# MECH 343 Theory of Machines I

Time: \_ \_ W \_ \_17:45 - 20:15

Lecture 12

## Example

- A has constant velocity 12.6ft/s. mechanism moves in horizontal plane. M<sub>3</sub> and IG<sub>3</sub> are 2.2lb and 0.0479in.lb.s<sup>2</sup>
- Find F<sub>A</sub> required for dynamic equilibrium. M<sub>2</sub> and M<sub>2</sub> assume to be negligible and neglect friction
- Draw velocity polygon to get  $V_{B/A}$  and then find the  $A^n_{B/A}$  with  $\omega_3$  from which complete the acceleration polygon kowing the direction of  $A^t_{B/A}$  and  $A_B$
- From  $A_B$ ,  $A_G$  can be scaled as 444ft/s<sup>2</sup> and

$$\alpha_3 = \frac{A_{BA}^t}{R_{BA}} = \frac{(713 \text{ ft/s}^2)(12 \text{ in/ft})}{10 \text{ in}} = 856 \text{ rad/s}^2 \text{ cw}.$$

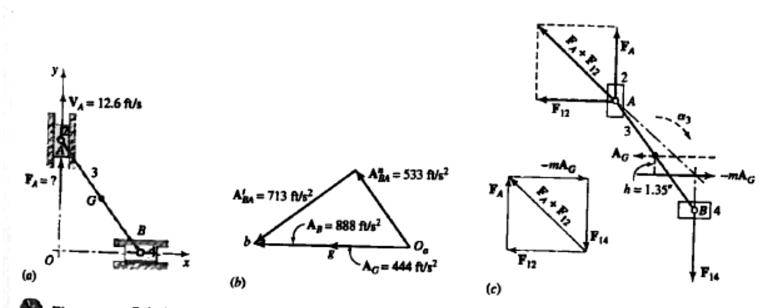


Figure 14.8 Solution for Example 14.3. (a) Scale drawing with  $R_{BA} = 10$  in,  $R_{GA} = 5$  in,  $R_{AO} = 8$  in, and  $R_{BO} = 6$  in. (b) Acceleration polygon. (c) Free-body diagram and force polygon.

## Example

- Knowing  $M_3$  and  $IG_3$  are 2.2lb and 0.0479in.lb.s<sup>2</sup>h can be found
  - $h = \frac{(0.047 \text{ 9 in} \cdot \text{lb} \cdot \text{s}^2)(856 \text{ rad/s}^2)}{(0.005 \text{ 70 lb} \cdot \text{s}^2/\text{in})(444 \text{ ft/s}^2)(12 \text{ in/ft})} = 1.35 \text{ in}$
- Drawing the FBD we can analyze this to find  $F_A$
- $F_{14}$  is the vertical reaction force and  $F_{12}$  is the horizontal reaction force.  $F_{12}$  should be equal and opposite to  $mA_G$
- $mA_G$  is offset by h from G. using this LOA of  $F_A + F_{12}$  can be found using point of concurrence of  $F_{14}$  and  $-mA_G$
- F<sub>A</sub> is found to be 27lb

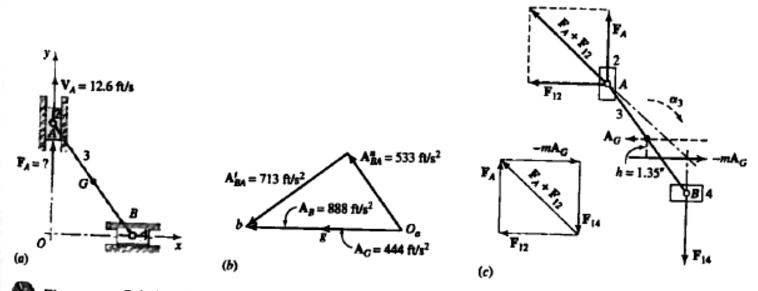


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# Example

### **EXAMPLE 14.3**

For the mechanism illustrated in Fig. 14.8a, point A has a constant velocity  $V_A = 12.6$  ft/s. The mechanism moves in a horizontal plane with gravity normal to the plane of motion. The weight and principal mass moment of inertia of coupler link 3 are 2.20 lb and  $I_{G_3} = 0.047$  9 in · lb · s<sup>2</sup>, respectively. Determine the force  $F_A$  required for dynamic equilibrium of the mechanism. Assume that the weights of links 2 and 4 and friction in the mechanism are negligible.

#### SOLUTION

A kinematic analysis provides the acceleration information illustrated in the polygon of Fig. 14.8b. The acceleration of the mass center of the coupler link is  $A_G = 444$  ft/s<sup>2</sup> and

the angular acceleration of this link is

$$\alpha_3 = \frac{A_{BA}^t}{R_{BA}} = \frac{(713 \text{ ft/s}^2)(12 \text{ in/ft})}{10 \text{ in}} = 856 \text{ rad/s}^2 \text{ cw}.$$

The mass of the coupler link is  $m_3 = (2.20 \, \text{lb})/(386 \, \text{in/s}^2) = 0.00570 \, \text{lb-s}^2/\text{in}$ . Substituting this information into Eq. (14.17), the offset distance is

$$h = \frac{(0.047 \text{ 9 in} \cdot \text{lb} \cdot \text{s}^2)(856 \text{ rad/s}^2)}{(0.005 \text{ 70 lb} \cdot \text{s}^2/\text{in})(444 \text{ ft/s}^2)(12 \text{ in/ft})} = 1.35 \text{ in}$$

The free-body diagram of links 2, 3, and 4 and the resulting force polygon are illustrated in Fig. 14.8c. Note that the inertia force  $-mA_G$  is offset from G by the distance h so as to include a counterclockwise moment  $-I_{GG3}$  about G and with the inertia force in the opposite sense to  $A_G$ . The constraint reaction at B is  $F_{14}$  and, with no friction, is vertically downward. The forces at A are the constraint horizontal reaction  $F_{12}$  and the vertical actuating force  $F_A$ . Recognizing this as a four-force member, as demonstrated in Section 13.8, we find the concurrency point at the intersection of the offset inertia force and  $F_{14}$ , with the directions of both being known. The line of action of the total force  $F_{12} + F_A$  at A must pass through this point of concurrency. This fact permits construction of the force polygon, where the unknown forces  $F_{12}$  and  $F_A$ , having known directions, are found as components of  $F_{12} + F_A$ . The actuating force  $F_A$  is determined by measurement to be

$$\mathbf{F}_A = 27\hat{\mathbf{j}}$$
 lb.