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# Investigation on metallic glass formation in Mg-Zn-Sr ternary system combined with the CALPHAD method

Jian Wang <sup>a,b,c</sup>, Zhang Zhang <sup>a,b</sup>, Yi-Nan Zhang <sup>d</sup>, Dong Han <sup>a,b</sup>, Liling Jin <sup>c</sup>, Liyuan Sheng <sup>b,\*</sup>, Patrice Chartrand <sup>c</sup>, Mamoun Medraj <sup>e</sup>

<sup>a</sup> School of Mechanical Engineering, Yangzhou University, Yangzhou 225009, China

<sup>b</sup> Shenzhen Institute, Peking University, Shenzhen 518057, China

<sup>c</sup> Center for Research in Computational Thermochemistry (CRCT), Dept. of Chemical Engineering, École Polytechnique, H3C 3A7, Canada

<sup>d</sup> Institute of Biomaterials and Biomedical Engineering, University of Toronto, Toronto M5S 3G9, Canada

e Department of Mechanical Engineering, Concordia University, 1455 De Maisonneuve Blvd. West, Montreal H3G 1M8, Canada

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#### ABSTRACT

Glass forming ability (GFA) of Mg-Zn alloys with Sr addition has been experimentally studied coupled with CALPHAD method. Two series of metallic glasses (MGs),  $Mg_{98-x}Zn_xSr_2$  (x = 38, 36, 33, 30, 28) and  $Mg_{95-x}Zn_xSr_5$  (x = 37, 33, 30, 27, 23), were designed and prepared successfully for the first time. The crystallization characteristics of these MGs were investigated by differential scanning calorimetry (DSC), X-ray diffraction (XRD). All results indicate that the extraordinary GFA should locate at the composition regions of  $Mg_{68}Zn_{27}Sr_5$  to  $Mg_{60}Zn_{35}Sr_5$  for  $Mg_{95-x}Zn_xSr_5$ , and  $Mg_{68}Zn_{30}Sr_2$  to  $Mg_{64}Zn_{34}Sr_2$  for  $Mg_{98-x}Zn_xSr_5$ , respectively.

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## 1. Introduction

Mg alloys with excellent biocompatibility have become one of the most revolutionary research topics as bio-implant materials [1]. However, the clinic applications are limited with the current developed Mg alloys due to their high corrosion rate and hydrogen release rate [2]. Mg-Zn-Ca based bulk metallic glasses have received considerable attention because of their much lower corrosion rate and good mechanical properties [3]. Unfortunately, the brittleness of Mg-Zn-Ca MGs and poor GFA have hindered their further application [4]. Thus, it is desirable to develop new Mgbased MGs with superior GFA and mechanical properties. Strontium, a bone-seeking element, has been reported to be capable of stimulating bone-cells replication and protein synthesis, depressing bone resorption, and increasing bone mass and strength [5,6]. Hence, it is necessary to develop MGs of the Mg-Zn-Sr system with superior biocompatibility.

The production of MGs is relied on the inhibition of crystalline phase(s) formation using fast solidification process. The composition with relatively lower nuclear driving forces (NDFs), resulting less ability of crystalline phase(s) formation, indicates a super GFA of alloys. Thermodynamic modeling of phase equilibria via

\* Corresponding author. E-mail address: lysheng@yeah.net (L. Sheng). CALPHAD technique enables calculating the NDFs of crystalline phases, which can be used to search the composition of Mg-Zn-Sr alloys with superior GFA. Therefore, in this work, the GFA of Mg-Zn-Sr alloys were studied experimentally combined CALPHAD technique for biomaterials application purpose.

## 2. Experimental procedure

Ten samples in total of  $Mg_{98-x}Zn_xSr_2$  (x = 38, 36, 33, 30, 28) and  $Mg_{95-x}Zn_xSr_5$  (x = 37, 33, 30, 27, 23) were prepared. All samples were prepared by melting high-purity Mg ingot of 99.8%, Sr of 99%, and Zn of 99.99% in an induction furnace. All the samples were melted at least 3 times in a cubic shaped Ta foil crucible under an argon atmosphere to reach good homogeneity. The mass losses of the elements during melting have been taken into account during the weighting, and they were controlled within 1 wt% for each sample. Then, samples were cut into pieces for single-roller meltspinning. The melt-spinning process was carried out under high purity helium protective atmosphere (at a pressure of 50 kPa) with a wheel tangential speed of 50 m/s. The XRD technique was used to verify the amorphous state on the free side of each ribbon. XRD patterns were obtained using PANanalytical X'pert Pro powder Xray diffractometer with a CuKa radiation at 45 kV and 40 mA. The XRD spectrum was acquired from 20 to  $120^{\circ} 2\theta$  with a  $0.02^{\circ}$ step size. The thermal properties of the as-quenched glassy







samples were studied by calibrated non-isothermal DSC from SETARAM instrumentation under a continuous flow of purified argon. All the samples were tested in a graphite crucible covered with lid at the heating rates of 5, 10, 20 and 40 K/min.

#### 3. Results and discussion

The NDFs of crystalline phases of Mg-Zn system are calculated as a function of Zn content at 340 °C (Fig. 1a), at which the alloys correspond to super-cooled liquids. Along with the varying of Zn content, the NDFs of crystalline phases show a "V" shape with the minimum value at the composition around  $Mg_{71}Zn_{29}$  having the superior GFA. Present calculated result is in a good agreement with the reported value of  $Mg_{70}Zn_{30}$  [7,8].

The NDFs of crystalline phases in Mg-Zn-Sr ternary system at 340 °C were calculated with constant values of 2 and 5 at. % Sr as shown in Fig. 1b and c. The "V" shape of NDFs with minimum point locates at compositions of  $Mg_{68}Zn_{30}Sr_2$  and  $Mg_{63}Zn_{32}Sr_5$ , respectively, where indicates the superior GFA of MGs.

Based on the present prediction, ten samples with compositions of  $Mg_{98-x}Zn_xSr_2$  (x = 38, 36, 33, 30, 28) and  $Mg_{95-x}Zn_xSr_5$  (x = 37, 33, 30, 27, 23) were selected for MGs preparation. The XRD patterns of free side part of the as-quenched Mg-Zn-Sr MGs obtained by the melt-spinning method are shown in Fig. 2. The absence of detectable crystalline diffraction peaks, together with the broad scattering peaks at  $2\theta = 38^{\circ}$  to  $66^{\circ}$ , confirms the amorphous nature of these samples except the sample A1 (Mg<sub>70</sub>Zn<sub>28</sub>Sr<sub>2</sub>). By increas-

ing the Zn content, the broad scattering maxima shift slightly towards higher diffraction angles because Zn atom have a smaller atomic radius than Mg. The appearance of little peaks in the XRD pattern indicates that A1 is not homogenous glass.

The "strong liquid" behavior of metallic glasses results in a reduced rate of both crystal nucleation and growth, therefore contributes greatly to the extraordinary GFA [9]. Here, the glass transition temperature (T<sub>g</sub>), melting temperature (T<sub>m</sub>), and crystallization temperatures  $(T_{p1}, T_{p2}, T_{p3}...)$  are used to evaluate the GFA of MGs. The composition dependence of characteristic temperatures: Tg, Tm, Tp1, Tp2, and Tp3 measured using DSC with constant heating rate of 5 K/min in the present work are shown in Fig. 3a, and results obtained from the other heating rates (10, 20, and 40 K/min) are listed in the Table 1. The minimum values of melting temperature changes were determined to be Mg<sub>65</sub>Zn<sub>33</sub>Sr<sub>2</sub> and Mg<sub>65</sub>Zn<sub>28</sub>Sr<sub>5</sub>. The composition dependence of the reduced glass transition temperature  $T_{rg}$  ( $T_{rg} = T_g/T_M$ ) of the two series samples with constant heating rate of 5 K/min are shown in Fig. 3b. These measured results indicated that the extraordinary GFA should locate at the composition regions of  $Mg_{68}Zn_{27}Sr_5$  to  $Mg_{60}Zn_{35}Sr_5$  for  $Mg_{95-x}Zn_xSr_5$ , and  $Mg_{68}Zn_{30}Sr_2$  to  $Mg_{64}Zn_{34}Sr_2$  for  $Mg_{98-x}Zn_xSr_2$ . Moreover, the  $Mg_{95-x}Zn_xSr_5$  alloys have larger formation range and more superior GFA of MGs comparing with  $Mg_{98-x}Zn_xSr_2$  alloys.

The heating rate dependence of crystallization of phase in metallic glass indicates that the nucleation and phase formation are thermally activated process, whereas the rate dependence of



Fig. 1. The calculated DFs of individual crystalline phases of (a) Mg-Zn, (b) Mg<sub>98-x</sub>Zn<sub>x</sub>Sr<sub>2</sub> and (c) Mg<sub>95-x</sub>Zn<sub>x</sub>Sr<sub>5</sub> alloys using CALPHAD technique.



Fig. 2. The XRD patterns of free side parts of the as-quenched Mg–Zn–Sr MGs: (a) Mg<sub>98–x</sub>Zn<sub>x</sub>Sr<sub>2</sub> and (b) Mg<sub>95–x</sub>Zn<sub>x</sub>Sr<sub>5</sub> alloys obtained by the melt-spinning method.



**Fig. 3.** The composition dependence of (a) characteristic temperatures:  $T_g$ ,  $T_m$ ,  $T_{p1}$ ,  $T_{p2}$ , and  $T_{p3}$ ; (b) reduced glass transition temperature  $T_{rg}$  measured of  $Mg_{98-x}Zn_xSr_2$  and  $Mg_{95-x}Zn_xSr_5$  MGs using DSC measurements with constant heating rate of 5 K/min.

Characteristic temperatures and activation energies for crystallization of Mg<sub>98-x</sub>Zn<sub>x</sub>Sr<sub>2</sub> (x = 38, 36, 33, 30) and Mg<sub>95-x</sub>Zn<sub>x</sub>Sr<sub>5</sub> (x = 37, 33, 30, 27, 23) metallic glass.

Sample	Crystallization temperature (K)	Heating rate (K/min)				Activation energy	
		5	10	20	40	(kJ/mol)	
Mg <sub>68</sub> Zn <sub>30</sub> Sr <sub>2</sub> (A2)	T <sub>p1</sub>	433	437	440	443	E <sub>p1</sub>	331.8
	T <sub>p2</sub>	464	469	473	477	E <sub>p2</sub>	296.3
$Mg_{65}Zn_{33}Sr_2$ (A3)	T <sub>p1</sub>	422	425	427	433	E <sub>p1</sub>	350.4
	T <sub>p2</sub>	449	455	461	466	E <sub>p2</sub>	271.7
$Mg_{62}Zn_{36}Sr_2$ (A4)	T <sub>p1</sub>	434	437	440	443	E <sub>p1</sub>	341.9
	$T_{p2}$	463	468	473	477	E <sub>p2</sub>	262.1
$Mg_{60}Zn_{38}Sr_2$ (A5)	T <sub>p1</sub>	442	445	448	452	E <sub>p1</sub>	339.8
	$T_{p2}$	463	468	473	478	E <sub>p2</sub>	247.3
Mg <sub>72</sub> Zn <sub>23</sub> Sr <sub>5</sub> (B1)	T <sub>p1</sub>	410	413	419	423	E <sub>p1</sub>	212.0
	$T_{p2}$	446	454	460	464	E <sub>p2</sub>	186.4
Mg <sub>68</sub> Zn <sub>27</sub> Sr <sub>5</sub> (B2)	T <sub>p1</sub>	422	426	430	436	E <sub>p1</sub>	221.2
	T <sub>p2</sub>	487	495	501	509	Ep2	189.5
$Mg_{65}Zn_{30}Sr_5$ (B3)	T <sub>p1</sub>	434	437	442	446	E <sub>p1</sub>	262.6
	$T_{p2}$	465	468	474	480	E <sub>p2</sub>	239.5
Mg <sub>62</sub> Zn <sub>33</sub> Sr <sub>5</sub> (B4)	T <sub>p1</sub>	443	448	453	457	E <sub>p1</sub>	239.9
	$T_{p2}$	474	478	485	489	E <sub>p2</sub>	245.5
Mg <sub>58</sub> Zn <sub>37</sub> Sr <sub>5</sub> (B5)	T <sub>p1</sub>	464	467	475	478	E <sub>p1</sub>	237.9
	$T_{p2}$	489	496	502	507	E <sub>p2</sub>	228.3

\*Note: Tp1 and Tp2 are crystallization peak temperatures, Ep1 and Ep2 are activation energies.

the kinetic glass transition temperature  $(T_{\sigma})$  is due to the relaxation process in the glass transition region. The apparent activation energy of each characteristic transformation was evaluated by Kissinger method [10]. The Kissinger Equation is based on the shift of the DSC curves with respect to different heating rates:  $Ln (B/T^2)$ = -E/RT + C, where E is the apparent activation energy (AE), B is the heating rate, R is the gas constant, C is a constant and T is the characteristic temperature such as  $T_{p1}$  and  $T_{p2}$  indicated on the DSC curves. The corresponding values of the characteristic temperatures and calculated AE are listed in Table 1. Whereas the 2nd crystallization E<sub>p2</sub> includes the growth of nuclei. The compositions with higher E<sub>p1</sub> should have higher resistance against crystallization, which results in superior GFA. The maximum E<sub>p1</sub> obtained from the Mg<sub>65</sub>Zn<sub>33</sub>Sr<sub>2</sub> and Mg<sub>65</sub>Zn<sub>30</sub>Sr<sub>5</sub> alloys indicates the best thermal stability of MGs compared to other samples. These results show great consistency with the findings (Fig. 3b) obtained from the reduced glass transition temperature T<sub>rg</sub>.

## 4. Conclusions

Table 1

In summary, firstly, the method to prediction GFA via calculating and minimizing NDFs of crystalline compounds using CALPHAD technique was justified. In general, the composition with superior GFA is closely related with minimum point of "V" shape of

crystalline phases NDFs. Moreover, two series of MGs:  $Mg_{98-x}Zn_xSr_2$  (x = 38, 36, 33, 30, 28) and  $Mg_{95-x}Zn_xSr_5$  (x = 37, 33, 30, 27, 23) were designed and prepared successfully for the first time. The crystallization characteristics of these two series of MGs were studied using DSC and XRD techniques. All results indicate that the extraordinary GFA should locates at the composition regions of  $Mg_{68}Zn_{27}Sr_5$  to  $Mg_{60}Zn_{35}Sr_5$  for  $Mg_{95-x}Zn_xSr_5$ , and  $Mg_{68}Zn_{30}Sr_2$  to  $Mg_{64}Zn_{34}Sr_2$  for  $Mg_{98-x}Zn_xSr_2$ .

### **Declaration of Competing Interest**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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