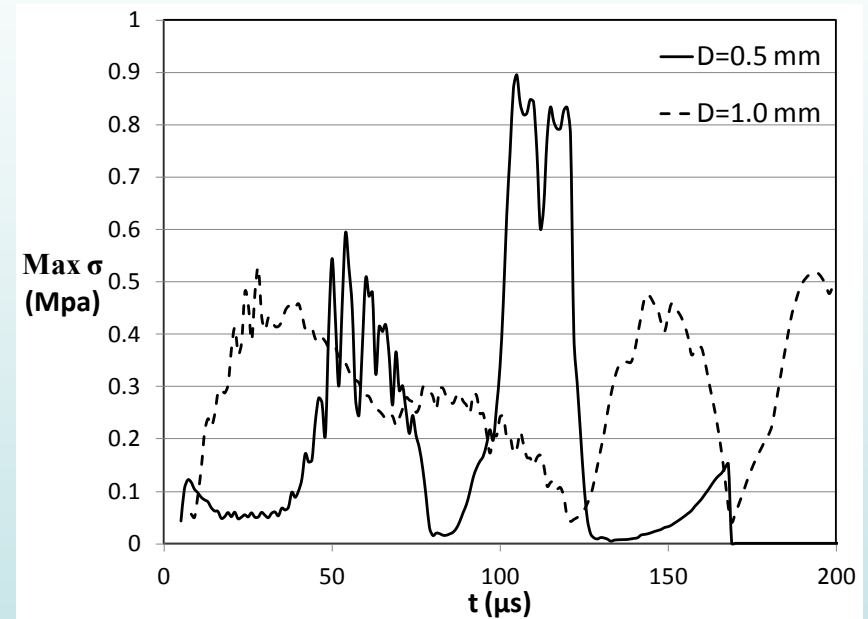
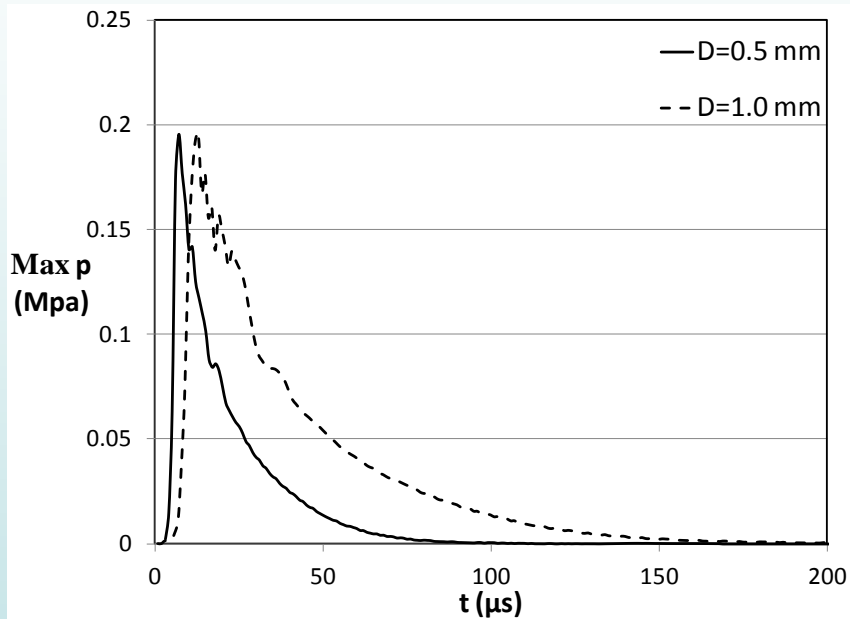
(SS, $V=10\text{m/s}$, $D=0.5\text{ mm}$)

Substrate thickness, deflection



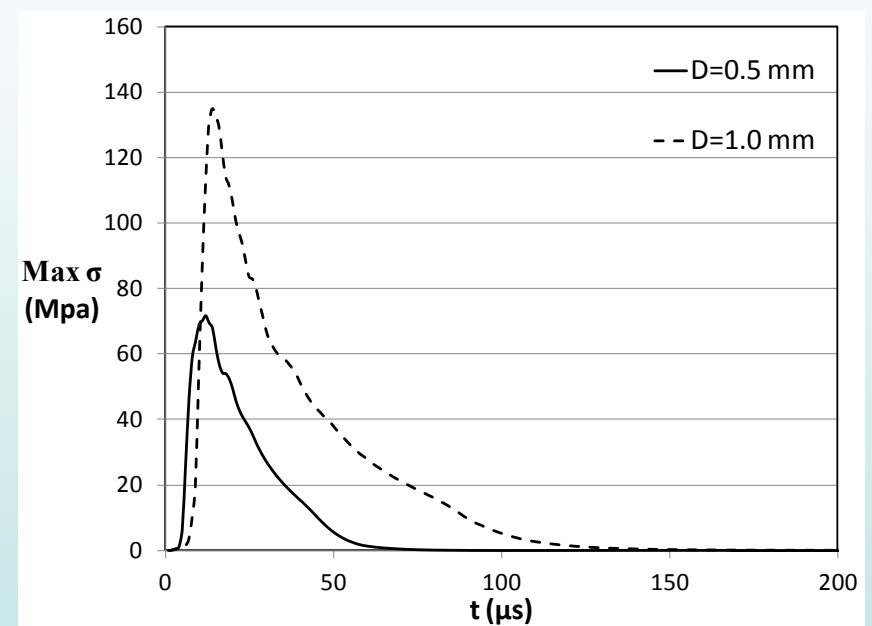
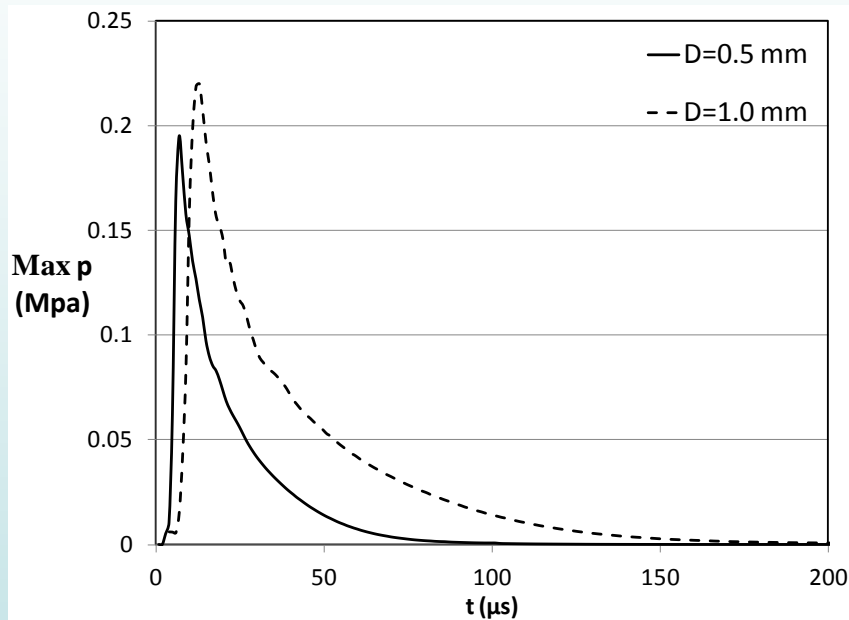
(SS, $V=10\text{m/s}$, $D=0.5$ mm)

Droplet size, interface



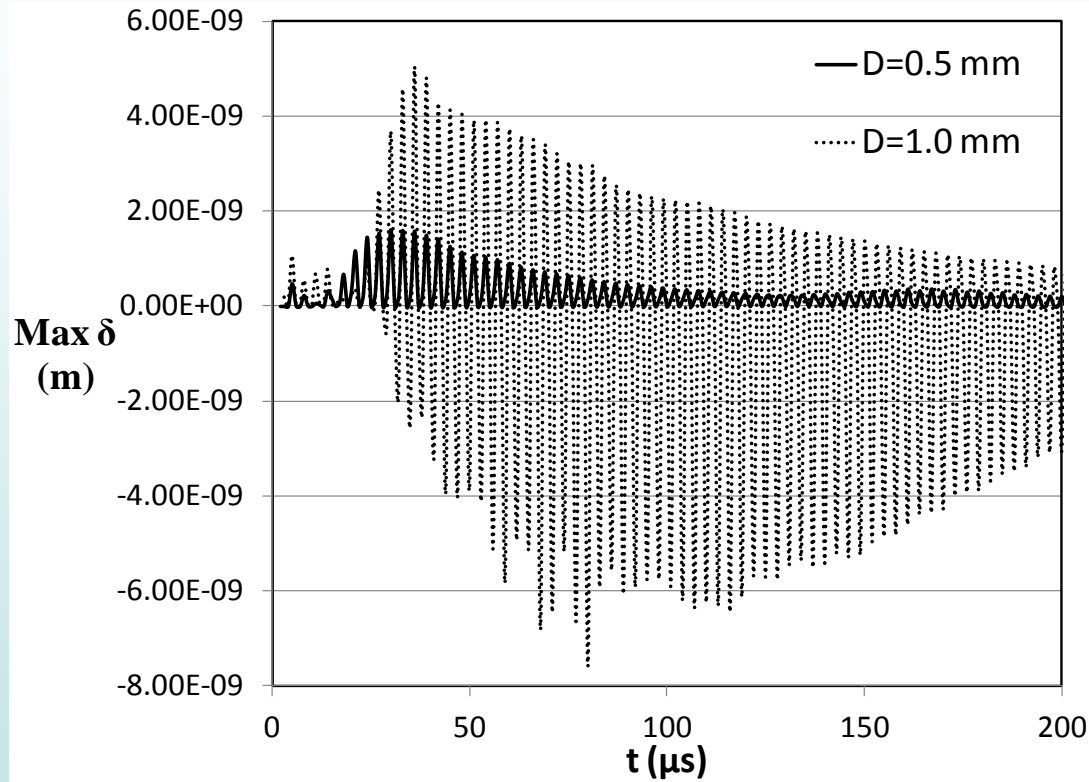
(SS, $V=10\text{m/s}$, $th=10\text{ mm}$)

Droplet size, axis



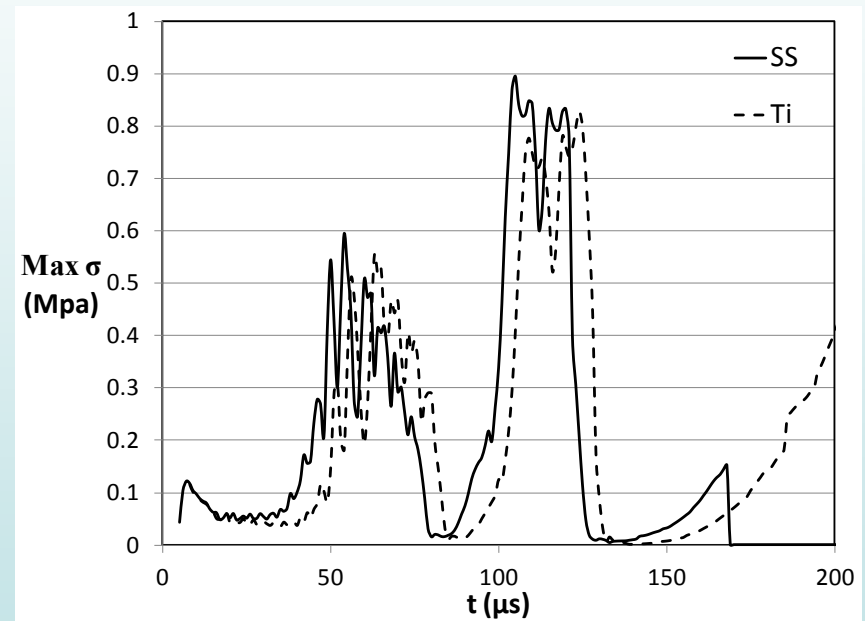
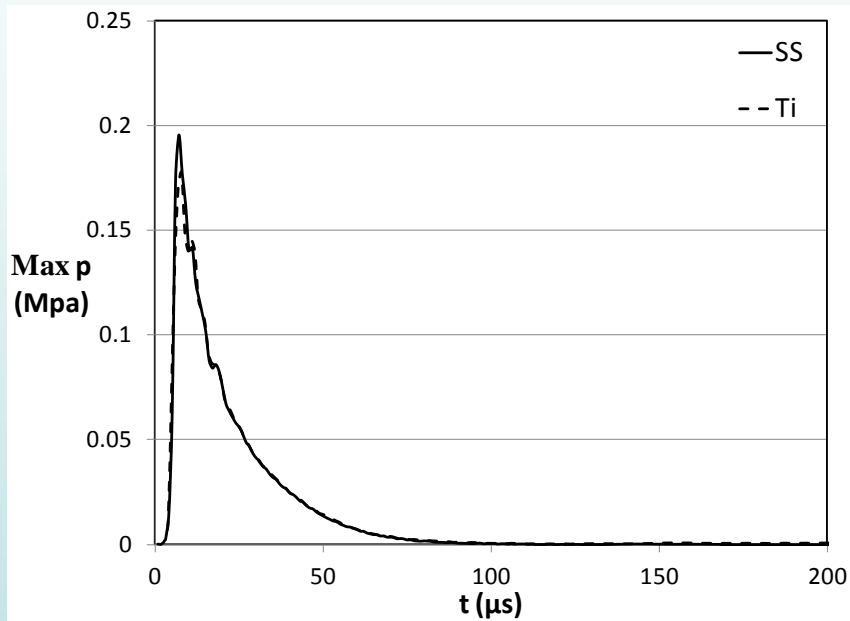
(SS, V=10m/s, th=10 mm)

Droplet size, deflection



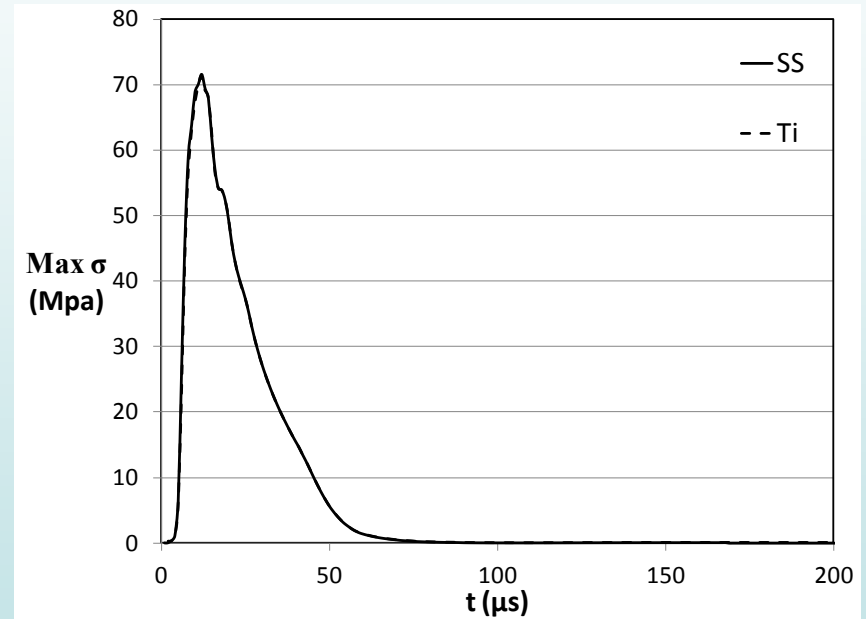
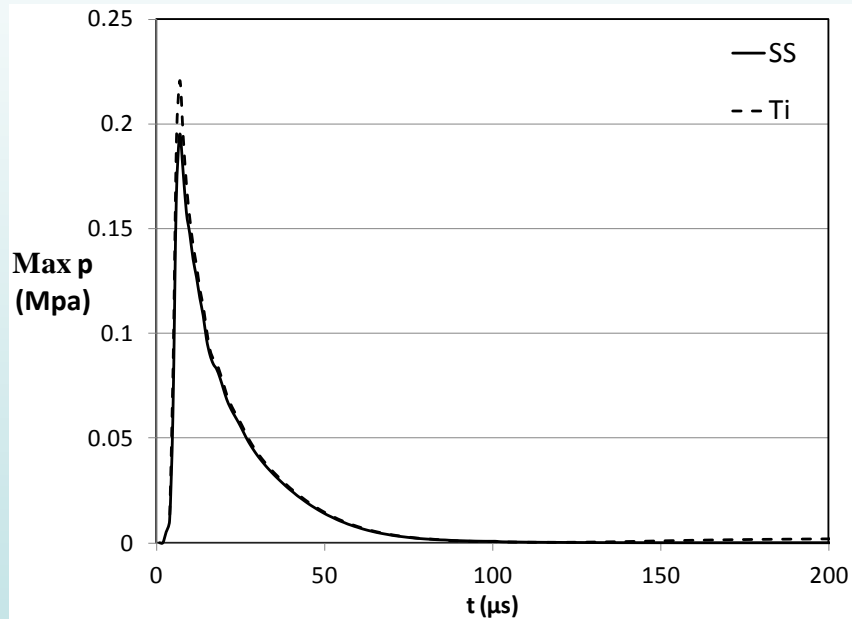
(SS, $V=10\text{m/s}$, $th=10$ mm)

Solid material, interface



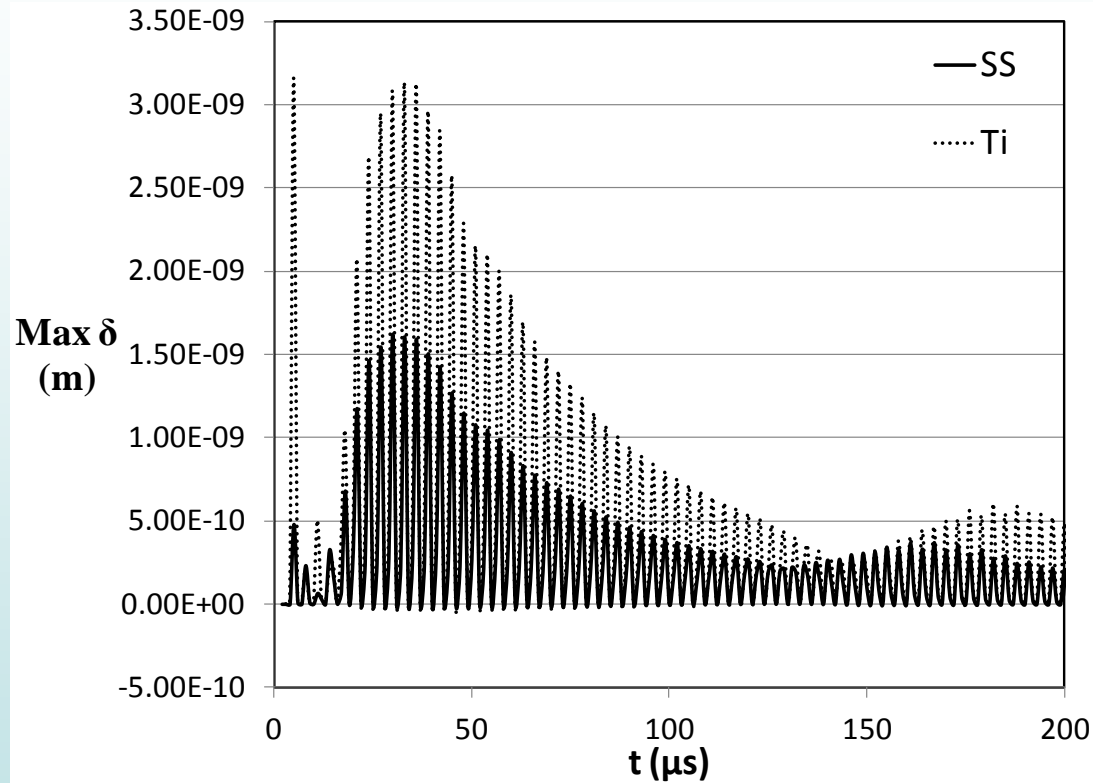
($V=10\text{m/s}$, $D=0.5\text{ mm}$, $th=10\text{ mm}$)

Solid material, axis



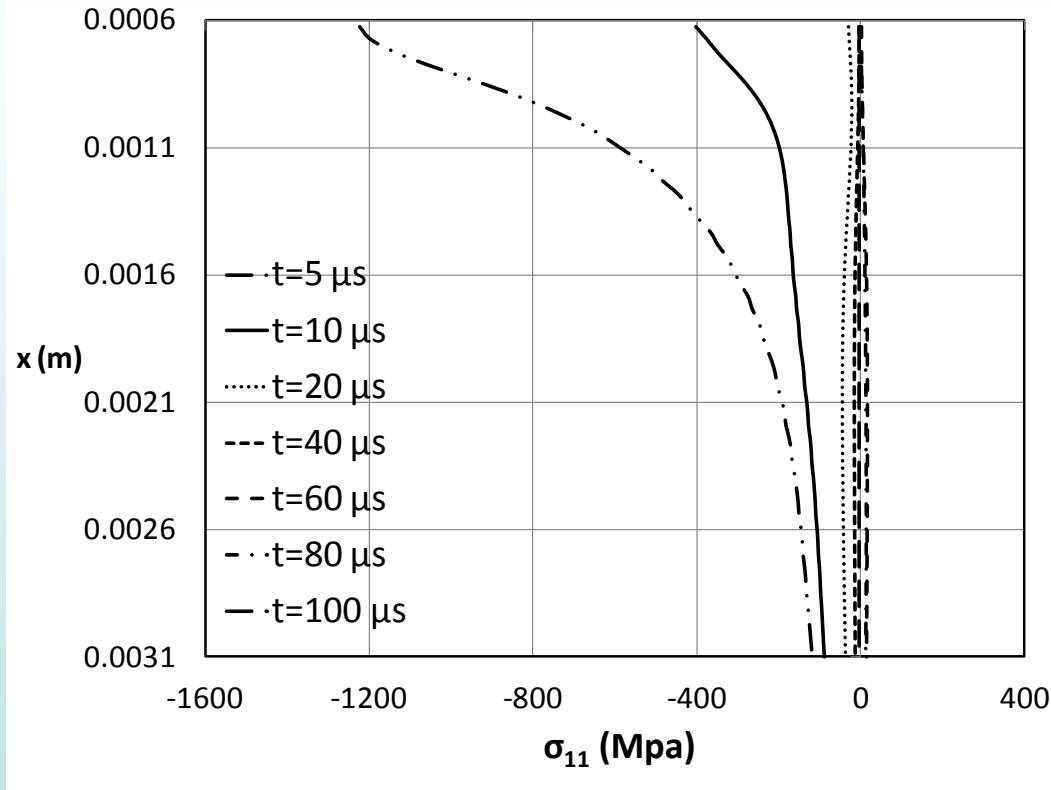
($V=10\text{m/s}$, $D=0.5\text{ mm}$, $th=10\text{ mm}$)

Solid material, deflection



($V=10\text{m/s}$, $D=0.5$ mm, $th=10$ mm)

Tensile Vs. Compressive stresses



(SS, $V=40\text{m/s}$, $D=0.5 \text{ mm}$, $th=2.5 \text{ mm}$)

Summary of numerical results

- Highest stress captured right below the interface
- Tensile stress appeared after loading stage in the solid
- Peak transient stress and maximum deflection were increased by increasing impact velocity and droplet size
- Peak transient stress and maximum deflection were decreased by increasing the substrate thickness
- Deflection was larger for Ti than SS although behavior was similar

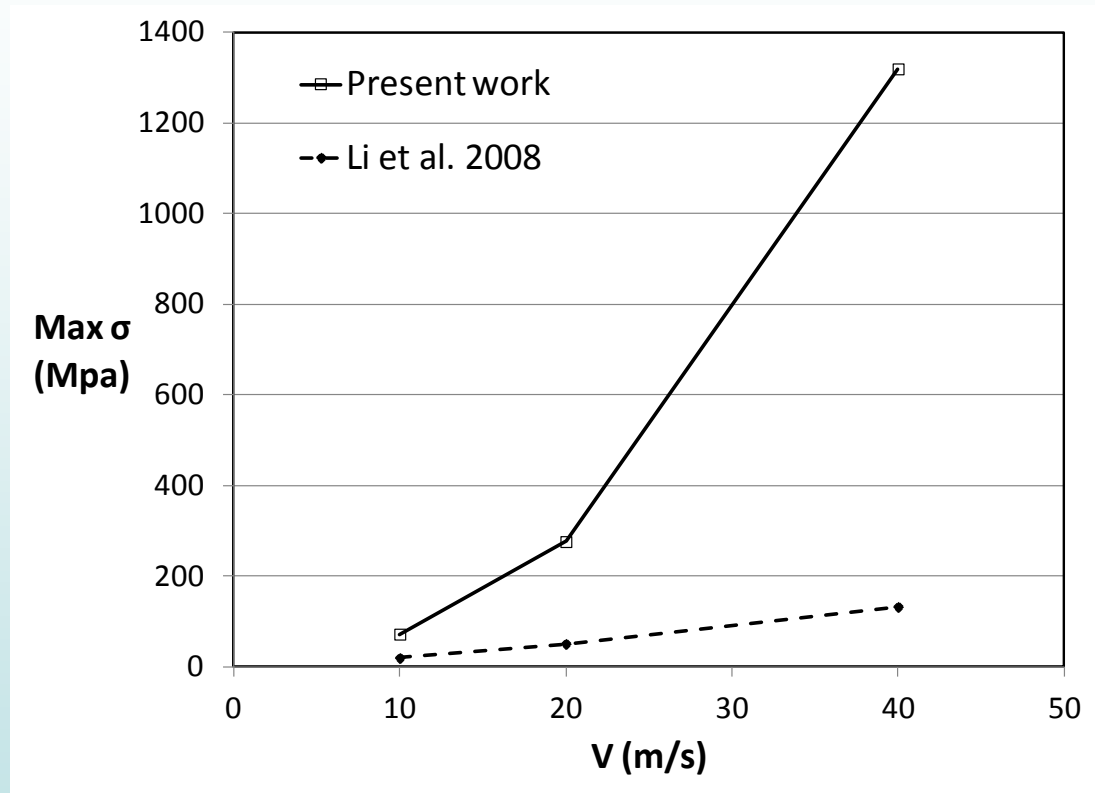
Comparison with literature

Similarities:

1. 2-D axisymmetric
2. SS substrate

Differences:

1. Fluid equation
2. Substrate thickness
3. Drop size



(SS, $D=0.5$ mm, $th=10.0$ mm)

Future work

- Validation of impact results for low/moderate velocities by experimental studies
- Modeling droplet impact at high velocities
- Using compressible equations to solve the fluid
- Implementing Dynamic Grid Adaption in the fluid solver
- 3-D modeling of the drop-solid interaction
- Modeling multiple impacts with on/off-axis orientation

Thank you!

Questions?