## CONCORDIA UNIVERSITY FACULTY OF ENGINEERING AND COMPUTER SCIENCE DEPARTMENT OF MECHANICAL ENGINEERING

## PROBLEM I [12 pts]

A frictionless piston shown in the figure below has a mass of 16 kg . Heat is added until the temperature reaches $400^{\circ} \mathrm{C}$. If the initial quality is $20 \%$, find:
a) the initial pressure,
b) the mass of the water,
c) the quality when the piston hits the stops,
d) the work done.

| $P_{1}$ | 120 GPa |
| :--- | :---: |
| $\mathrm{m}_{2}$ | 0.001373 Kg |
| $x_{2}$ | 0.32 |
| $\mathbf{W}$ | 28.3 Jl |



PROBLEM II [12 pts]
Two kilograms of air experiences the three-process cycle in the figure below. Calculate the net work.



## PROBLEM III [6 pts]

1. Express mathematically the variation of pressure with depth for an ideal gas.
2. Demonstrate that the compressive/expensive work (like in piston-cylinder assembly), can be computed as: $\int P d V$
3. What is thermodynamic equilibrium?

CONSTANTS FOR ALL PROBLEMS: $\mathbf{P}_{\mathrm{atm}}=100 \mathrm{kPa}$ For air: $\mathbf{R}=0.2870 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$

## TABLEA-5

## TABLE

Ṡaturated water-Pressure table

|  |  | Specific volume,$\qquad$ $\mathrm{m}^{3} / \mathrm{kg}$ |  | Internal energy, king |  |  | Enthaipy, $\mathrm{kJ} / \mathrm{kg}$ |  |  | Entropy, <br> $\mathrm{kJ} / \mathrm{kg} \cdot \mathrm{K}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Press., PkPa | Sat. temp., $T_{\text {sat }}{ }^{\circ} \mathrm{C}$ | Sat. liquid, $v_{f}$ | Sat. vapor, $v_{g}$ | Sat. liquid, $u_{f}$ | Evap., $u_{f g}$ | Sat. vapor, $u_{g}$ | Sat. liquid, $h_{f}$ | Evap., $h_{f g}$ | Sat. vapor, $h_{g}$ | Sat. liquid, $s_{f}$ | Evap., $s_{t g}$ | Sat. vapor, $\mathrm{S}_{\mathrm{B}}$ |
| 1.0 | 6.97 | 0.001000 | 129 | 02 | 2355.2 | 2384.5 | 29.303 | 2484.4 | 2513.7 | 0.1059 | 8.8690 | 8.9749 |
| 1.5 | 13.02 | 0.001001 | 87.964 | 54.686 | 2338.1 | 2392.8 | 54.688 | 2470.1 | 2524.7 | 0.1956 | 8.6314 | 8.8270 |
| 2.0 | 17.50 | 0.001001 | 66.990 | 73.431 | 2325.5 | 2398.9 | 73.433 | 2459.5 | 2532.9 | 0.2606 | 8.4621 | 8.7227 |
| 2.5 | 21.08 | 0.001002 | 54.242 | 88.422 | 2315.4 | 2403.8 | 88.424 | 2451.0 | 2539.4 | 0.3118 | 8.3302 | 8.6421 |
| 3.0 | 24.08 | 0.001003 | 45.654 | 100.98 | 2306.9 | 2407.9 | 100.98 | 2443.9 | 2544.8 | 0.3543 | 8.2222 | 8.5765 |
| 4.0 | 28.96 | 0.001004 | 34.791 | 121.39 | 2293.1 | 2414.5 | 121.39 | 2432.3 | 2553.7 | 0.4224 | 8.0510 | 8.4734 |
| 5.0 | 32.87 | 0.001005 | 28.185 | 137.75 | 2282.1 | 2419.8 | 137.75 | 2423.0 | 2560.7 | 0.4762 | 7.9176 | 8.3938 |
| 7.5 | 40.29 | 0.001008 | 19.233 | 168.74 | 2261.1 | 2429.8 | 168.75 | 2405.3 | 2574.0 | 0.5763 | 7.6738 | 8.2501 |
| 10 | 45.81 | 0.001010 | 14.670 | 191.79 | 2245.4 | 2437.2 | 191.81 | 2392.1 | 2583.9 | 0.6492 | 7.4996 | 8.1488 |
| 15 | 53.97 | 0.001014 | 10.020 | 225.93 | 2222.1 | 2448.0 | 225.94 | 2372.3 | 2598.3 | 0.7549 | 7.2522 | 8.0071 |
| 20 | 60.06 | 0.001017 | 7.6481 | 251.40 | 2204.6 | 2456.0 | 251.42 | 2357.5 | 2608.9 | 0.8320 | 7.0752 | 7.9073 |
| 25 | 64.96 | 0.001020 | 6.2034 | 271.93 | 2190.4 | 2462.4 | 271.96 | 2345.5 | 2617.5 | 0.8932 | 6.9370 | 7.8302 |
| 30 | 69.09 | 0.001022 | 5.2287 | 289.24 | 2178.5 | 2467.7 | 289.27 | 2335.3 | 2624.6 | 0.9441 | 6.8234 | 7.7675 |
| 40 | 75.86 | 0.001026 | 3.9933 | 317.58 | 2158.8 | 2476.3 | 317.62 | 2318.4 | 2636.1 | 1.0261 | 6.6430 | 7.6691 |
| 50 | 81.32 | 0.001030 | 3.2403 | 340.49 | 2142.7 | 2483.2 | 340.54 | 2304.7 | 2645.2 | 1.0912 | 6.5019 | 7.5931 |
| 5 | 91.76 | 0.001037 | 2.2172 | 384.36 | 2111.8 | 2496.1 | 384.44 | 2278.0 | 2662.4 | 1.2132 | 6.2426 | 7.4558 |
| 100 | 99.61 | 0.001043 | 1.6941 | 417.40 | 2088.2 | 2505.6 | 417.51 | 2257.5 | 2675.0 | 1.3028 | 6.0562 | 7.3589 |
| 101.325 | 99.97 | 0.001043 | 1.6734 | 418.95 | 2087.0 | 2506.0 | 419.06 | 2256.5 | 2675.6 | 1.3069 | 6.0476 | 7.3545 |
| 125 | 105.97 | 0.001048 | 1.3750 | 444.23 | 2068.8 | 2513.0 | 444.36 | 2240.6 | 2684.9 | 1.3741 | 5.9100 | 7.2841 |
| 150 | 111.35 | 0.001053 | 1.1594 | 466.97 | 2052.3 | 2519.2 | 467.13 | 2226.0 | 2693.1 | 1.4337 | 5.7894 | 7.2231 |
| 5 | 116.04 | 0.001057 | 1.0037 | 486.82 | 2037.7 | 2524.5 | 487.01 | 2213.1 | 2700.2 | 1.4850 | 5.6865 | 7.1716 |
| 200 | 120.21 | 0.001061 | 0.88578 | 504.50 | 2024.6 | 2529.1 | 504.71 | 2201.6 | 2706.3 | 1.5302 | 5.5968 | 7.1270 |
| 225 | 123.97 | 0.001064 | 0.79329 | 520.47 | 2012.7 | 2533.2 | 520.71 | 2191.0 | 2711.7 | 1.5706 | 5.5171 | 7.0877 |
| 250 | 127.41 | 0.001067 | 0.71873 | 535.08 | 2001.8 | 2536.8 | 535.35 | 2181.2 | 2716.5 | 1.6072 | 5.4453 | 7.0525 |
| 275 | 130.58 | 0.001070 | 0.65732 | 548.57 | 1991.6 | 2540.1 | 548.86 | 2172.0 | 2720.9 | 1.6408 | 5.3800 | 7.0207 |
| 300 | 133.52 | 0.001073 | 0.60582 | 561.11 | 1982.1 | 2543.2 | 561.43 | 2163.5 | 2724.9 | 1.6717 | 5.3200 | 6.9917 |
| 325 | 136.27 | 0.001076 | 0.56199 | 572.84 | 1973.1 | 2545.9 | 573.19 | 2155.4 | 2728.6 | 1.7005 | 5.2645 | 6.9650 |
| 350 | 138.86 | 0.001079 | 0.52422 | 583.89 | 1964.6 | 2548.5 | 584.26 | 2147.7 | 2732.0 | 1.7274 | 5.2128 | 6.9402 |
| 375 | 141.30 | 0.001081 | 0.49133 | 594.32 | 1956.6 | 2550.9 | 594.73 | 2140.4 | 2735.1 | 1.7526 | 5.1645 | 6.9171 |
| 400 | 143.61 | 0.001084 | 0.46242 | 604.22 | 1948.9 | 2553.1 | 604.6 | 2133.4 | 273 | 1.7765 | 5.1191 | 6.8955 |
| 450 | 147.90 | 0.001088 | 0.41392 | 622.65 | 1934.5 | 2557.1 | 623.14 | 2120.3 | 2743.4 | 1.8205 | 5.0356 | 6.8561 |
| 500 | 151.83 | 0.001093 | 0.37483 | 639.54 | 1921.2 | 2560.7 | 640.09 | 2108.0 | 2748.1 | 1.8604 | 4.9603 | 6.8207 |
| 550 | 155.46 | 0.001097 | 0.34261 | 655.16 | 1908.8 | 2563.9 | 655.77 | 2096.6 | 2752.4 | 1.8970 | 4.8916 | 6.7886 |
| 600 | 158.83 | 0.001101 | 0.31560 | 669.72 | 1897.1 | 2566.8 | 670.38 | 2085.8 | 2756.2 | 1.9308 | 4.8285 | 6.7593 |
| 650 | 161.98 | 0.001104 | 0.29260 | 683.37 | 1886.1 | 2569.4 | 684.08 | 2075.5 | 2759.6 | 1.9623 | 4.7699 | 6.7322 |
| 700 | 164.95 | 0.001108 | 0.27278 | 696.23 | 1875.6 | 2571.8 | 697.00 | 2065.8 | 2762.8 | 1.9918 | 4.7153 | 6.7071 |
| 750 | 167.75 | 0.001111 | 0.25552 | 708.40 | 1865.6 | 2574.0 | 709.24 | 2056.4 | 2765 | 2.0195 | 4.6642 | 6.683 |

## CONCORDIA UNIVERSITY FACULTY OF ENGINEERING AND COMPUTER SCIENCE DEPARTMENT OF MECHANICAL ENGINEERING

## PROBLEM I [12 pts]

A piston-cylinder device with a set of stops initially contains 0.3 kg of steam at 1.0 MPa and $400^{\circ} \mathrm{C}$. The location of the stops corresponds to 60 percent of the initial volume. Now the steam is cooled.
Determine the compression work if the final state is:
a) 1.0 MPa and $250^{\circ} \mathrm{C}$,
b) 500 kPa
c) Also determine the temperature at the final state in part (b).

| $W$ (a) | 22.16 kJ |
| :--- | :---: |
| $W(b)$ | 36.79 kJ |
| $\mathrm{~T}_{2}$ | $151.8^{\circ} \mathrm{C}$ |



## PROBLEM II [12 pts]

Six grams of air is contained in the cylinder shown in the figure below. The air is heated until the piston raises 50 mm . The spring just touches the piston initially. Calculate:
a) the temperature when the piston leaves the stops,
b) the work done.

| $T_{1}$ | 530 K |
| :--- | :--- |
| $\mathbf{W}$ | 0.804 kJ |



## PROBLEM III [6 pts]

- Explain physically why $\mathrm{C}_{\mathrm{p}}$ is higher than $\mathrm{C}_{\mathrm{v}}$ for an ideal gas?
- Demonstrate that for an ideal gas: $\mathrm{C}_{\mathrm{p}}-\mathrm{C}_{\mathrm{v}}=\mathrm{R}$.
- What does the area under a Cp .vs T graph represents?


## CONSTANTS FOR ALL PROBLEMS: $\mathbf{P}_{\mathrm{atm}}=100 \mathrm{kPa}$ For air: $\mathbf{R}=0.2870 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$

## 918 I Thermodynamics

| TABLE A-5 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Saturated water-Pressure table |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Specific volume, $\mathrm{m}^{3} / \mathrm{kg}$ |  | Internal energy,$\qquad$ |  |  | Enthalpy, $\mathrm{kJ} / \mathrm{kg}$ |  |  | Entropy, <br> kJ/kg • K |  |  |
| Press., <br> PkPa | Sat. temp., $T_{\text {sat }}{ }^{\circ} \mathrm{C}$ | Sat. <br> liquid, <br> $v_{f}$ | Sat. <br> vapor, $v_{g}$ | Sat. liquid, $u_{f}$ | Evap., $u_{f g}$ | Sat. <br> vapor, $u_{g}$ | Sat. <br> liquid, $h_{f}$ | Evap., $h_{t g}$ | Sat. <br> vapor, $h_{s}$ | Sat. <br> liquid, $s_{f}$ | Evap., $s_{\text {和 }}$ | Sat. <br> vapor, <br> $5_{8}$ |
| 1.0 | 6.97 | 0.001000 | 129.19 | 29.302 | 2355.2 | 2384.5 | 29.303 | 2484.4 | 2513.7 | 0.1059 | 8.8690 | 8.9749 |
| 1.5 | 13.02 | 0.001001 | 87.964 | 54.686 | 2338.1 | 2392.8 | 54.688 | 2470.1 | 2524.7 | 0.1956 | 8.6314 | 8.8270 |
| 2.0 | 17.50 | 0.001001 | 66.990 | 73.431 | 2325.5 | 2398.9 | 73.433 | 2459.5 | 2532.9 | 0.2606 | 8.4621 | 8.7227 |
| 2.5 | 21.08 | 0.001002 | 54.242 | 88.422 | 2315.4 | 2403.8 | 88.424 | 2451.0 | 2539.4 | 0.3118 | 8.3302 | 8.6421 |
| 3.0 | 24.08 | 0.001003 | 45.654 | 100.98 | 2306.9 | 2407.9 | 100.98 | 2443.9 | 2544.8 | 0.3543 | 8.2222 | 8.5765 |
| 4.0 | 28.96 | 0.001004 | 34.791 | 121.39 | 2293.1 | 2414.5 | 121.39 | 2432.3 | 2553.7 | 0.4224 | 8.0510 | 8.4734 |
| 5.0 | 32.87 | 0.001005 | 28.185 | 137.75 | 2282.1 | 2419.8 | 137.75 | 2423.0 | 2560.7 | 0.4762 | 7.9176 | 8.3938 |
| 7.5 | 40.29 | 0.001008 | 19.233 | 168.74 | 2261.1 | 2429.8 | 168.75 | 2405.3 | 2574.0 | 0.5763 | 7.6738 | 8.2501 |
| 10 | 45.81 | 0.001010 | 14.670 | 191.79 | 2245.4 | 2437.2 | 191.81 | 2392.1 | 2583.9 | 0.6492 | 7.4996 | 8.1488 |
| 15 | 53.97 | 0.001014 | 10.020 | 225.93 | 2222.1 | 2448.0 | 225.94 | 2372.3 | 2598.3 | 0.7549 | 7.2522 | 8.0071 |
| 20 | 60.06 | 0.001017 | 7.6481 | 251.40 | 2204.6 | 2456.0 | 251.42 | 2357.5 | 2608.9 | 0.8320 | 7.0752 | 7.9073 |
| 25 | 64.96 | 0.001020 | 6.2034 | 271.93 | 2190.4 | 2462.4 | 271.96 | 2345.5 | 2617.5 | 0.8932 | 6.9370 | 7.8302 |
| 30 | 69.09 | 0.001022 | 5.2287 | 289.24 | 2178.5 | 2467.7 | 289.27 | 2335.3 | 2624.6 | 0.9441 | 6.8234 | 7.7675 |
| 40 | 75.86 | 0.001026 | 3.9933 | 317.58 | 2158.8 | 2476.3 | 317.62 | 2318.4 | 2636.1 | 1.0261 | 6.6430 | 7.6691 |
| 50 | 81.32 | 0.001030 | 3.2403 | 340.49 | 2142.7 | 2483.2 | 340.54 | 2304.7 | 2645.2 | 1.0912 | 6.5019 | 7.5931 |
| 75 | 91.76 | 0.001037 | 2.2172 | 384.36 | 2111.8 | 2496.1 | 384.44 | 2278.0 | 2662.4 | 1.2132 | 6.2426 | 7.4558 |
| 100 | 99.61 | 0.001043 | 1.6941 | 417.40 | 2088.2 | 2505.6 | 417.51 | 2257.5 | 2675.0 | 1.3028 | 6.0562 | 7.3589 |
| 101.325 | 99.97 | 0.001043 | 1.6734 | 418.95 | 2087.0 | 2506.0 | 419.06 | 2256.5 | 2675.6 | 1.3069 | 6.0476 | 7.3545 |
| 125 | 105.97 | 0.001048 | 1.3750 | 444.23 | 2068.8 | 2513.0 | 444.36 | 2240.6 | 2684.9 | 1.3741 | 5.9100 | 7.2841 |
| 150 | 111.35 | 0.001053 | 1.1594 | 466.97 | 2052.3 | 2519.2 | 467.13 | 2226.0 | 2693.1 | 1.4337 | 5.7894 | 7.2231 |
| 175 | 116.04 | 0.001057 | 1.0037 | 486.82 | 2037.7 | 2524.5 | 487.01 | 2213.1 | 2700.2 | 1.4850 | 5.6865 | 7.1716 |
| 200 | 120.21 | 0.001061 | 0.88578 | 504.50 | 2024.6 | 2529.1 | 504.71 | 2201.6 | 2706.3 | 1.5302 | 5.5968 | 7.1270 |
| 225 | 123.97 | 0.001064 | 0.79329 | 520.47 | 2012.7 | 2533.2 | 520.71 | 2191.0 | 2711.7 | 1.5706 | 5.5171 | 7.0877 |
| 250 | 127.41 | 0.001067 | 0.71873 | 535.08 | 2001.8 | 2536.8 | 535.35 | 2181.2 | 2716.5 | 1.6072 | 5.4453 | 7.0525 |
| 275 | 130.58 | 0.001070 | 0.65732 | 548.57 | 1991.6 | 2540.1 | 548.86 | 2172.0 | 2720.9 | 1.6408 | 5.3800 | 7.0207 |
| 300 | 133.52 | 0.001073 | 0.60582 | 561.11 | 1982.1 | 2543.2 | 561.43 | 2163.5 | 2724.9 | 1.6717 | 5.3200 | 6.9917 |
| 325 | 136.27 | 0.001076 | 0.56199 | 572.84 | 1973.1 | 2545.9 | 573.19 | 2155.4 | 2728.6 | 1.7005 | 5.2645 | 6.9650 |
| 350 | 138.86 | 0.001079 | 0.52422 | 583.89 | 1964.6 | 2548.5 | 584.26 | 2147.7 | 2732.0 | 1.7274 | 5.2128 | 6.9402 |
| 375 | 141.30 | 0.001081 | 0.49133 | 594.32 | 1956.6 | 2550.9 | 594.73 | 2140.4 | 2735.1 | 1.7526 | 5.1645 | 6.9171 |
| 400 | 143.61 | 0.001084 | 0.46242 | 604.22 | 1948.9 | 2553.1 | 604.66 | 2133.4 | 2738.1 | 1.7765 | 5.1191 | 6.8955 |
| 450 | 147.90 | 0.001088 | 0.41392 | 622.65 | 1934.5 | 2557.1 | 623.14 | 2120.3 | 2743.4 | 1.8205 | 5.0356 | 6.8561 |
| 500 | 151.83 | 0.001093 | 0.37483 | 639.54 | 1921.2 | 2560.7 | 640.09 | 2108.0 | 2748.1 | 1.8604 | 4.9603 | 6.8207 |
| 550 | 155.46 | 0.001097 | 0.34261 | 655.16 | 1908.8 | 2563.9 | 655.77 | 2096.6 | 2752.4 | 1.8970 | 4.8916 | 6.7886 |
| 600 | 158.83 | 0.001101 | 0.31560 | 669.72 | 1897.1 | 2566.8 | 670.38 | 2085.8 | 2756.2 | 1.9308 | 4.8285 | 6.7593 |
| 650 | 16198 | 0.001104 | 0.29260 | 683.37 | 1886.1 | 2569.4 | 684.08 | 2075.5 | 2759.6 | 1.9623 | 4.7699 | 6.7322 |

2250
2500 3000
3500
4000
6000
7000
8000
9000
10,000 11,000 12,000
13,000
14,000 15,000
16,000
17,000
18,000
19,000
20,000
21,000 22.00 n

## TABLE A-6

Superheated water (Continued)

| $\begin{aligned} & T \\ & { }^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $\begin{aligned} & u \\ & \mathrm{k} / \mathrm{kg} \end{aligned}$ | $h$ $\mathrm{kJ} / \mathrm{kg}$ | $\begin{aligned} & \mathrm{s} \mathrm{~J} / \mathrm{kg} \cdot \mathrm{~K} \end{aligned}$ | $\begin{aligned} & v \\ & \mathrm{~m}^{3} \mathrm{~kg} \end{aligned}$ | $\begin{aligned} & u \\ & \mathrm{~kJ} / \mathrm{kg} \end{aligned}$ | h $\mathrm{kJ} / \mathrm{kg}$ | $\begin{aligned} & s \\ & \mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K} \end{aligned}$ | $\begin{aligned} & v \\ & \mathrm{~m}^{3} / \mathrm{kg} \end{aligned}$ | $\begin{aligned} & u \\ & \mathrm{~kJ} / \mathrm{kg} \end{aligned}$ | $\begin{aligned} & h \\ & \mathrm{~kJ} / \mathrm{kg} \end{aligned}$ | $\begin{aligned} & \mathrm{s} \\ & \mathrm{kJg} \cdot \mathrm{~K} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $P=1.00 \mathrm{MPa}(179.88 \mathrm{C})$ |  |  |  | $P=1.20 \mathrm{MPa}\left(187.96{ }^{\circ} \mathrm{C}\right)$ |  |  |  | $P=1.40 \mathrm{MPa}\left(195.044^{\circ} \mathrm{C}\right.$ |  |  |  |
| Sat. | 0.19437 | 2582.8 | 2777.1 | 6.5850 | 0.16326 | 258 | 2783.8 | 6.5217 | 0.14078 | 2591.8 | 2788.9 | 6.4675 |
| 200 | 0.20602 | 2622.3 | 2828.3 | 6.6956 | 0.16934 | 2612.9 | 2816.1 | 6.5909 | 0.14303 | 2602.7 | 2803.0 | 6.4975 |
| 250 | 0.23275 | 2710.4 | 2943.1 | 6.9265 | 0.19241 | 2704.7 | 2935.6 | 6.8313 | 0.16356 | 2698.9 | 2927.9 | 6.7488 |
| 300 | 0.25799 | 2793.7 | 3051.6 | 7.1246 | 0.21386 | 2789.7 | 3046.3 | 7.0335 | 0.18233 | 2785.7 | 3040.9 | 6.9553 |
| 350 | 0.28250 | 2875.7 | 3158.2 | 7.3029 | 0.23455 | 2872.7 | 3154.2 | 7.2139 | 0.20029 | 2869.7 | 3150.1 | 7.137 |
| 400 | 0.30661 | 2957.9 | 3264.5 | 7.4670 | 0.25482 | 2955.5 | 3261.3 | 7.3793 | 0.21782 | 2953.1 | 3258.1 | 7.3046 |
| 00 | 0.35411 | 3125.0 | 3479.1 | 7.7642 | 0.29464 | 3123.4 | 3477.0 | 7.6779 | 0.25216 | 3121.8 | 3474.8 | 7.6047 |
| 600 | 0.40111 | 3297.5 | 3698.6 | 8.0311 | 0.33395 | 3296.3 | 3697.0 | 7.9456 | 0.28597 | 3295.1 | 3695.5 | 7.8730 |
| 700 | 0.44783 | 3476.3 | 3924.1 | 8.2755 | 0.37297 | 3475.3 | 3922.9 | 8.1904 | 0.31951 | 3474.4 | 3921.7 | 8.1183 |
| 000 | 0.49438 | 3661.7 | 4156.1 | 8.5024 | 0.41184 | 3661.0 | 4155.2 | 8.4176 | 0.35288 | 3660.3 | 4154.3 | 8.3458 |
| 900 | 0.54083 | 3853.9 | 4394.8 | 8.7150 | 0.45059 | 3853.3 | 4394.0 | 8.6303 | 0.38614 | 3852.7 | 4393.3 | 8.55 |
| 1000 | 0.58721 | 4052.7 | 4640.0 | 8.9155 | 0.48928 | 4052.2 | 4639.4 | 8.8310 | 0.41933 | 4051.7 | 4638.8 | 8.7595 |
| 1100 | 0.63354 | 4257.9 | 4891 | 9.1057 | 0.52792 | 4257.5 | 4891.0 | 9.0212 | 10.45247 | 4257.0 | 4890.5 | 8.9497 |

FACULTY OF ENGINEERING AND COMPUTER SCIENCE DEPARTMENT OF MECHANICAL ENGINEERING

## ENGR-251 THERMODYNAMICS I

Student's Name:
I.D.:

Duration 60 minutes

## PROBLEM 1

$0.1 \mathrm{~m}^{3}$ of an ideal gas is compressed from a pressure of 120 kPa and temperature of $25^{\circ} \mathrm{C}$ to a pressure of 1.2 MPa according to the law PV ${ }^{1.2}=$ constant. Determine:

1- The work transferred during the compression.
Note: Demonstrate the formulation of the work for a polytropic process (4 points), otherwise use the formulation:
Work for a polytropic process: $W=\frac{P_{2} V_{2}-P_{1} V_{1}}{1-n}$
2- The change in internal energy.
3- The heat transferred during the compression.
Assume: $\mathrm{C}_{\mathrm{v}}=0.72 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ and $\mathrm{R}=0.285 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$

## Formulas:

Ideal gas law: $P v=R T$
First law of thermodynamics for a closed system: $\Delta U=Q-W$ (neglecting $\Delta \mathrm{E}_{\mathrm{k}}$ and $\Delta \mathrm{E}_{\mathrm{p}}$ )
Specific heat at constant pressure: $C_{p}=\frac{\partial h}{\partial T}$
Specific heat at constant volume: $C_{v}=\frac{\partial u}{\partial T}$

## PROBLEM 2

Water contained in a piston-cylinder assembly undergoes two processes in series from an initial state where the pressure is 1 MPa and the temperature is $400^{\circ} \mathrm{C}$.

Process 1-2: The water is cooled as it is compressed at a constant pressure of 1 MPa to the saturated vapor state.
Process 2-3: The water is cooled at constant volume to $150^{\circ} \mathrm{C}$.

1- For the overall process determine the work, in $\mathrm{kJ} / \mathrm{kg}$.
2- For the overall process determine the heat transfer, in $\mathrm{kJ} / \mathrm{kg}$.

## Formulas:

Work: $W=\int_{\text {initial state }}^{\text {final state }} P d v$
First law of thermodynamics for a closed system: $\Delta U=Q-W$ (neglecting $\Delta \mathrm{E}_{k}$ and $\Delta \mathrm{E}_{\mathrm{p}}$ )

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## Student's Name:

I.D.:

## PROBLEM I [40 pt]

Carbon dioxide contained in a piston-cylinder device is compressed from 0.3 to $0.1 \mathrm{~m}^{3}$. During the process, the pressure and the volume are related by $\mathrm{P}=\mathrm{a} \mathrm{V}^{-2}$, where $\mathrm{a}=8 \mathrm{kPa} \mathrm{m}^{6}$.

- Plot the process on a P-v diagram.
- Calculate the work done on the carbon dioxide during this process.


## PROBLEM II [40 pt]

Air is compressed from 101.325 kPa and $17^{\circ} \mathrm{C}$ to a pressure of 1000 kPa while being cooled at a rate of $25 \mathrm{~kJ} / \mathrm{kg}$ by circulating water through the compressor casing. The volume flow rate of the air at the inlet conditions is $142 \mathrm{~m}^{3} / \mathrm{min}$, and the power input to the compressor is 522 kW . Determine:
a- The mass flow rate of the air in $\mathrm{kg} / \mathrm{s}$.
b- The temperature at the compressor exit.

## PROBLEM III [20 pt]

- Explain physically why $\mathrm{C}_{\mathrm{p}}$ is higher than $\mathrm{C}_{\mathrm{v}}$ for an ideal gas?
- Express mathematically the variation of pressure with depth for an ideal gas.
- Show under which conditions, the total heat provided to a gas in a piston-cylinder assembly is converted into work?


## CONSTANTS FOR AIR

```
R = 0.287 kJ/kg K
C
C
```


# CONCORDIA UNIVERSITY <br> FACULTY OF ENGINEERING AND COMPUTER SCIENCE DEPARTMENT OF MECHANICAL ENGINEERING 

## Student's Name:

I.D.:

## PROBLEM I [40 pt]

A piston-cylinder device whose piston is resting on top of a set of stops initially contains 0.5 kg of helium gas at 100 kPa and $25^{\circ} \mathrm{C}$. The mass of the piston is such that 500 kPa of pressure is required to rise it. How much heat (in kJ ) must be transferred to the helium before the piston starts rising?

| Heat |  |
| :--- | :--- |

## PROBLEM II [40 pt]

Argon gas enters an adiabatic turbine steadily at 900 kPa and $450^{\circ} \mathrm{C}$ with a velocity of $80 \mathrm{~m} / \mathrm{s}$ and leaves at 150 kPa with a velocity of $150 \mathrm{~m} / \mathrm{s}$. The inlet area of the turbine is $60 \mathrm{~cm}^{2}$. If the power output of the turbine is 250 kW.
Determine the exit temperature of the argon?


## PROBLEM III [20 pt]

- Explain physically why $\mathrm{C}_{\mathrm{p}}$ is higher than $\mathrm{C}_{\mathrm{v}}$ for an ideal gas?
- Determine the expression of the compressive/expansion work when the process is: a) isobaric; b) isochoric; c) isothermal (consider an ideal gas); d) polytropic.
- Knowing that for an ideal gas the internal energy is only a function of temperature, show then that the enthalpy is also only a function of temperature.

| CONSTANTS FOR HELIUM | CONSTANTS FOR ARGON |
| :--- | :--- |
|  |  |
| $C_{v}=3.1156 ~ k J / k g ~ K ~$ | $C_{v}=0.3122 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ |
| $C_{p}=5.1926 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ | $C_{p}=0.5203 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$ |

