

# Model Reference Adaptive Fault/Damage Tolerant Control of Quadrotor Unmanned Aerial Vehicle (UAV)

**Course instuctor:** 

Dr. Youmin Zhang,

Project by:
Iman Sadeghzadeh
Ankit Mehta

Dept. of Mechanical and Industrial Engineering Concordia University, Montreal, Quebec, Canada

#### **Outlines**

■ Conclusion

■Introduction **■ Modeling the Quad-Rotor UAV** > System model ■ Model Reference Adaptive Control (MRAC) Methods MIT rule an structure **□Simulation Results** > MRAC+LQR **Experimental Results** Nominal case Fault Case: 14.2% loss of the throttle and 15% of Propeller thrust

#### Introduction

- The advantages of the quad-rotor UAV:
  - VTOL
  - Omni-directional flying
  - Does not require mechanical linkages to vary rotor angle of attack.
  - Can be protected by enclosing within a frame (Qball)
- ➤ MRAC controller advantages
  - The MRAC or MRAS is an important adaptive control methodology
  - Robustness to some changes of plant parameters and disturbance
  - Variety of applications: Aerospace, Chemical, Petrochemical, etc...



# System Model

The Qball dynamics are:

$$\ddot{x} = (\sin\psi\sin\phi + \cos\psi\sin\theta\cos\phi)\frac{U_1}{M} \qquad ; \qquad \ddot{\phi} = \frac{U_2}{J_{xx}}$$

$$\ddot{y} = (\sin\psi\sin\theta\cos\phi - \cos\psi\sin\phi)\frac{U_1}{M} \qquad ; \qquad \ddot{\theta} = \frac{U_3}{J_{yy}} \qquad (1)$$

$$\ddot{z} = -g + (\cos\theta\cos\phi)\frac{U_1}{M} \qquad ; \qquad \ddot{\psi} = \frac{U_4}{J_{77}}$$

with the relation between the force/moments  $U_i$  and the thrusts  $T_i$  is

$$U_{1} = T_{1} + T_{2} + T_{3} + T_{4}$$

$$U_{2} = L(T_{3} - T_{4})$$

$$U_{3} = L(T_{1} - T_{2})$$

$$U_{4} = K_{yaw}(u_{1} + u_{2} - u_{3} - u_{4})$$
(2)

and the brushless motor dynamics

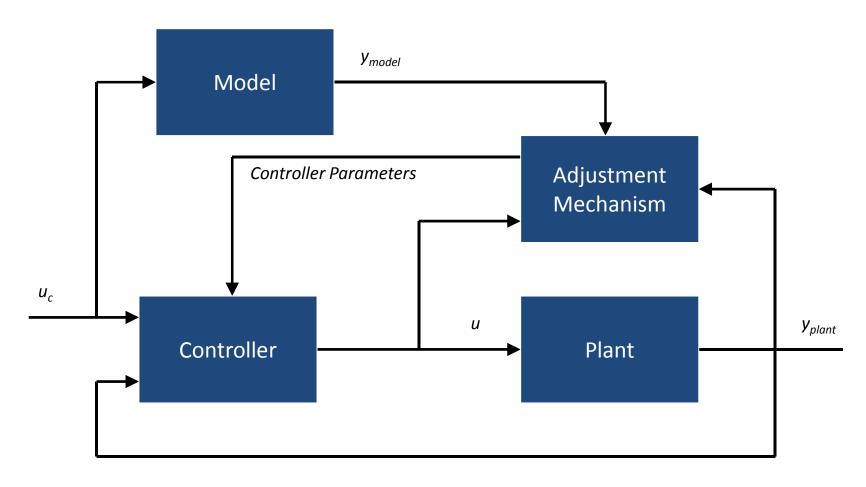
$$T_i = K \frac{W}{s + W} u_i \tag{3}$$

### Different Adaptive Systems

## Model-Reference Adaptive Systems

- The MIT rule
- Lyapunov stability theory
- Design of MRAS based on Lyapunov stability theory
- Hyperstability and passivity theory
- The error model
- Augmented error
- A model-following MRAS

#### **MRAC Structure**



Design controller to drive plant response to mimic ideal response (error =  $y_{plant}$  $y_{\text{model}} => 0$ ) Designer chooses: reference model, controller structure, and tuning gains for

adjustment mechanism

#### The MIT rule

This MRAC approach has been developed around 1960 at MIT for aerospace applications. For illustration, consider the plant :

$$\ddot{y} = -a_1 \dot{y} - a_2 y + u \tag{4}$$

where  $a_1$  and  $a_2$  are the unknown plant parameters. The reference model to be matched by the closed loop plant is :

$$\ddot{y}_m = -2\dot{y}_m - y_m + r \tag{5}$$

where r is the reference command. Let the control input u be defined as follows:

$$u = k_1 \dot{y} + k_2 y + r \tag{6}$$

It is obvious that one can achieve perfect model following if  $k_1$  and  $k_2$  are chosen as:

$$k_1 = a_1 - 2$$
 and  $k_2 = a_2 - 1$  (7)

#### The MIT rule

• With  $e = y - y_m$ , adjust the parameters  $\theta$  to minimize

$$J(\theta) = \frac{1}{2}e^2$$

 It is reasonable to adjust the parameters in the direction of the negative gradient of J:

$$\frac{d\theta}{dt} = -\gamma \frac{\partial J}{\partial \theta} = -\gamma e \frac{\partial e}{\partial \theta}$$

•  $\partial e/\partial \theta$  is called the sensitivity derivative of the system and is evaluated under the assumption that  $\theta$  varies slowly

#### The MIT rule

• The derivative of J is then described by

$$\frac{dJ}{dt} = e\frac{\partial e}{\partial t} = -\gamma e^2 \left(\frac{\partial e}{\partial \theta}\right)^2$$

• Alternatively, one may consider J(e) = |e| in which case

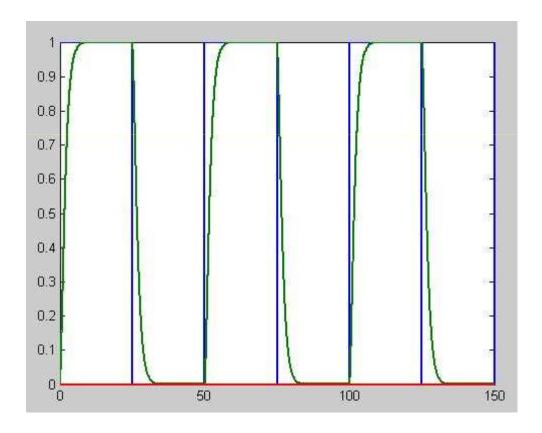
$$\frac{d\theta}{dt} = -\gamma \frac{\partial J}{\partial \theta} = -\gamma \frac{\partial e}{\partial \theta} \text{sign(e)}$$

 The sign-sign algorithm used in telecommunications where simple implementation and fast computations are required, is

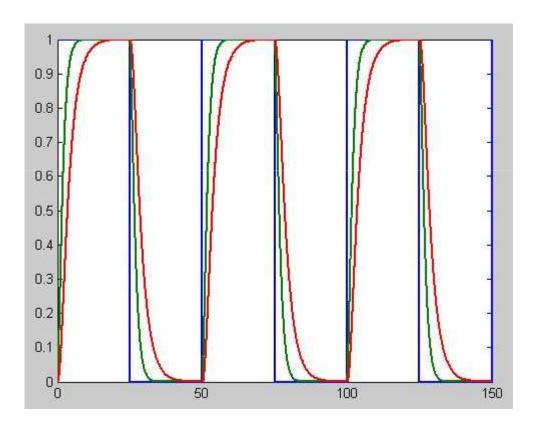
$$\frac{d\theta}{dt} = -\gamma \frac{\partial J}{\partial \theta} = -\gamma \operatorname{sign}\left(\frac{\partial e}{\partial \theta}\right) \operatorname{sign}(e)$$

# Simulation

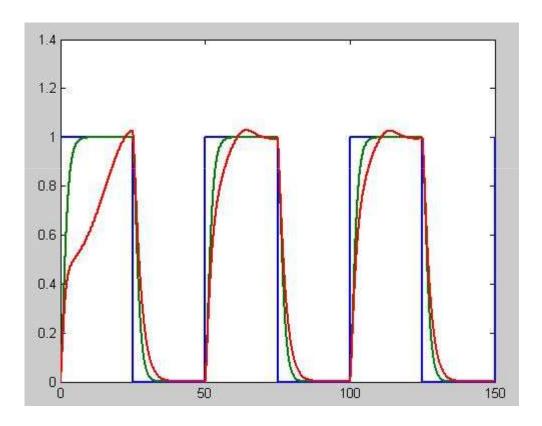
#### MRAC and LQR both are set to zero



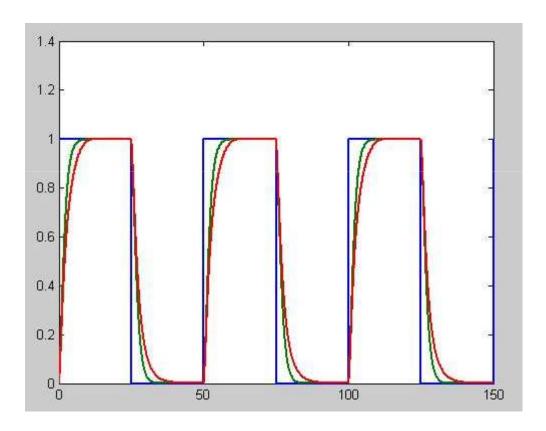
#### MRAC is set to zero



#### LQR is set to zero

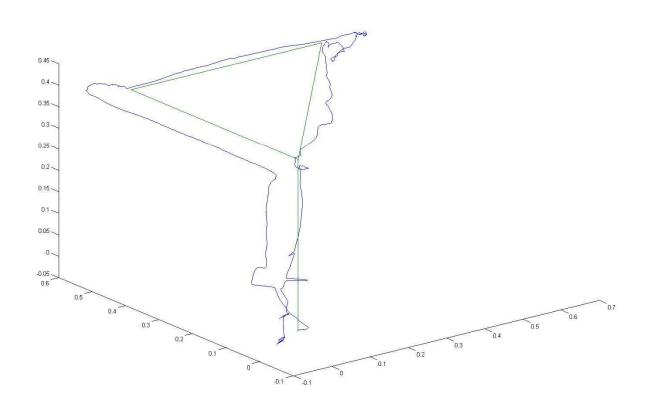


#### MRAC+LQR



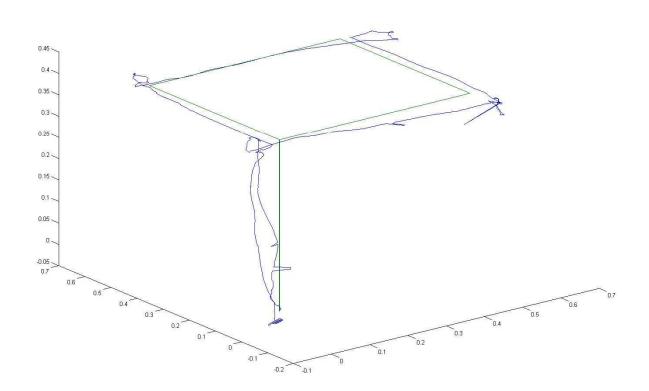
#### Fault-Free Implementation Result

## Triangle trajectory tracking

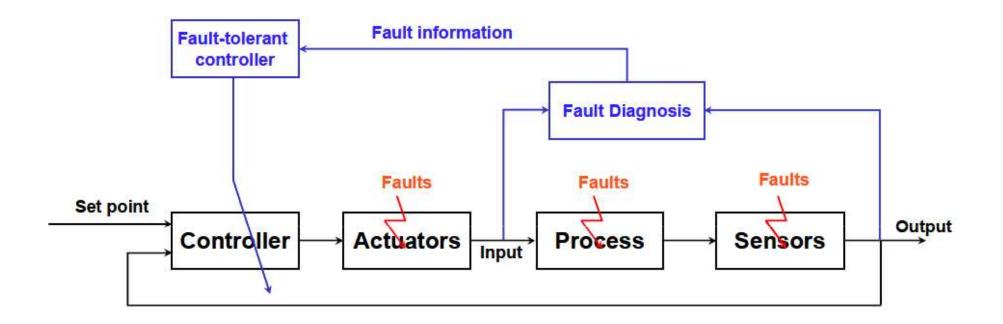


## Fault-Free Implementation Result

## Square trajectory tracking

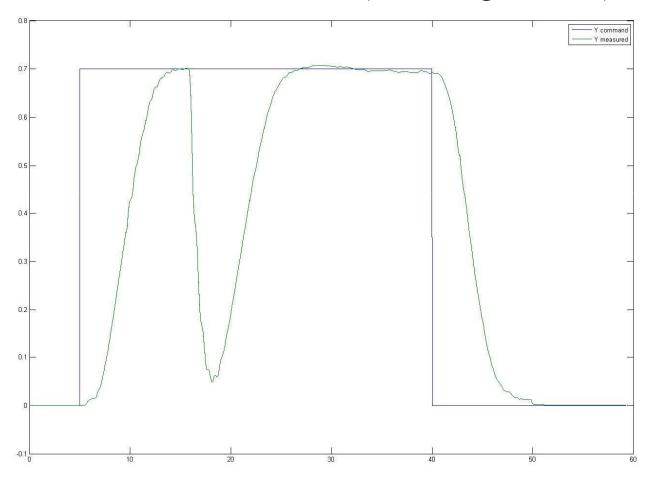


#### Fault Diagnosis and Fault-Tolerant Control

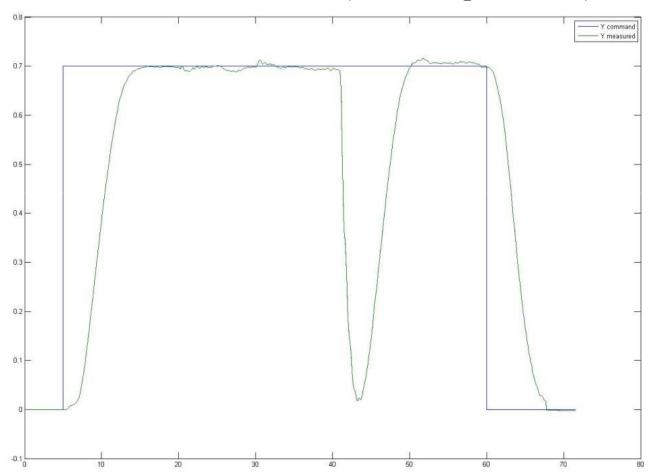


The fault diagnosis module detects, isolates and identifies the fault. The fault-tolerant control module accommodates the fault effect.

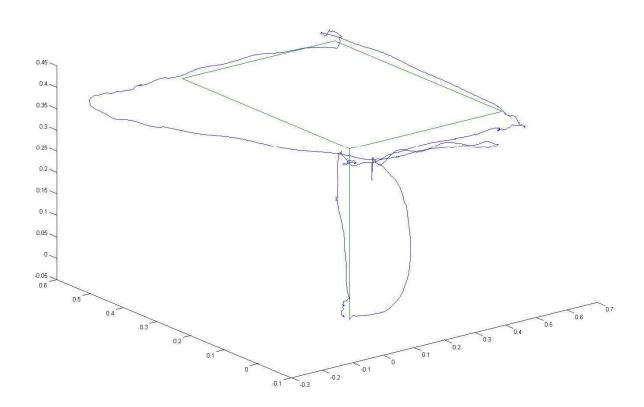
#### 14.2 % of Fault in all actuators (Hovering mode 1)



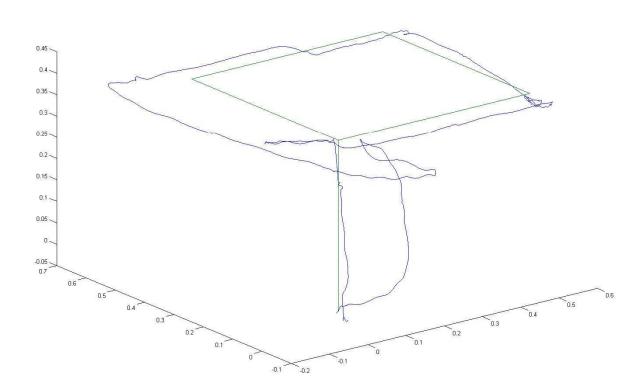
#### 14.2 % of Fault in all actuators (Hovering mode 2)



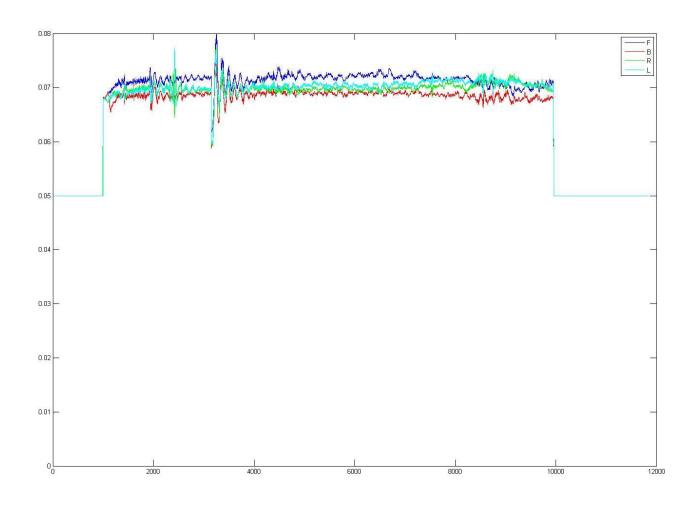
Fault injection to back and left motor (Trajectory tracking mode 1)



Fault injection to back and left motor (Trajectory tracking mode 2)



## **PWM Signals**



#### Conclusions

- 1. Model Reference Adaptive Control forces the dynamic response of the controlled plant to approach asymptotically to that of reference model.
- 2. MRAC and LQR give the best performance to the system.
- 3. The model reference adaptive control minimize the effect of fault on the system's behaviour.
- 4. Better result can be obtained with higher adaption rates. However, very large adaption rate leads to system's instability.
- 5. Two types of fault (Throttle loss and propeller loss) showed almost the same result.

# Thank you

# Questions