

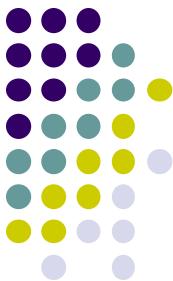


Title: Flight Control Systems

**Submitted to Professor Youmin
Zhang**

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Date: 16-12-2011



1. Combined control method
2. LQG/LTR method
3. Their comparison for two example (longitudinal landing and flare phase landing)

Combined method

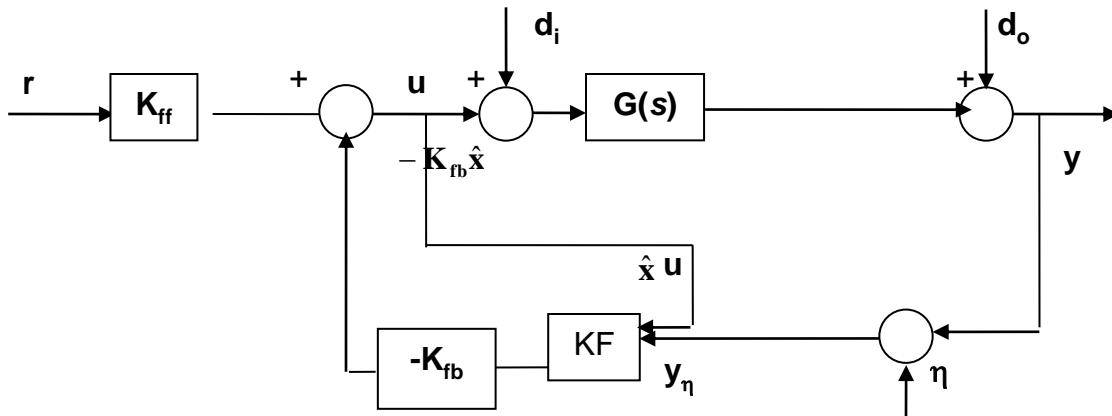
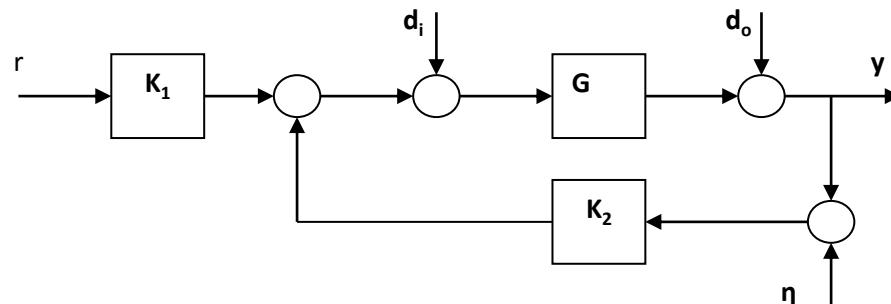


Figure 1. Combination LQT with Kalman Filter (KF)



$$K_1(s) = (I - K_{fb}(sI - A + BK_{fb} + LC)^{-1}B)K_{ff}$$

$$y = (I + GK_2)^{-1}[GK_1r - GK_2\eta + Gd_i + d_o]$$

$$K_2(s) = K_{fb}(sI - A + BK_{fb} + LC)^{-1}L$$

LQG/LTR method

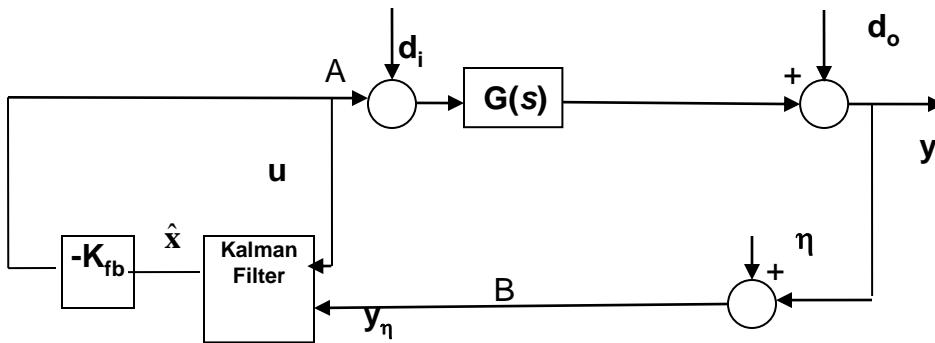
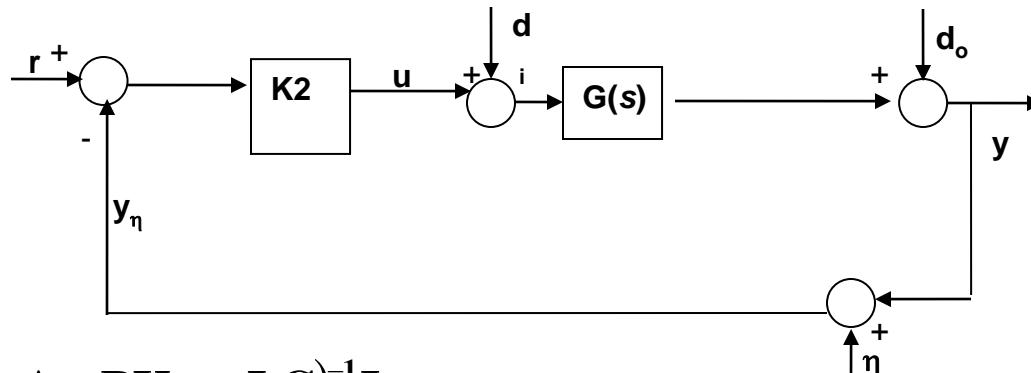
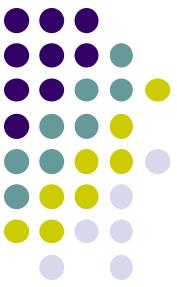


Figure 2. Combination LQR with Kalman Filter (KF).



$$\mathbf{K}_2(s) = \mathbf{K}_{fb}(s\mathbf{I} - \mathbf{A} + \mathbf{B}\mathbf{K}_{fb} + \mathbf{L}\mathbf{C})^{-1}\mathbf{L}$$

$$\mathbf{y} = (\mathbf{I} + \mathbf{G}\mathbf{K}_2)^{-1} [\mathbf{G}\mathbf{K}_2\mathbf{r} - \mathbf{G}\mathbf{K}_2\mathbf{\eta} + \mathbf{G}\mathbf{d}_i + \mathbf{d}_o]$$



$$\dot{\mathbf{x}}(t)=\mathbf{A}.\mathbf{x}(t)+\mathbf{B}.\mathbf{u}(t)$$

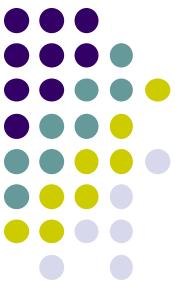
$$\mathbf{y}(t)=\mathbf{C}\mathbf{x}(t)$$

$$\mathbf{e}(t)=\mathbf{r}(t)-\mathbf{y}(t)=\mathbf{r}(t)-\mathbf{C}\mathbf{x}(t)$$

$$\mathbf{x}(t)\in R^n \qquad \mathbf{u}(t)\in R^m$$

$$\mathbf{x}(t_0)=\mathbf{x_0} \qquad t_0 \leq t \leq t_f$$

$$\mathbf{y}(t)\in R^p \qquad m \geq p$$

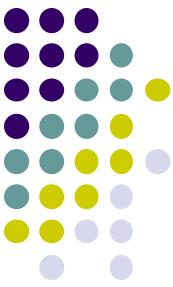


Minimisation Policy in combined méthod

$$J = \frac{1}{2} \mathbf{e}^T(t_f) \mathbf{F} \mathbf{e}(t_f) + \frac{1}{2} \int_{t_0}^{t_f} [\mathbf{e}^T(t) \mathbf{Q} \mathbf{e}(t) + \mathbf{u}^T(t) \mathbf{R} \mathbf{u}(t)] dt$$

Minimisation Policy in LQG/LTR

$$J = \frac{1}{2} x^T(t_f) \mathbf{F} x(t_f) + \frac{1}{2} \int_{t_0}^{t_f} [x^T(t) \mathbf{Q} x(t) + \mathbf{u}^T(t) \mathbf{R} \mathbf{u}(t)] dt$$



Calculating feed forward and feedback gain.

$$\text{Rank } [\mathbf{co}] = n$$

$$[\mathbf{co}] = \begin{bmatrix} \mathbf{B} & \mathbf{AB} & \dots & \mathbf{A}^{n-1}\mathbf{B} \end{bmatrix}$$

$$\mathbf{u}(t) = -\mathbf{K}_{fb}\mathbf{x}(t) + \mathbf{u}_c(t)$$

$$\dot{\mathbf{P}}(t) = -\mathbf{PA} - \mathbf{A}^T\mathbf{P} - \mathbf{C}'\mathbf{QC} + \mathbf{PBR}^{-1}\mathbf{B}^T\mathbf{P} = \mathbf{0}$$

$$\mathbf{K}_{fb} = \mathbf{R}^{-1}\mathbf{B}^T\mathbf{P}$$

Calculating Feedback gain for both methods are the same

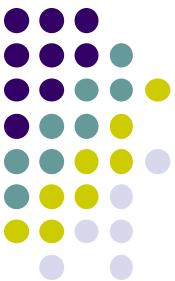
$$\dot{\mathbf{h}}(t) = -[\mathbf{A} - \mathbf{BK}_{fb}]^T\mathbf{h}(t) - \mathbf{C}^T\mathbf{Qr}(t) = 0$$

$$\mathbf{h}(t) = (\mathbf{A} - \mathbf{BK}_{fb})^{T^{-1}}(-\mathbf{C}^T\mathbf{Qr}(t))$$

$$\mathbf{K}_{ff} = \mathbf{R}^{-1}\mathbf{B}^T \left[-(\mathbf{A} - \mathbf{BK}_{fb})^{T^{-1}}\mathbf{C}^T\mathbf{Q} \right]$$

$$\mathbf{u}_c(t) = \mathbf{R}^{-1}\mathbf{B}^T\mathbf{h}(t)$$

$$\mathbf{u}(t) = -\mathbf{K}_{fb}\mathbf{x}(t) + \mathbf{K}_{ff}\mathbf{r}(t)$$



Kalman Filter Dynamics and its gain calculation

$$\dot{\mathbf{x}}(t) = \mathbf{Ax}(t) + \mathbf{Bu}(t) + \mathbf{H}\xi(t)$$

$$\mathbf{y}(t) = \mathbf{Cx}(t) + \boldsymbol{\theta}(t)$$

$$\boldsymbol{\varepsilon}(t) = \mathbf{x}(t) - \hat{\mathbf{x}}(t)$$

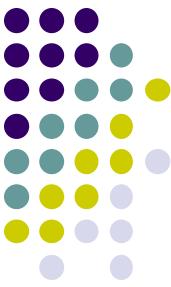
$$J = E\left\{ \sum_{i=1}^n \varepsilon_i^2(t) \right\} = E\left\{ \boldsymbol{\varepsilon}^T(t) \boldsymbol{\varepsilon}(t) \right\} = \text{trace}\left[E\left\{ \boldsymbol{\varepsilon}(t) \boldsymbol{\varepsilon}^T(t) \right\} \right]$$

$$\dot{\hat{\mathbf{x}}}(t) = \mathbf{A}\hat{\mathbf{x}}(t) + \mathbf{Bu}(t) + \mathbf{L}[\mathbf{y}(t) - \mathbf{C}\hat{\mathbf{x}}(t)]$$

$$\boldsymbol{\Sigma} = \text{cov}\left\{ \boldsymbol{\varepsilon}; \boldsymbol{\varepsilon} \right\} = E\left\{ \boldsymbol{\varepsilon} \boldsymbol{\varepsilon}^T \right\}$$

$$\mathbf{A}\boldsymbol{\Sigma} + \boldsymbol{\Sigma}\mathbf{A}^T + \mathbf{G}\boldsymbol{\Xi}\boldsymbol{\Xi}^T - \boldsymbol{\Sigma}\mathbf{C}^T\boldsymbol{\Theta}^{-1}\mathbf{C}\boldsymbol{\Sigma} = \mathbf{0}$$

$$\mathbf{L} = \boldsymbol{\Sigma}\mathbf{C}^T\boldsymbol{\Theta}^{-1}$$



LTR Procedure for both methods:

Consider: $\mathbf{G}_p(s) = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$

Is minimum phase. We have to select an appropriate \mathbf{Q} and \mathbf{R} for the riccati equation to find feedback gain so that $\mathbf{K}_{fb}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$ Has good step respond ie.

In low frequency $\underline{\sigma}[\mathbf{K}_{fb}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}] \succ 1$

In high frequency $\bar{\sigma}[\mathbf{K}_{fb}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}] \ll 1$

$$\boldsymbol{\Xi} = \mu\mathbf{I} + \mathbf{B}\mathbf{B}'$$

$$\boldsymbol{\Theta} = \mu\mathbf{I}$$

$$\mathbf{K}_2(s)\mathbf{G}_p(s) \xrightarrow{\hspace{2cm}} \mathbf{K}_{fb}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$$



Example: The example is about
Longitudinal Control for automatic landing.

The matrices **A**, **B** and **C** describe the
longitudinal dynamics for a transport
aircraft in the flare phase when its speed is

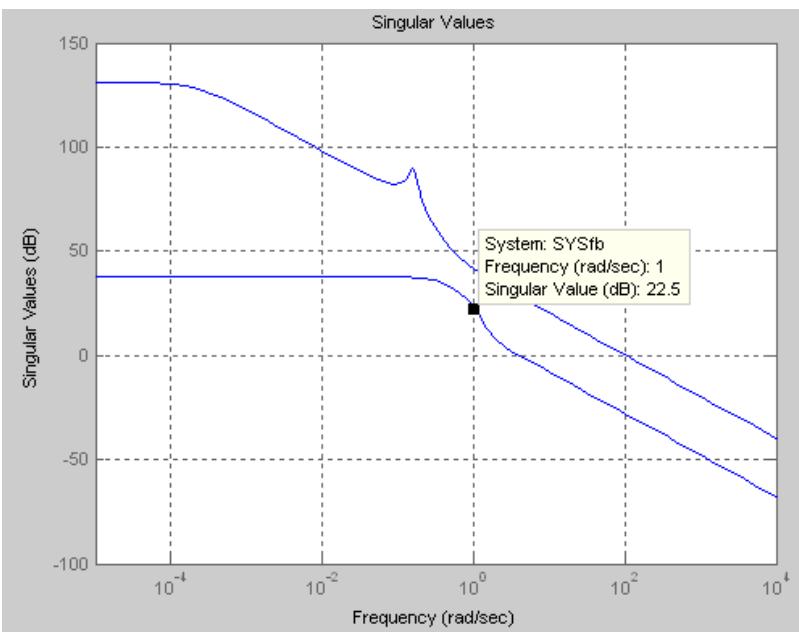
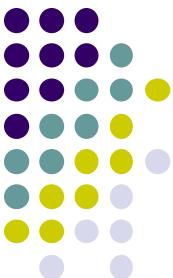
250 ft/s.

$$\mathbf{V}(t) = \sin(t) \quad \mathbf{h}(t) = 29.1 \times \exp\left(-\frac{t}{2.667}\right)$$

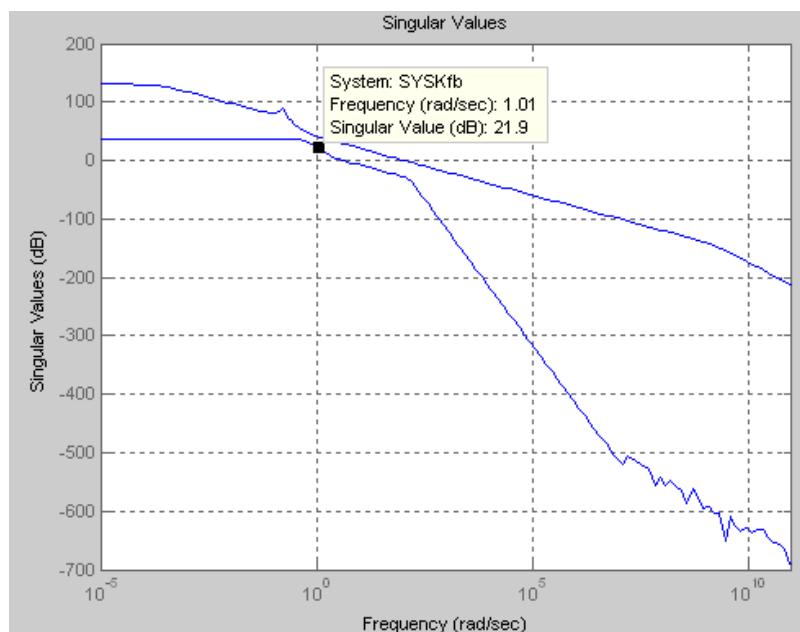
$$\mathbf{A} = \begin{pmatrix} -0.0386 & 18.9840 & -32.1930 & 0 & 0.0001 \\ -0.0010 & -0.6325 & 0.0056 & 1.0000 & 0.0000 \\ 0 & 0 & 0 & 1.0000 & 0 \\ 0.0001 & -0.7591 & -0.0008 & -0.5138 & 0.0000 \\ -0.0436 & -249.7600 & 249.7600 & 0 & 0 \end{pmatrix}$$

$$\mathbf{B} = \begin{pmatrix} 10.1000 & 0 \\ -0.0002 & 0 \\ 0 & 0 \\ 0.0247 & -0.0108 \\ 0 & 0 \end{pmatrix} \quad \mathbf{C} = \begin{pmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

$$-1 < \delta_{th} < 1 \quad -25^0 < \delta_e < 25^0$$



(a)



(b)

Figure 3: (a) Minimum and maximum singular values diagram for $SYS_{fb} = K_{fb}(sI - A)^{-1}B$ (dB). (b) Minimum and maximum singular values diagram for $SYS_{Kbf} = K_2(s)G_p(s)$ (dB).

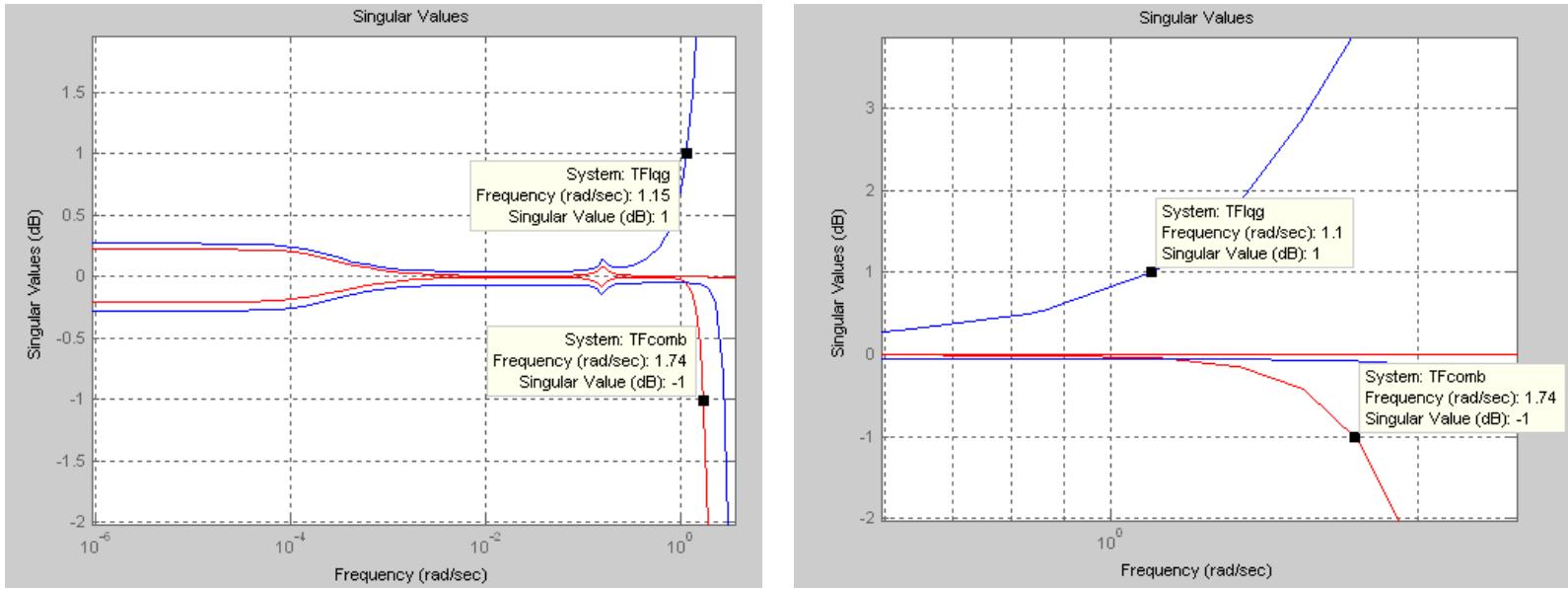
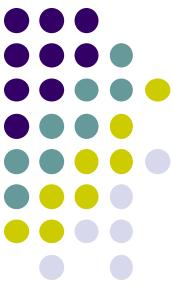
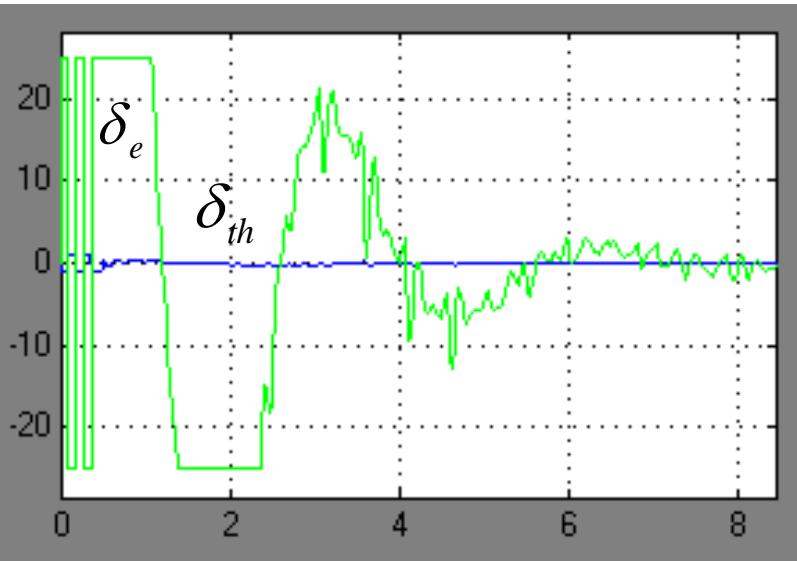
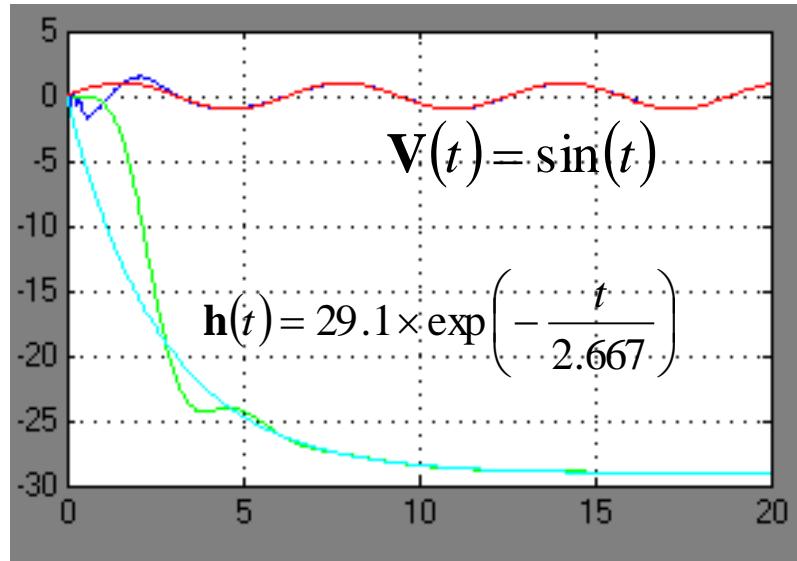
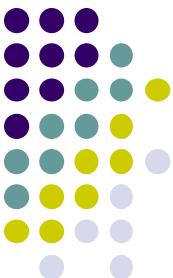


Figure 4: LQG/LTR minimum and maximum singular values diagram for input to output transfer function ($(\mathbf{I} + \mathbf{GK}_2)^{-1} \mathbf{GK}_2$)

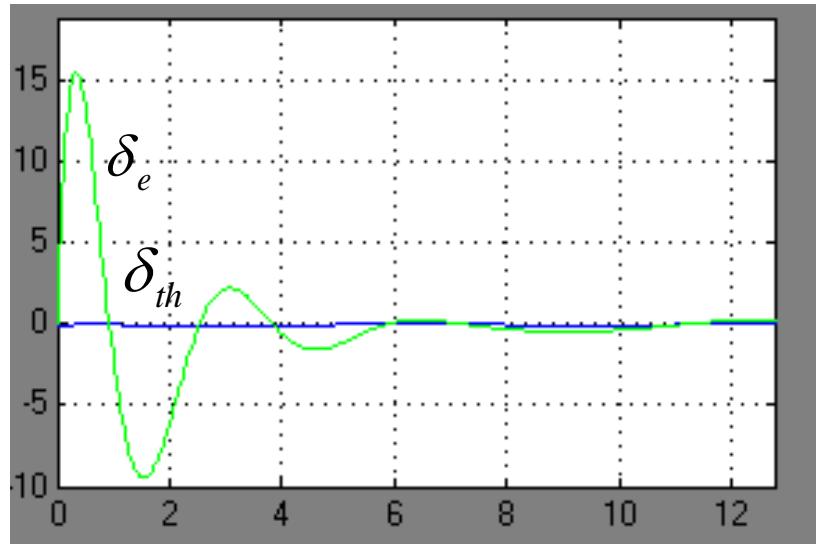
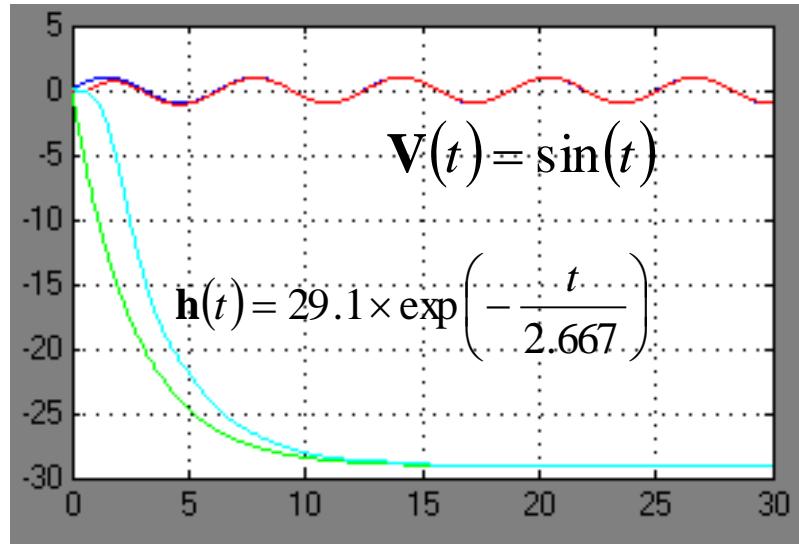
and combined method minimum and maximum singular values diagram for input to output transfer function ($(\mathbf{I} + \mathbf{GK}_2)^{-1} \mathbf{GK}_1$) (dB).



(a)

(b)

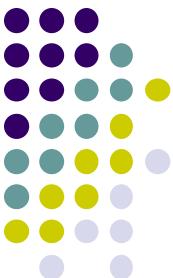
Figure 5: (a) LQG/LTR's tracking performance
(b) Control vector



(a)

(b)

Figure 6: (a) combined method's tracking performance
(b) Control vector

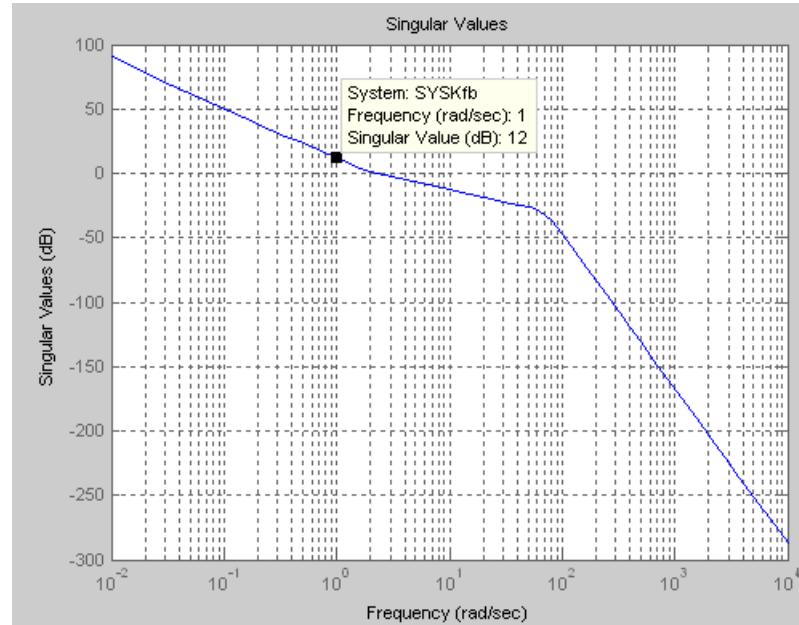
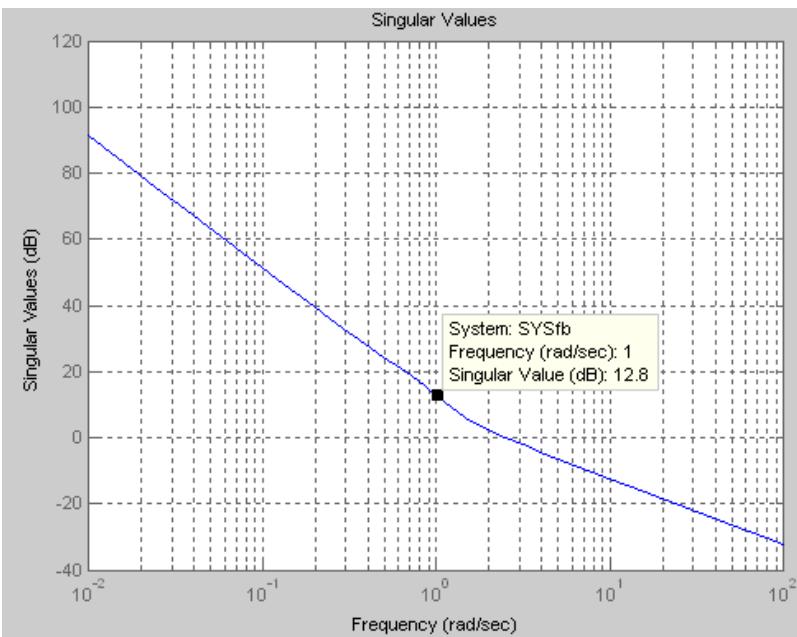
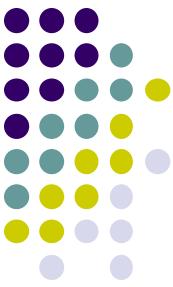


Example 2: The example is about Longitudinal Control for automatic landing. The matrices A, B and C describe the longitudinal dynamics for a medium size transport aircraft in the flare phase when its speed is 250 ft/s.

$$\mathbf{A} = \begin{pmatrix} -0.6463 & 0 & 1.0000 & 0 & 0 \\ 0 & 0 & 1.0000 & 0 & 0 \\ -0.7739 & 0 & -0.5298 & 0 & -0.0110 \\ -250.0000 & 250.0000 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -10.0000 \end{pmatrix}$$

$$\mathbf{B} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 10 \end{pmatrix} \quad -25^0 < \delta_{te} < 25^0$$
$$\mathbf{h}(t) = 36.37 \times \exp\left(-\frac{t}{3.333}\right)$$

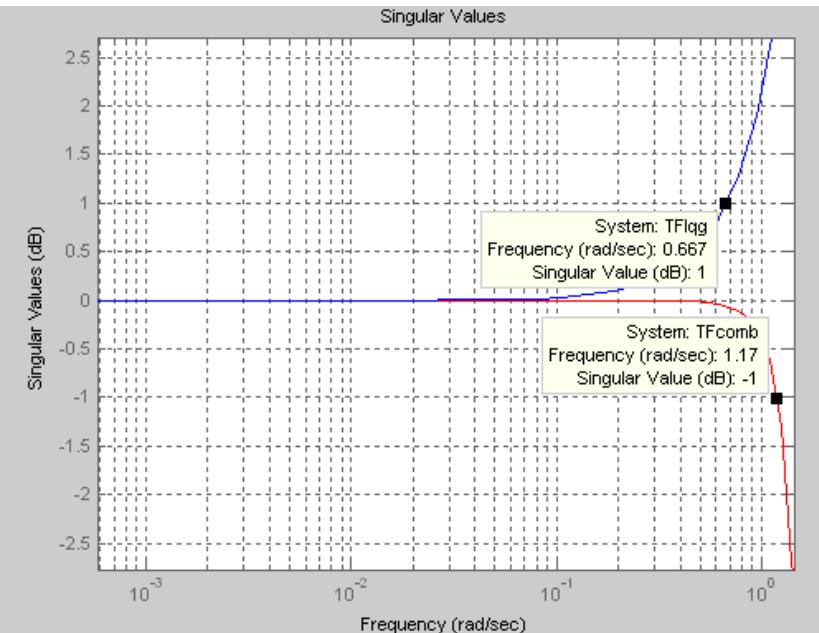
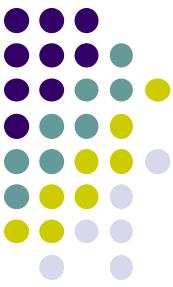
$$\mathbf{C} = (0 \quad 0 \quad 0 \quad 1 \quad 0)$$



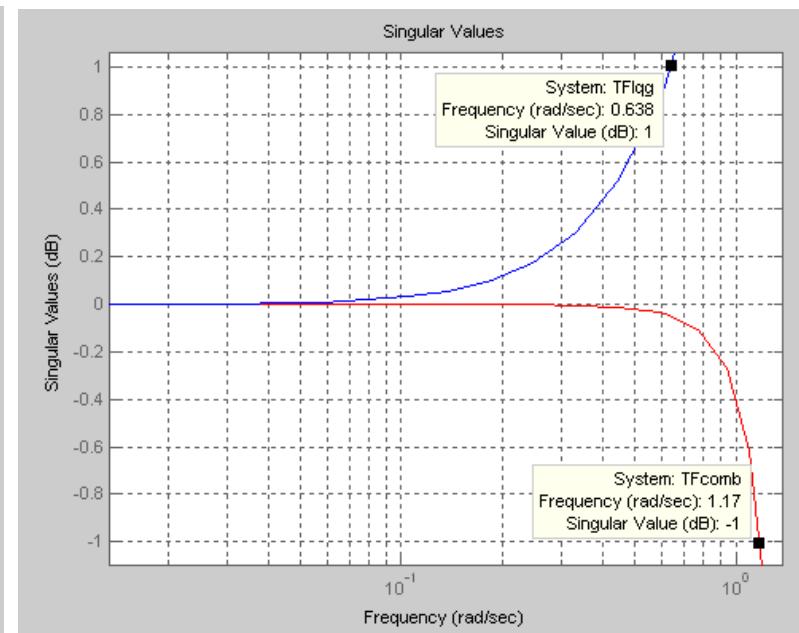
(a)

(b)

Figure 7: (a) Minimum and maximum singular values diagram for $SYS_{fb} = K_{fb}(sI - A)^{-1}B$ (dB). (b) Minimum and maximum singular values diagram for $SYS_{Kbf} = K_2(s)G_p(s)$ (dB).



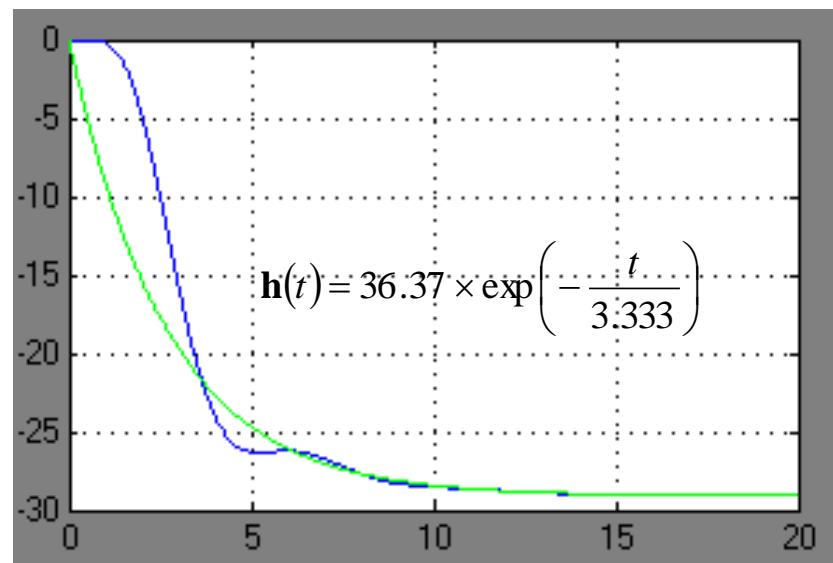
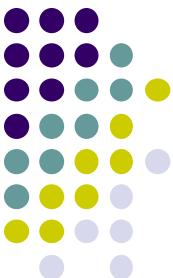
(a)



(b)

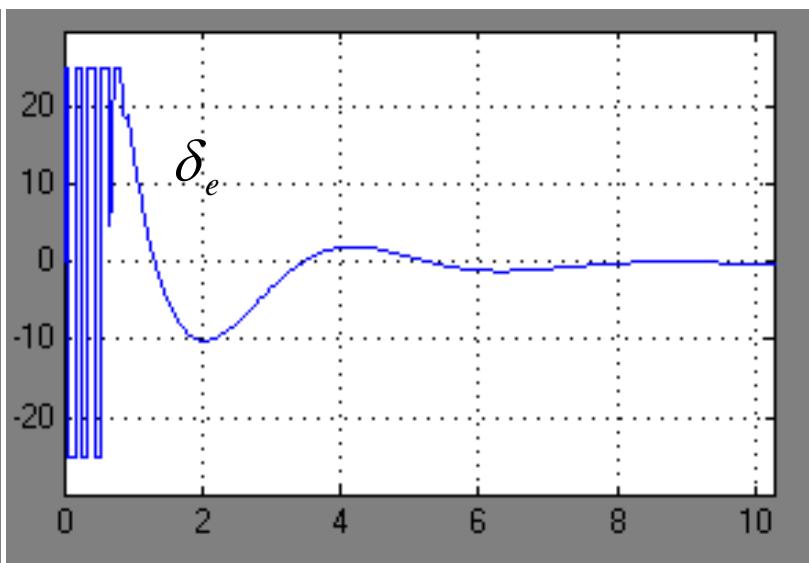
Figure 8 : (a) LQG/LTR's minimum and maximum singular values diagram for input to output transfer function ($(\mathbf{I} + \mathbf{GK}_2)^{-1} \mathbf{GK}_2$)

(b) combined method's minimum and maximum singular values diagram for input to output transfer function ($(\mathbf{I} + \mathbf{GK}_2)^{-1} \mathbf{GK}_1$) (dB).

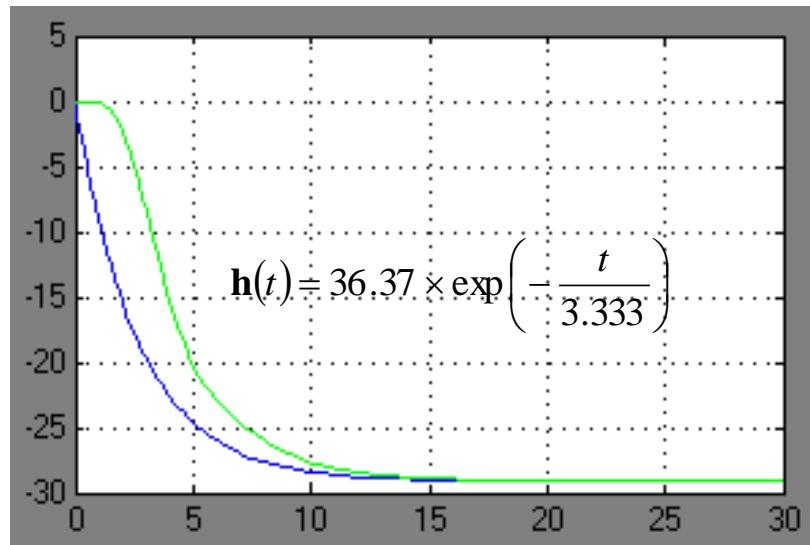
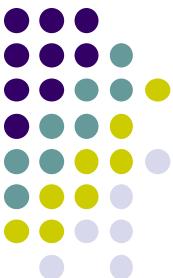


(a)

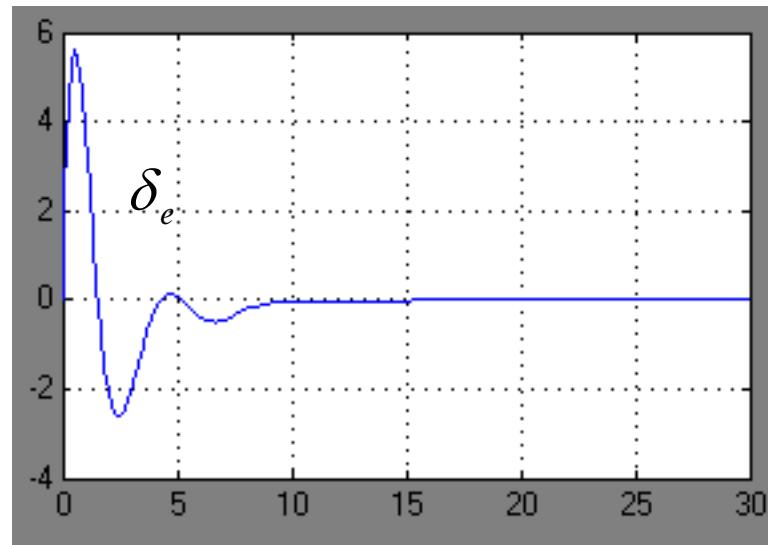
Figure 9: (a) LQG/LTR's tracking performance
(b) Control



(b)



(a)



(b)

Figure 10: (a) combined method's tracking performance
(b) Control vector

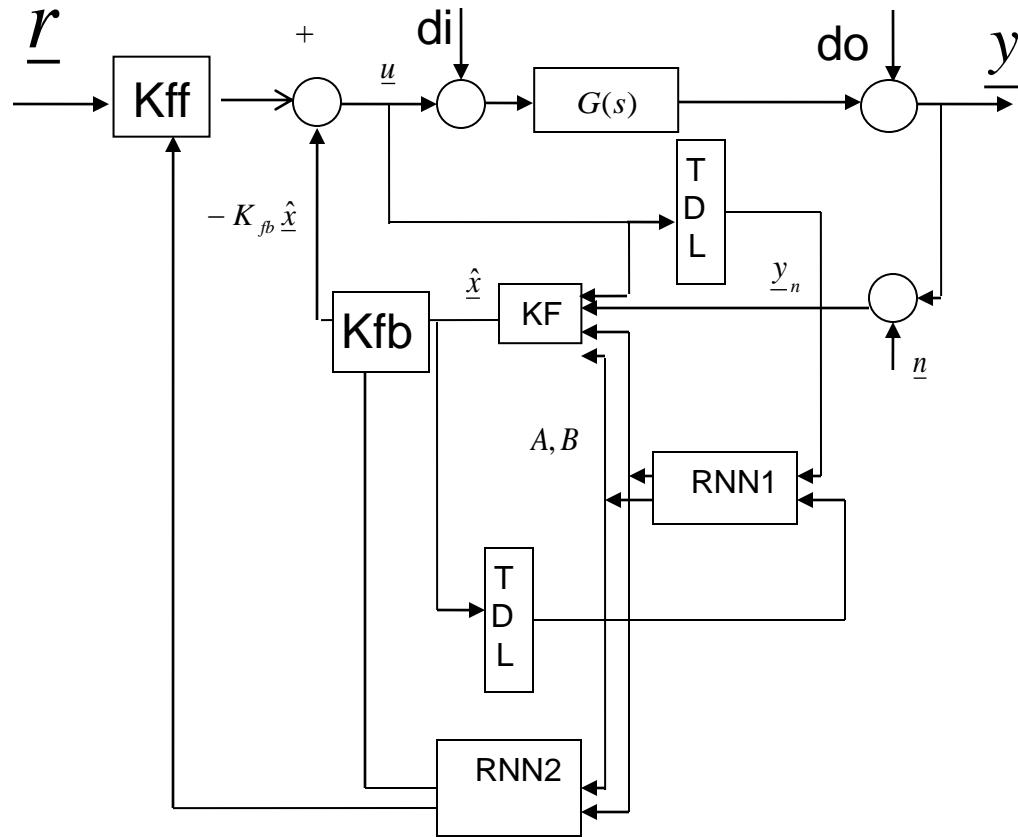


Figure 11: A new idea for Online Controller system



End

Thank you for your attention